



FOSSEE Winter Internship Report

On

Report Generation of Steel Connection Modules for Osdag

Submitted by

Roushan Raj

3rd Year B.Tech Student, Department of Computer Science and Engineering

B.I.T. Sindri

Sindri, Dhanbad, Jharkhand

Under the Guidance of

Prof. Siddhartha Ghosh

Department of Civil Engineering

Indian Institute of Technology Bombay

Mentors:

Ajmal Babu M S

Parth Karia

Ajinkya Dahale

February 3, 2026

Acknowledgments

I would like to extend my sincere gratitude to the following individuals and organizations whose guidance and support were instrumental in the successful completion of this fellowship project:

- My heartfelt thanks go to the Osdag team, particularly **Ajmal Babu M. S.**, **Ajinkya Dahale**, and **Parth Karia**, for their continuous technical expertise and collaborative support during the report generation of modules.
- I am truly grateful for the mentorship and inspiring leadership of **Prof. Siddhartha Ghosh**, Principal Investigator of the Osdag project, from the Department of Civil Engineering at IIT Bombay.
- I would like to express my gratitude to **Prof. Kannan M. Moudgalya**, Principal Investigator of the FOSSEE project, and the entire FOSSEE team in the Department of Chemical Engineering at IIT Bombay for their invaluable project guidance and academic support.
- My sincere appreciation is extended to **Usha Viswanathan**, **Vineeta Parmar**, and the FOSSEE management team for their exceptional administrative support, which ensured the seamless progression of this internship.
- I gratefully acknowledge the financial and institutional support from the **National Mission on Education through Information and Communication Technology (NMEICT)**, Ministry of Education, Government of India.
- Finally, I would like to thank my alma mater, **B.I.T. Sindri**, along with the mentors and administrative staff who have supported me throughout my academic journey.

Contents

1	Introduction	5
1.1	National Mission in Education through ICT	5
1.1.1	ICT Initiatives of MoE	6
1.2	FOSSEE Project	7
1.2.1	Projects and Activities	7
1.2.2	Fellowships	7
1.3	Osdag Software	8
1.3.1	Osdag GUI	9
1.3.2	Features	9
2	Report Generation of Welded Plate Girder	10
2.1	Problem Statement	10
2.2	Tasks Done	10
2.2.1	Design Automation Workflow	10
2.2.2	Core Design Functions	10
2.2.3	Report Generation with <code>save_design</code>	11
2.3	Python Code	12
2.3.1	Explanation of the Code	56
2.4	Documentation	57
2.5	References	57
3	Report Generation of Bolted Lap Joint	59
3.1	Problem Statement	59
3.2	Tasks Done	59
3.2.1	Core Save Design Function Development	59
3.2.2	Detailed Design Verification and Check Implementation	61
3.2.3	Advanced LaTeX Mathematical Formatting	62
3.2.4	Design Calculations Integration	62
3.3	Python Code	63
3.3.1	Explanation of the Code	85
3.4	Documentation	87

3.5	References	87
4	Report Generation of Bolted Butt Joint	88
4.1	Problem Statement	88
4.2	Tasks Done	88
4.2.1	Core Save Design Function Development	88
4.2.2	Detailed Design Verification and Check Implementation	90
4.2.3	Advanced LaTeX Mathematical Formatting	91
4.2.4	Design Calculations Integration	92
4.3	Python Code	92
4.3.1	Explanation of the Code	119
4.4	Documentation	120
4.5	References	121
5	Report Generation of Welded Lap Joint	122
5.1	Problem Statement	122
5.2	Tasks Done	122
5.2.1	Development of <code>save_design()</code> Function	122
5.2.2	Check Implementation and Output	123
5.3	Python Code	124
5.3.1	Explanation of the Code	140
5.4	Documentation	141
5.5	References	142
6	Report Generation of Welded Butt Joint	143
6.1	Problem Statement	143
6.2	Tasks Done	143
6.2.1	Design Automation Workflow	143
6.2.2	Core Design Functions	144
6.2.3	Report Generation with <code>save_design</code>	145
6.3	Python Code	146
6.3.1	Explanation of the Code	173
6.4	Documentation	174
6.5	References	175

7	Standardization of Report Generation Infrastructure	176
7.1	Problem Statement	176
7.2	Tasks Done	176
7.2.1	Global Infrastructure Enhancements	176
7.3	Python Code (reportGenerator_latex.py)	177
7.4	Documentation	178
7.5	References	178
8	Conclusions	179
8.1	Tasks Accomplished	179
8.2	Skills Developed	181
A	Appendix	184
A.1	Work Reports	184
	Bibliography	187

Chapter 1

Introduction

1.1 National Mission in Education through ICT

The National Mission on Education through ICT (NMEICT) is a scheme under the Department of Higher Education, Ministry of Education, Government of India. It aims to leverage the potential of ICT to enhance teaching and learning in Higher Education Institutions in an anytime-anywhere mode.

The mission aligns with the three cardinal principles of the Education Policy—**access, equity, and quality**—by:

- Providing connectivity and affordable access devices for learners and institutions.
- Generating high-quality e-content free of cost.

NMEICT seeks to bridge the digital divide by empowering learners and teachers in urban and rural areas, fostering inclusivity in the knowledge economy. Key focus areas include:

- Development of e-learning pedagogies and virtual laboratories.
- Online testing, certification, and mentorship through accessible platforms like EduSAT and DTH.
- Training and empowering teachers to adopt ICT-based teaching methods.

For further details, visit the official website: www.nmeict.ac.in.

1.1.1 ICT Initiatives of MoE

The Ministry of Education (MoE) has launched several ICT initiatives aimed at students, researchers, and institutions. The table below summarizes the key details:

No.	Resource	For Students/Researchers	For Institutions
Audio-Video e-content			
1	SWAYAM	Earn credit via online courses	Develop and host courses; accept credits
2	SWAYAMPBABHA	Access 24x7 TV programs	Enable SWAYAMPBABHA viewing facilities
Digital Content Access			
3	National Digital Library	Access e-content in multiple disciplines	List e-content; form NDL Clubs
4	e-PG Pathshala	Access free books and e-content	Host e-books
5	Shodhganga	Access Indian research theses	List institutional theses
6	e-ShodhSindhu	Access full-text e-resources	Access e-resources for institutions
Hands-on Learning			
7	e-Yantra	Hands-on embedded systems training	Create e-Yantra labs with IIT Bombay
8	FOSSEE	Volunteer for open-source software	Run labs with open-source software
9	Spoken Tutorial	Learn IT skills via tutorials	Provide self-learning IT content
10	Virtual Labs	Perform online experiments	Develop curriculum-based experiments
E-Governance			
11	SAMARTH ERP	Manage student lifecycle digitally	Enable institutional e-governance
Tracking and Research Tools			
12	VIDWAN	Register and access experts	Monitor faculty research outcomes
13	Shodh Shuddhi	Ensure plagiarism-free work	Improve research quality and reputation
14	Academic Bank of Credits	Store and transfer credits	Facilitate credit redemption

Table 1.1: Summary of ICT Initiatives by the Ministry of Education

1.2 FOSSEE Project

The FOSSEE (Free/Libre and Open Source Software for Education) project promotes the use of FLOSS tools in academia and research. It is part of the National Mission on Education through Information and Communication Technology (NMEICT), Ministry of Education (MoE), Government of India.

1.2.1 Projects and Activities

The FOSSEE Project supports the use of various FLOSS tools to enhance education and research. Key activities include:

- **Textbook Companion:** Porting solved examples from textbooks using FLOSS.
- **Lab Migration:** Facilitating the migration of proprietary labs to FLOSS alternatives.
- **Niche Software Activities:** Specialized activities to promote niche software tools.
- **Forums:** Providing a collaborative space for users.
- **Workshops and Conferences:** Organizing events to train and inform users.

1.2.2 Fellowships

FOSSEE offers various internship and fellowship opportunities for students:

- Winter Internship
- Summer Fellowship
- Semester-Long Internship

Students from any degree and academic stage can apply for these internships. Selection is based on the completion of screening tasks involving programming, scientific computing, or data collection that benefit the FLOSS community. These tasks are designed to be completed within a week.

For more details, visit the official FOSSEE website.

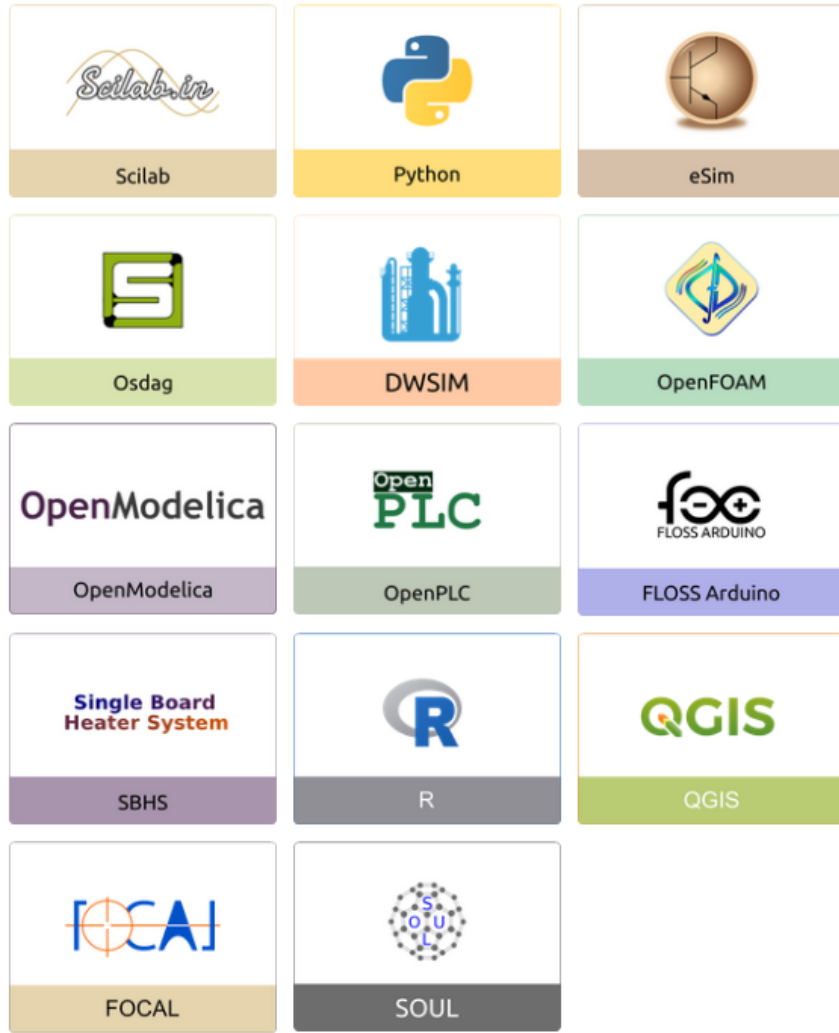


Figure 1.1: FOSSEE Projects and Activities

1.3 Osdag Software

Osdag (Open steel design and graphics) is a cross-platform, free/libre and open-source software designed for the detailing and design of steel structures based on the Indian Standard IS 800:2007. It allows users to design steel connections, members, and systems through an interactive graphical user interface (GUI) and provides 3D visualizations of designed components. The software enables easy export of CAD models to drafting tools for construction/fabrication drawings, with optimized designs following industry best practices [1, 2, 3]. Built on Python and several Python-based FLOSS tools (e.g., PyQt and PythonOCC), Osdag is licensed under the GNU Lesser General Public License (LGPL) Version 3.

1.3.1 Osdag GUI

The Osdag GUI is designed to be user-friendly and interactive. It consists of

- **Input Dock:** Collects and validates user inputs.
- **Output Dock:** Displays design results after validation.
- **CAD Window:** Displays the 3D CAD model, where users can pan, zoom, and rotate the design.
- **Message Log:** Shows errors, warnings, and suggestions based on design checks.

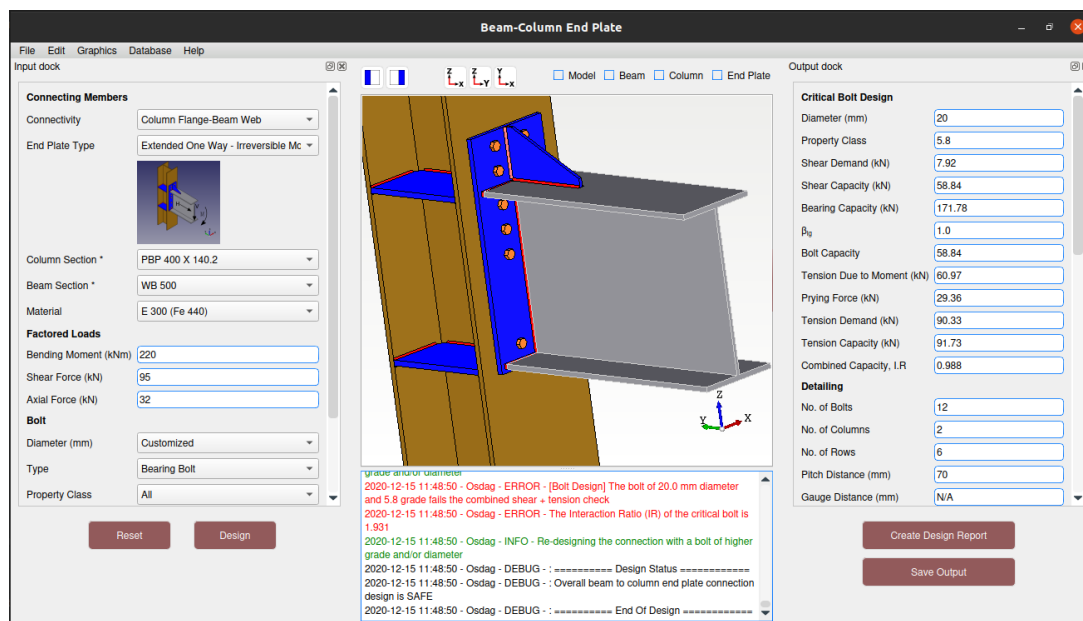


Figure 1.2: Osdag GUI

1.3.2 Features

- **CAD Model:** The 3D CAD model is color-coded and can be saved in multiple formats such as IGS, STL, and STEP.
- **Design Preferences:** Customizes the design process, with advanced users able to set preferences for bolts, welds, and detailing.
- **Design Report:** Creates a detailed report in PDF format, summarizing all checks, calculations, and design details, including any discrepancies.

For more details, visit the official Osdag website.

Chapter 2

Report Generation of Welded Plate Girder

2.1 Problem Statement

The objective of this task was to develop an automated reporting workflow for a **Welded Plate Girder** in Osdag. The module must verify all limit states (shear capacity, moment capacity, web buckling/crippling, deflection, and weld strength) and generate a clear, stepwise LaTeX report for documentation and checking purposes.

2.2 Tasks Done

2.2.1 Design Automation Workflow

- Implemented the `save_design` function to orchestrate the report generation process, gathering all necessary design data from the `PlateGirderWelded` object.
- Developed helper functions `prepare_report_input` and `prepare_design_checks` to organize inputs and calculation steps into a DDCL-compliant structure.

2.2.2 Core Design Functions

- **Initialisation** (`prepare_report_input`): Extracts user inputs and derived section properties (Mass, Area, I_z , I_y , Z_p , Z_e) to populate the report header and “Section

Details” table with accurate, rounded values.

- **Design Checks** (`prepare_design_checks`):
 - **Section Classification:** Added detailed calculation logic to display flange and web outstands and their resulting classification (Plastic, Compact, Semi-compact, or Slender) in the report.
 - **Shear Capacity:** Implemented logic to dynamically display formulas for V_d and V_{cr} based on the chosen web philosophy (“Thick Web”, “Simple Post Critical”, or “Tension Field”).
 - **Moment Capacity:** Added conditional logic to distinguish between Laterally Supported (Yielding governed) and Unsupported (Buckling governed) beams, explicitly writing out steps for M_{cr} , λ_{LT} , χ_{LT} , and f_{bd} .
 - **Stiffener Detailing:** Integrated checks for Stiffener Spacing (c/d ratios), Minimum Inertia (I_s), and Longitudinal Stiffener placement/inertia if required by the aspect ratio d/t_w .
 - **Weld Design:** Included checks for required vs. provided weld sizes for flange-web connections.
 - **Deflection:** Added Actual vs. Allowable deflection checks to the report output.
- **Final Check** (`final_format`): Implemented logic to aggregate utilization ratios (Shear, Moment, Deflection) and determine the overall “PASS/FAIL” status for the report summary.

2.2.3 Report Generation with `save_design`

- The `save_design` function is called irrespective of `design_status` is SAFE or UNSAFE. It gathers all important data (forces, material strengths, plate dimensions, weld size, cover plate type) into a `report_input` dictionary.
- It then constructs a detailed `report_check` list containing:
 - Weld size limits ($s_{\min}$, $s_{\max}$) and pass/fail status,
 - Weld strength calculation with substituted values,

- Base metal capacity in tension or compression,
 - Overall capacity, utilization ratio and final design status.
- Mathematical expressions are wrapped using `NoEscape` so that LaTeX formulas (for example the expression of f_w or P_w) appear correctly in the final PDF.
 - Finally, `CreateLatex.save_latex` is invoked to generate the formatted PDF report, including 2D/3D images and a summary table of all checks.

2.3 Python Code

The entire logic for the report generation of the Plate Girder module is within the `latex_report.py` file. Below are key snippets from the module with explanations of their functionality. Below are key snippets from the module with explanations of their functionality.

Description of the Script

The script defines the `save_design()` function and helper functions `prepare_report_input()` and `prepare_design_checks()`, which handle the translation of the `PlateGirderWelded` object's state into a LaTeX-compatible dictionary and list structure.

Python Code

The following snippets showcase the core logic implemented in the report generation task.

Listing 2.1: Plate Girder `save_design()` function

```

1 %-----begin code-----
2 """
3 Module: latex_report.py
4 Description: DDCL-COMPLIANT Design Report Generator for Plate Girder (
    Updated)
5 Author: Roushan Raj
6 Date: 2026-01-16
7 """
8
9 import logging

```

```

10 from pylatex import Math
11 from pylatex.utils import NoEscape
12 from ....design_report.reportGenerator_latex import CreateLatex
13 from ....Common import KEY_DISP_SEC_PROFILE
14 from ....utils.common.Unsymmetrical_Section_Properties import
    Unsymmetrical_I_Section_Properties
15 import os
16 import math
17 from ..checks.shear import tension_field_unequal_I_corrected, calc_K_v
18 from ....utils.common.is800_2007 import IS800_2007
19
20 def save_design(popup_summary):
21     """Generate LaTeX design report for Plate Girder module"""
22     unique_logger_name = 'Osdag_plate_girder_flexure'
23     logger = logging.getLogger(unique_logger_name)
24     logger.info(" :=====Start of design report generation
        =====")
25
26     try:
27         pg_obj = popup_summary.get('plate_girder_object')
28         if pg_obj is None:
29             logger.error("Plate Girder Object is None")
30             return False
31
32         if not pg_obj.design_status:
33             logger.warning("Design is not complete/failed checks.
                Generating report with failures.")
34
35         report_input = prepare_report_input(pg_obj, logger)
36         report_check = prepare_design_checks(pg_obj, logger)
37
38         # Prepare report summary
39         report_summary = popup_summary.copy()
40         if 'ProfileSummary' not in report_summary:
41             report_summary['ProfileSummary'] = {
42                 'CompanyName': report_summary.get('CompanyName', ''),
43                 'CompanyLogo': report_summary.get('CompanyLogo', ''),
44                 'Group/TeamName': report_summary.get('Group/TeamName',
                    ''),

```

```

45         'Designer': report_summary.get('Designer', '')
46     }
47
48     report_summary.setdefault('ProjectTitle', 'Plate Girder Design'
49                               )
50     report_summary.setdefault('Subtitle', 'Welded Plate Girder')
51     report_summary.setdefault('JobNumber', '')
52     report_summary.setdefault('Client', '')
53     report_summary['does_design_exist'] = pg_obj.design_status
54     report_summary.setdefault('logger_messages', '')
55
56     # Image paths
57     Disp_2d_image = []
58     Disp_3D_image = "/ResourceFiles/images/3d.png"
59     rel_path = os.path.abspath(".").replace("\\", "/")
60     fname_no_ext = popup_summary.get("filename", "
        ButtJointWeldedReport")
61     folder = popup_summary.get('folder', './reports')
62     os.makedirs(folder, exist_ok=True)
63
64     CreateLatex.save_latex(
65         CreateLatex(), report_input, report_check,
66         popup_summary, fname_no_ext, rel_path, Disp_2d_image,
67         Disp_3D_image,
68         module="Plate Girder"
69     )
70     logger.info(f"Report generated successfully: {fname_no_ext}.pdf
71                ")
72
73     pdf_file_path = os.path.join(folder, f"{fname_no_ext}.pdf")
74     if os.path.exists(pdf_file_path):
75         file_size = os.path.getsize(pdf_file_path)
76         print(f"SUCCESS: Report generated: {pdf_file_path} ({
77               file_size} bytes)")
78         return True
79     else:
80         print("ERROR: PDF not found")
81         return False

```

```

79     except Exception as e:
80         logger.error(f"Report generation failed: {str(e)}")
81         return False
82
83
84 def prepare_report_input(pg_obj, logger):
85     """
86     Prepare input section - ONLY user inputs, NO calculations
87     """
88     report_input = {}
89
90     try:
91         report_input['Module'] = 'PLATE GIRDER'
92         report_input['Main Module'] = 'Flexural Member'
93         # ===== 1. General Inputs =====
94         report_input['General Inputs'] = 'TITLE'
95
96         # Material
97         material = getattr(pg_obj, 'material', None)
98         report_input['Material Grade'] = getattr(material, 'designation', 'E 250') if material else 'E 250'
99
100        # Structure Type
101        # Try to get from attributes, fallback to reasonable default if
102        # missing
103        report_input['Type of Structure'] = getattr(pg_obj, 'structure_type', 'Industrial Structure')
104
105        # Torsional Restraint
106        report_input['Torsional Restraint'] = getattr(pg_obj, 'torsional_restraint', 'Fully Restrained')
107
108        # Warping Restraint
109        report_input['Warping Restraint'] = getattr(pg_obj, 'warping_restraint', 'No Restraint')
110
111        # Span
112        report_input['Span (mm)'] = round(getattr(pg_obj, 'length', 0),
113                                           1)

```

```

112
113     if hasattr(pg_obj, 'max_deflection'):
114         report_input['Maximum deflection observed (mm)'] = getattr
            (pg_obj, 'max_deflection', '-')
115
116     # ===== Girder Properties =====
117     girder_props = {}
118     girder_props[KEY_DISP_SEC_PROFILE] = 'ISection'
119
120     # Material Properties
121     if material:
122         girder_props['Material'] = getattr(material, 'designation',
            'E 250')
123         girder_props['Ultimate Strength (MPa)'] = getattr(material,
            'fu', 410)
124         girder_props['Yield Strength (MPa)'] = getattr(material, '
            fy', 250)
125         E = getattr(material, 'modulus_of_elasticity', 200000)
126         girder_props['Modulus of Elasticity (MPa)'] = E
127         mu = getattr(material, 'poisson_ratio', 0.3)
128         girder_props["Poisson's Ratio"] = mu
129         # Calculate G if not present
130         if hasattr(material, 'shear_modulus'):
131             girder_props['Modulus of Rigidity (MPa)'] = getattr(
                material, 'shear_modulus')
132         else:
133             girder_props['Modulus of Rigidity (MPa)'] = round(E /
                (2 * (1 + mu)), 2)
134
135         girder_props['Thermal Expansion'] = getattr(material, '
            coeff_thermal_expansion', 12e-6)
136
137     girder_props['Type'] = 'Welded'
138
139     # Geometry for Calculation
140     D = getattr(pg_obj, 'total_depth', 0)
141     bf_top = getattr(pg_obj, 'top_flange_width', 0)
142     bf_bot = getattr(pg_obj, 'bottom_flange_width', 0)
143     tw = getattr(pg_obj, 'web_thickness', 0)

```

```

144     tf_top = getattr(pg_obj, 'top_flange_thickness', 0)
145     tf_bot = getattr(pg_obj, 'bottom_flange_thickness', 0)
146
147     # Section Properties Calculations
148     girder_props['Mass (kg/m)'] =
149         Unsymmetrical_I_Sections.Properties.calc_mass(D, bf_top,
150             bf_bot, tw, tf_top, tf_bot)
151     girder_props['Area (cm2)'] = round(
152         Unsymmetrical_I_Sections.Properties.calc_area(D, bf_top,
153             bf_bot, tw, tf_top, tf_bot) / 100, 2)
154
155     girder_props['Moment of Area, Iz (cm4)'] = round(
156         Unsymmetrical_I_Sections.Properties.calc_MomentOfAreaZ(D,
157             bf_top, bf_bot, tw, tf_top, tf_bot) / 10000, 2)
158     girder_props['Moment of Area, Iy (cm4)'] = round(
159         Unsymmetrical_I_Sections.Properties.calc_MomentOfAreaY(D,
160             bf_top, bf_bot, tw, tf_top, tf_bot) / 10000, 2)
161
162     girder_props['Radius of Gyration, rz (cm)'] = round(
163         Unsymmetrical_I_Sections.Properties.calc_RadiusOfGyrationZ(D,
164             bf_top, bf_bot, tw, tf_top, tf_bot) / 10, 2)
165     girder_props['Radius of Gyration, ry (cm)'] = round(
166         Unsymmetrical_I_Sections.Properties.calc_RadiusOfGyrationY(D,
167             bf_top, bf_bot, tw, tf_top, tf_bot) / 10, 2)
168
169     girder_props['Elastic Modulus, Zez (cm3)'] = round(
170         Unsymmetrical_I_Sections.Properties.calc_ElasticModulusZz(D,
171             bf_top, bf_bot, tw, tf_top, tf_bot) / 1000, 2)
172     girder_props['Elastic Modulus, Zey (cm3)'] = round(
173         Unsymmetrical_I_Sections.Properties.calc_ElasticModulusZy(D,
174             bf_top, bf_bot, tw, tf_top, tf_bot) / 1000, 2)
175
176     girder_props['Plastic Modulus, Zpz (cm3)'] = round(
177         Unsymmetrical_I_Sections.Properties.calc_PlasticModulusZ(D,
178             bf_top, bf_bot, tw, tf_top, tf_bot) / 1000, 2)
179     girder_props['Plastic Modulus, Zpy (cm3)'] = round(
180         Unsymmetrical_I_Sections.Properties.calc_PlasticModulusY(D,
181             bf_top, bf_bot, tw, tf_top, tf_bot) / 1000, 2)

```

```

163     report_input['Girder Properties'] = girder_props
164
165     # ===== 2. Dimensions Inputs =====
166     report_input['Dimensions Inputs'] = 'TITLE'
167
168     report_input['Top Flange Width (mm)'] = round(getattr(pg_obj, '
169         top_flange_width', 0), 1)
170     report_input['Top Flange Thickness (mm)'] = round(getattr(
171         pg_obj, 'top_flange_thickness', 0), 1)
172     report_input['Bottom Flange Width (mm)'] = round(getattr(pg_obj
173         , 'bottom_flange_width', 0), 1)
174     report_input['Bottom Flange Thickness (mm)'] = round(getattr(
175         pg_obj, 'bottom_flange_thickness', 0), 1)
176     report_input['Depth of Section (mm)'] = round(getattr(pg_obj, '
177         total_depth', 0), 1)
178     report_input['Web Thickness (mm)'] = round(getattr(pg_obj, '
179         web_thickness', 0), 1)
180
181     # ===== 3. Load Inputs =====
182     report_input['Load Inputs'] = 'TITLE'
183
184     load = getattr(pg_obj, 'load', None)
185     if load:
186         report_input['Maximum Bending Moment (kN-m)'] = round(
187             getattr(load, 'moment', 0) * 1e-6, 2)
188         report_input['Maximum Shear Force (kN)'] = round(getattr(
189             load, 'shear_force', 0) * 1e-3, 2)
190     else:
191         report_input['Maximum Bending Moment (kN-m)'] = 0
192         report_input['Maximum Shear Force (kN)'] = 0
193
194     report_input['Bending moment diagram shape'] = getattr(pg_obj,
195         'moment_diagram_type', 'Uniform Loading')
196
197     # ===== 4. Support Condition Inputs =====
198     report_input['Support Condition Inputs'] = 'TITLE'

```

```

191     report_input['Support Condition'] = getattr(pg_obj, '
        support_type', 'Major Laterally Supported')
192     report_input['Bearing length (mm)'] = round(getattr(pg_obj, '
        bearing_length', 0), 1)
193
194     # ===== 5. Web Philosophy Inputs
        =====
195     report_input['Web Philosophy Inputs'] = 'TITLE'
196
197     report_input['Web Type'] = getattr(pg_obj, 'web_philosophy', '
        Thick Web without ITS')
198
199     # Additional Material Details (Standard)
200     if material:
201         report_input['Yield Strength, fy (MPa)'] = round(getattr(
            material, 'fy', 0), 1)
202         report_input['Ultimate Strength, fu (MPa)'] = round(getattr
            (material, 'fu', 0), 1)
203
204     except Exception as e:
205         logger.error(f"Error preparing report input: {str(e)}")
206
207     return report_input
208
209 def prepare_design_checks(pg_obj, logger):
210     """
211     Prepare design checks - DDCL compliant with multi-line equations
212     All equations formatted per lap_joint_bolted.py pattern
213     """
214     report_check = []
215     table_format = '|p{4cm}|p{4.5cm}|p{6cm}|p{1.5cm}|'
216
217     try:
218         # ===== GET VALUES FROM PG_OBJ
            =====
219
220         # Material
221         material = getattr(pg_obj, 'material', None)
222         fy = round(material.fy, 1) if material else 250
223         fu = round(material.fu, 1) if material else 410

```

```

223     E = getattr(material, 'modulus_of_elasticity', 200000) if
        material else 200000
224
225     # Loads
226     load = getattr(pg_obj, 'load', None)
227     M_applied = round(getattr(load, 'moment', 0) * 1e-6, 2) if load
        else 0
228     V_applied = round(getattr(load, 'shear_force', 0) * 1e-3, 2) if
        load else 0
229
230     # Dimensions
231     D = getattr(pg_obj, 'total_depth', 0)
232     d = getattr(pg_obj, 'eff_depth', 0)
233     tw = getattr(pg_obj, 'web_thickness', 0)
234     tf_top = getattr(pg_obj, 'top_flange_thickness', 0)
235     tf_bot = getattr(pg_obj, 'bottom_flange_thickness', 0)
236     bf_top = getattr(pg_obj, 'top_flange_width', 0)
237     bf_bot = getattr(pg_obj, 'bottom_flange_width', 0)
238     L = getattr(pg_obj, 'length', 0)
239
240     # Design parameters
241     gamma_m0 = getattr(pg_obj, 'gamma_m0', 1.1)
242     epsilon = getattr(pg_obj, 'epsilon', 1.0)
243
244     # Design decisions from pg_obj
245     section_class = getattr(pg_obj, 'section_class', None)
246     if section_class is None:
247         section_class = getattr(pg_obj, 'section_classification_val
            ', 'NA')
248
249     design_status = getattr(pg_obj, 'design_status', False)
250     shear_flag1 = getattr(pg_obj, 'shearflag1', False)
251     shear_flag2 = getattr(pg_obj, 'shearflag2', False)
252     shear_flag3 = getattr(pg_obj, 'shearflag3', False)
253     moment_checks = getattr(pg_obj, 'momentchecks', False)
254     defl_check = getattr(pg_obj, 'defl_check', False)
255     web_philosophy = getattr(pg_obj, 'web_philosophy', '')
256
257     # ===== SECTION CLASSIFICATION

```

```

=====
258     report_check.append(['SubSection', 'Section Classification',
259                           table_format])
260
261     # Top flange slenderness
262     if bf_top > 0 and tf_top > 0:
263         btftop = round((bf_top - tw) / (2 * tf_top), 2)
264
265         btftop_eq = Math(inline=True)
266         btftop_eq.append(NoEscape(r'\begin{aligned}\\'))
267         btftop_eq.append(NoEscape(rf'\dfrac{{{b_f} - {t_w}}}{{2 {t_f}}} \&= \
268             \dfrac{{{bf_top:.1f} - {tw:.1f}}}{{2 \times {tf_top:.1f}
269             }}}\\'))
270         btftop_eq.append(NoEscape(rf'\&= {btftop:.2f}\\'))
271         btftop_eq.append(NoEscape(r'\&\text{[Ref: IS 800:2007, Table
272             2]}\\'))
273         btftop_eq.append(NoEscape(r'\end{aligned}'))
274
275     # Determine Class
276     outstand_top = (bf_top - tw) / 2
277     class_top = IS800_2007.Table2_i(outstand_top, tf_top, fy, '
278         Welded')[0]
279
280     report_check.append([
281         'Top Flange Slenderness Ratio',
282         '',
283         btftop_eq,
284         class_top
285     ])
286
287     # Bottom flange slenderness
288     if bf_bot > 0 and tf_bot > 0:
289         btfbot = round((bf_bot - tw) / (2 * tf_bot), 2)
290
291         btfbot_eq = Math(inline=True)
292         btfbot_eq.append(NoEscape(r'\begin{aligned}\\'))
293         btfbot_eq.append(NoEscape(rf'\dfrac{{{b_f} - {t_w}}}{{2 {t_f}}}
294             \&= \dfrac{{{bf_bot:.1f} - {tw:.1f}}}{{2 \times {tf_bot
295             :.1f}}}\&\&\\'))

```

```

289         btf_bot_eq.append(NoEscape(rf'&= {btf_bot:.2f}\\'))
290         btf_bot_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007,
           Table 2]}\\'))
291         btf_bot_eq.append(NoEscape(r'\end{aligned}'))
292
293         # Determine Class
294         outstand_bot = (bf_bot - tw) / 2
295         class_bot = IS800_2007.Table2_i(outstand_bot, tf_bot, fy, '
           Welded')[0]
296
297         report_check.append([
298             'Bottom Flange Slenderness Ratio',
299             '',
300             btf_bot_eq,
301             class_bot
302         ])
303
304         # Web slenderness
305         d_tw_ratio = round(d / tw, 2) if tw > 0 else 0
306
307         dtw_eq = Math(inline=True)
308         dtw_eq.append(NoEscape(r'\begin{aligned}\\'))
309         dtw_eq.append(NoEscape(rf'\dfrac{{{d}}}{{{t_w}}} &= \dfrac{{{d:.1f
           }}} {{{tw:.1f}}} \\'))
310         dtw_eq.append(NoEscape(rf'&= {d_tw_ratio:.2f}\\'))
311         dtw_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Table 2]}\\'
           ))
312         dtw_eq.append(NoEscape(r'\end{aligned}'))
313
314         web_depth = d
315         class_web = IS800_2007.Table2_iii(web_depth, tw, fy)
316
317         report_check.append([
318             'Web Slenderness Ratio',
319             '',
320             dtw_eq,
321             class_web
322         ])
323

```

```

324 # Overall section classification
325 overall_eq = Math(inline=True)
326 overall_eq.append(NoEscape(r'\begin{aligned}\\'))
327 overall_eq.append(NoEscape(r'&\text{Governing classification
      based on}\\'))
328 overall_eq.append(NoEscape(r'&\text{most critical element}\\'))
329 overall_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Table
      2]}\\'))
330 overall_eq.append(NoEscape(r'\end{aligned}'))
331
332 report_check.append([
333     'Overall Section Classification',
334     overall_eq,
335     str(section_class),
336     ''
337 ])
338
339 # ===== SHEAR CAPACITY CHECK
      =====
340 report_check.append(['SubSection', 'Shear Capacity Check',
      table_format])
341
342 V_d_N = getattr(pg_obj, 'V_d', 0)
343 V_d = round(V_d_N / 1000, 2) if V_d_N else 0
344
345 # Shear area
346 Avw = round(d * tw, 2)
347
348 avw_eq = Math(inline=True)
349 avw_eq.append(NoEscape(r'\begin{aligned}\\'))
350 avw_eq.append(NoEscape(rf'A_{vw} &= d \times t_w\\'))
351 avw_eq.append(NoEscape(rf'&= {d:.1f} \times {tw:.1f}\\'))
352 avw_eq.append(NoEscape(rf'&= {Avw:.2f} \text{{ mm}}^2\\'))
353 avw_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Cl.8.4]}\\'))
      )
354 avw_eq.append(NoEscape(r'\end{aligned}'))
355
356 report_check.append([
357     NoEscape(r'Shear Area'),

```

```

358         '' ,
359         avw_eq ,
360         ''
361     ])
362
363     # Design shear strength
364     if web_philosophy == 'Thick Web without ITS':
365         vd_eq = Math(inline=True)
366         vd_eq.append(NoEscape(r'\begin{aligned}\\'))
367         vd_eq.append(NoEscape(r'V_d &= \dfrac{A_{vw} \times f_y}{\sqrt{3} \times \gamma_{m0}}\\'))
368         vd_eq.append(NoEscape(rf'&= \dfrac{{{Avw:.2f}} \times {fy:.1f}}{\sqrt{{{3}}} \times {\gamma_{m0}}}\'))
369         vd_eq.append(NoEscape(rf'&= {V_d:.2f} \text{{ kN}}\'))
370         vd_eq.append(NoEscape(r'\&\text{[Ref: IS 800:2007, Cl .8.4.1]}\'))
371         vd_eq.append(NoEscape(r'\end{aligned}'))
372
373         shear_status = 'Pass' if shear_flag1 else 'Fail'
374
375         report_check.append([
376             NoEscape(r'Design Shear Strength'),
377             f'{V_applied:.2f}',
378             vd_eq,
379             shear_status
380         ])
381     else:
382         # Thin web - Check if Tension Field or Simple Post Critical
383         shear_method = getattr(pg_obj, 'x', 'Simple Post Critical')
384
385         # Common parameters for both methods
386         d_eff = getattr(pg_obj, 'eff_depth', 0)
387         c_val = getattr(pg_obj, 'c', 0)
388         if c_val == 'NA': c_val = 0
389
390         kv = calc_K_v(c_val, d_eff, web_philosophy)
391
392         kv_nm = 5.35
393         kv_m = 4.0

```

```

394     a_ratio = c_val / d_eff if d_eff != 0 else 0
395
396     kv_calc_eq = Math(inline=True)
397     kv_calc_eq.append(NoEscape(r'\begin{aligned}\\'))
398     kv_calc_eq.append(NoEscape(rf'\dfrac{{{c}}}{{{d}}} &= \dfrac{{{
399         c_val:.1f}}}{{{{d_eff:.1f}}}} = {a_ratio:.2f}\\\\'))
400
401     if a_ratio < 1.0:
402         kv_calc_eq.append(NoEscape(r'k_v &= 4.0 + \dfrac
403             {5.35}{(c/d)^2}\\\\'))
404         kv_calc_eq.append(NoEscape(rf'&= 4.0 + \dfrac
405             {{{5.35}}}{{{{(a_ratio:.2f)}}^2}} = {kv:.3f}\\\\'))
406     else:
407         kv_calc_eq.append(NoEscape(r'k_v &= 5.35 + \dfrac
408             {4.0}{(c/d)^2}\\\\'))
409         kv_calc_eq.append(NoEscape(rf'&= 5.35 + \dfrac
410             {{{4.0}}}{{{{(a_ratio:.2f)}}^2}} = {kv:.3f}\\\\'))
411
412     kv_calc_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Cl
413         .8.4.2.2]}\\\\'))
414     kv_calc_eq.append(NoEscape(r'\end{aligned}'))
415
416     report_check.append([
417         NoEscape(r'Buckling Coefficient'),
418         '',
419         kv_calc_eq,
420         ''
421     ])
422
423     # Calculate Tau_crc, Lambda_w, Tau_b generically first
424     # using IS800 module logic
425     # (replicating shear.py logic for consistency)
426     mu = 0.3
427     tau_crc = IS800_2007.cl_8_4_2_2_tau_crc_Simple_postcritical
428         (kv, E, mu, d_eff, tw)
429     lambda_w = IS800_2007.
430         cl_8_4_2_2_lambda_w_Simple_postcritical(fy, tau_crc)
431     tau_b = IS800_2007.cl_8_4_2_2_tau_b_Simple_postcritical(
432         lambda_w, fy)

```

```

423
424     # Display Lambda_w
425     lambda_eq = Math(inline=True)
426     lambda_eq.append(NoEscape(r'\begin{aligned}\\'))
427     lambda_eq.append(NoEscape(r'\lambda_w \;=\; \sqrt{\dfrac{f_{yw}}{3}} \tau_{cr,e}}\\'))
428     lambda_eq.append(NoEscape(rf'\;=\; \sqrt{{\dfrac{{{fy:.2f}}{3}} \times {\tau_{cr,e}:.2f}}}}\\'))
429     lambda_eq.append(NoEscape(rf'\;=\; {\lambda_w:.3f}\\'))
430     lambda_eq.append(NoEscape(r'\&\text{[Ref: IS 800:2007, Cl .8.4.2.2]}\\'))
431     lambda_eq.append(NoEscape(r'\end{aligned}'))
432
433     report_check.append([
434         NoEscape(r'Web Slenderness'),
435         '',
436         lambda_eq,
437         ''
438     ])
439
440     if lambda_w <= 0.8:
441         tau_b = round(fy / (3*0.5), 2)
442         tau_b_eq = Math(inline=True)
443         tau_b_eq.append(NoEscape(r'\begin{aligned}\\'))
444         tau_b_eq.append(NoEscape(rf'\lambda_w \leq 0.8: \quad \tau_b \;=\; \dfrac{f_{yw}}{3} \sqrt{3}}\\'))
445         tau_b_eq.append(NoEscape(rf'\;=\; \dfrac{{{fy:.1f}}{\sqrt{3}}}}\\'))
446         tau_b_eq.append(NoEscape(rf'\;=\; {\tau_b:.2f} \text{ MPa}}\\'))
447         tau_b_eq.append(NoEscape(r'\&\text{[Ref: IS 800:2007, Cl .8.4.2.2, Eq. 1.21]}\\'))
448         tau_b_eq.append(NoEscape(r'\end{aligned}'))
449     elif 0.8 < lambda_w < 1.2:
450         tau_b = round((1 - 0.8 * (lambda_w - 0.8)) * (fy / (3*0.5)), 2)
451         tau_b_eq = Math(inline=True)
452         tau_b_eq.append(NoEscape(r'\begin{aligned}\\'))
453         tau_b_eq.append(NoEscape(r'0.8 < \lambda_w < 1.2: \quad

```

```

        \tau_b \&= [1 - 0.8(\lambda_w - 0.8)]\dfrac{f_{yw}}{\sqrt{3}}\\\\')
454 tau_b_eq.append(NoEscape(rf'\&= [1 - 0.8({lambda_w:.3f}
    - 0.8)] \times \dfrac{{{fy:.1f}}}{{\sqrt{3}}}}\\\\')
    ))
455 tau_b_eq.append(NoEscape(rf'\&= {\tau_b:.2f} \text{{ MPa
    }}\\\\'))
456 tau_b_eq.append(NoEscape(r'\&\text{{[Ref: IS 800:2007, Cl
    .8.4.2.2, Eq. 1.21]}}\\'))
457 tau_b_eq.append(NoEscape(r'\end{aligned}'))
458 else:
459 tau_b = round(fy / (3*0.5 * lambda_w), 2)
460 tau_b_eq = Math(inline=True)
461 tau_b_eq.append(NoEscape(r'\begin{aligned}\\\\'))
462 tau_b_eq.append(NoEscape(r'\lambda_w \geq 1.2: \quad \
    \tau_b \&= \dfrac{f_{yw}}{\sqrt{3}\lambda_w}\\\\'))
463 tau_b_eq.append(NoEscape(rf'\&= \dfrac{{{fy:.1f}}}{{\
    \sqrt{3}} \times {\lambda_w:.3f}}}}\\\\'))
464 tau_b_eq.append(NoEscape(rf'\&= {\tau_b:.2f} \text{{ MPa
    }}\\\\'))
465 tau_b_eq.append(NoEscape(r'\&\text{{[Ref: IS 800:2007, Cl
    .8.4.2.2]}}\\'))
466 tau_b_eq.append(NoEscape(r'\end{aligned}'))
467
468 report_check.append([
469     'Design Shear Stress',
470     '',
471     tau_b_eq,
472     ''
473 ])
474
475 V_cr_val = round(Avw * tau_b / 1000, 2)
476
477 Vcr_eq = Math(inline=True)
478 Vcr_eq.append(NoEscape(r'\begin{aligned}\\\\'))
479 Vcr_eq.append(NoEscape(r'V_{cr} \&= A_{vw} \times \tau_b\\\\
    '))
480 Vcr_eq.append(NoEscape(rf'\&= {Avw:.2f} \times {\tau_b:.2f
    }}\\\\'))

```

```

481     Vcr_eq.append(NoEscape(rf'&= {V_cr_val:.2f} \text{{ kN
      }}\\\\'))
482     Vcr_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Cl
      .8.4.2.1]}\\\\'))
483     Vcr_eq.append(NoEscape(r'\end{aligned}'))
484
485     report_check.append([
486         'Shear Buckling Resistance',
487         '',
488         Vcr_eq,
489         ''
490     ])
491
492     if shear_method == 'Tension Field Action':
493         # --- TENSION FIELD ACTION REPORTING ---
494
495         # Recalculate Tension Field parameters
496         V_cr = IS800_2007.cl_8_4_2_2_Vcr_Simple_postcritical(
497             tau_b, Avw)
498
499         # We need M_applied (calculated/user) but for
500         # calculation of N_f, shear.py uses load.moment (N-mm)
501         # Ensure units are correct. M_applied earlier is in kNm
502         .
503         # tension_field_unequal_I_corrected expects M in N-mm
504         M_design_Nmm = M_applied * 1e6
505
506         Nf_val = M_design_Nmm / (d_eff + (tf_top + tf_bot) / 2)
507
508         phi, Mfr_t, Mfr_b, s_t, s_b, w_tf, psi, fv, V_tf_val =
509         tension_field_unequal_I_corrected(
510             c_val, d_eff, tw, fy, bf_top, tf_top, bf_bot,
511             tf_bot, Nf_val, gamma_m0, Avw, tau_b
512         )
513
514         V_tf_final = round(V_tf_val / 1000, 2)
515
516         # 1. Tension Field Angle (phi) - DDCL Eq 1.29
517         phi_eq = Math(inline=True)

```

```

513 phi_eq.append(NoEscape(r'\begin{aligned}\\'))
514 phi_eq.append(NoEscape(r'\phi \;=\; \tan^{-1} \left( \right. \left. \frac{d}{c} \right)\\\\'))
515 phi_eq.append(NoEscape(rf'\;=\; \tan^{{-1}} \left( \frac{{{d_eff:.1f}}}{{{c_val:.1f}}} \right)\\\\'))
516 phi_eq.append(NoEscape(rf'\;=\; {\phi:.2f}^\circ\\'))
517 phi_eq.append(NoEscape(r'\text{[Ref: IS 800:2007, C1.8.4.2.a]}\\'))
518 phi_eq.append(NoEscape(r'\end{aligned}'))
519
520 report_check.append([
521     NoEscape(r'Tension Field Angle'),
522     '',
523     phi_eq,
524     '',
525 ])
526
527 # 2. Width of Tension Field (w_tf) - DDCL Eq 1.30
528 # w_tf = d*cos(phi) + (c - sc - st)*sin(phi)
529 # Note: 'sc' in code is 's_b' (anchor length bottom/
530 # compression?) or s_t/s_b generically
531 # The function returns s_t (top) and s_b (bottom). DDCL
532 # uses sc and st.
533 # Just show the formula with values.
534
535 wtf_eq = Math(inline=True)
536 wtf_eq.append(NoEscape(r'\begin{aligned}\\'))
537 wtf_eq.append(NoEscape(r'w_{tf} \;=\; d \cos \phi + (c - s_c - s_t) \sin \phi\\\\'))
538 wtf_eq.append(NoEscape(rf'\;=\; {d_eff:.1f} \cos({\phi:.2f}) + ({c_val:.1f} - {s_b:.1f} - {s_t:.1f}) \sin({\phi:.2f})\\\\'))
539 wtf_eq.append(NoEscape(rf'\;=\; {w_tf:.2f} \text{[ mm]}\\'))
540 wtf_eq.append(NoEscape(r'\text{[Ref: IS 800:2007, C1.8.4.2.a]}\\'))
541 wtf_eq.append(NoEscape(r'\end{aligned}'))
542
543 report_check.append([

```

```

542         NoEscape(r'Width of Tension Field'),
543         '',
544         wtf_eq,
545         ''
546     ])
547
548     # 3. Yield Strength of Tension Field (fv) - DDCL Eq
549         1.31
550     # fv = sqrt(fy^2 - 3*tau_b^2 + psi^2) - psi
551     # psi = 1.5 * tau_b * sin(2phi)
552
553     fv_eq = Math(inline=True)
554     fv_eq.append(NoEscape(r'\begin{aligned}'))
555     fv_eq.append(NoEscape(r'\psi &= 1.5 \tau_b \sin(2\phi)'))
556     fv_eq.append(NoEscape(rf'&= 1.5 \times {\tau_b:.2f} \times \sin(2 \times {\phi:.2f}) = {\psi:.2f}'))
557     fv_eq.append(NoEscape(rf'&= \sqrt{{fy:.1f}^2 - 3({\tau_b:.2f})^2 + ({\psi:.2f})^2} - {\psi:.2f}'))
558     fv_eq.append(NoEscape(rf'&= {fv:.2f} \text{{ MPa}}'))
559     fv_eq.append(NoEscape(r'&\text{{[Ref: IS 800:2007, Cl 8.4.2.2a]}}'))
560     fv_eq.append(NoEscape(r'\end{aligned}'))
561
562     report_check.append([
563         NoEscape(r'Yield Strength of Web'),
564         '',
565         fv_eq,
566         ''
567     ])
568
569     # 4. Design Shear Strength (V_tf) - DDCL Eq 1.28
570     vtf_eq = Math(inline=True)
571     vtf_eq.append(NoEscape(r'\begin{aligned}'))
572     vtf_eq.append(NoEscape(r'V_{tf} &= A_{vm} \tau_b + 0.9 w_{tf} t_w f_v \sin \phi')) # A_vm typically A_w
573     vtf_eq.append(NoEscape(rf'&= {Avw:.2f} \times {\tau_b:.2f}'))

```

```

        f} + 0.9 \times {w_tf:.2f} \times {tw:.1f} \times {
        fv:.2f} \times \sin({phi:.2f})\\\\'))
574     vtf_eq.append(NoEscape(rf'&= {V_tf_final:.2f} \text{{
        kN}}\\\\'))
575     vtf_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, C1
        .8.4.2.2a]}\\\\'))
576     vtf_eq.append(NoEscape(r'\end{aligned}'))
577
578     shear_status = 'Pass' if shear_flag1 else 'Fail'
579
580     report_check.append([
581         NoEscape(r'Design Shear Strength'),
582         f'{V_applied:.2f}', # Applied Load
583         vtf_eq,
584         shear_status
585     ])
586
587     # Web crippling
588     if hasattr(pg_obj, 'F_q') and pg_obj.F_q not in [None, 'NA',
589     0]:
589         Fq = round(pg_obj.F_q / 1000, 2)
590         b1 = getattr(pg_obj, 'b1', 0)
591         bearing_note = ""
592         if b1 <= 0 or b1 < pg_obj.web_thickness * 2:
593             bearing_note = " (min. assumed)"
594
595         fq_eq = Math(inline=True)
596         fq_eq.append(NoEscape(r'\begin{aligned}\\\\'))
597
598         # Calculate n2 for display purpose if not explicitly
599         # available, based on Fq equation
600         # Fq = (b1 + n2) * tw * fy / gamma_m0
601         # (b1 + n2) = Fq * gamma_m0 / (tw * fy)
602         # n2 = [Fq * 1000 * gamma_m0 / (tw * fy)] - b1
603         # Note: Fq in pg_obj is in N. b1 in mm.
604
605         n2_disp = 0
606         if tw > 0 and fy > 0:
607             try:

```

```

607         n2_disp = (pg_obj.F_q * gamma_m0) / (tw * fy) - b1
608         except Exception:
609             n2_disp = 0
610
611         fq_eq.append(NoEscape(r'F_q &= \dfrac{(b_1 + n_2) t_w f_y
612             }\{\gamma_{m0}\}\\\'))
613         fq_eq.append(NoEscape(rf'&= \dfrac{{{b1:.1f} + {n2_disp:.1
614             f}} \times {tw:.1f} \times {fy:.1f}}{\{\gamma_{m0}\}}\\'))
615         fq_eq.append(NoEscape(rf'&= {Fq:.2f} \text{{ kN}}\\'))
616         fq_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Cl
617             .8.7.1.1]}\\'))
618         fq_eq.append(NoEscape(r'\end{aligned}'))
619
620         fq_status = 'Pass' if shear_flag3 else 'Fail'
621
622         report_check.append([
623             NoEscape(r'Web Crippling Strength'),
624             '',
625             fq_eq,
626             fq_status
627         ])
628
629         # ===== MOMENT CAPACITY CHECK
630         =====
631         report_check.append(['SubSection', 'Moment Capacity Check',
632             table_format])
633
634         # READ Md from pg_obj
635         Md_val = getattr(pg_obj, 'Md', 0)
636         Md = round(Md_val * 1e-6, 2) if Md_val and Md_val > 0 else 0
637
638         Zp_val = getattr(pg_obj, 'plast_sec_mod_z', 0)
639         Zp = round(Zp_val * 1e-3, 2) if Zp_val and Zp_val > 0 else 0
640
641         Ze_val = getattr(pg_obj, 'elast_sec_mod_z', 0)
642         Ze = round(Ze_val * 1e-3, 2) if Ze_val and Ze_val > 0 else 0
643
644         beta_b_val = getattr(pg_obj, 'betab', 1.0)

```

```

640     beta_b = round(beta_b_val, 3) if beta_b_val else 1.0
641
642     if section_class in ['Plastic', 'Compact']:
643         Z_used = Zp
644         Z_label = 'Z_p'
645     else:
646         Z_used = Ze
647         Z_label = 'Z_e'
648
649     # Beta_b
650     beta_eq = Math(inline=True)
651     beta_eq.append(NoEscape(r'\begin{aligned}'))
652     beta_eq.append(NoEscape(rf'\beta_b &= {\beta_b:.2f}'))
653     beta_eq.append(NoEscape(r'\end{aligned}'))
654
655     report_check.append([
656         NoEscape(r'Betab Factor'),
657         '',
658         beta_eq,
659         ''
660     ])
661
662     # Design moment capacity
663     md_eq = Math(inline=True)
664     md_eq.append(NoEscape(r'\begin{aligned}'))
665
666     support_type = getattr(pg_obj, 'support_type', '')
667     if support_type == 'Major Laterally Unsupported':
668         md_eq.append(NoEscape(r'M_d &= \beta_b Z_p f_{bd}'))
669         md_eq.append(NoEscape(rf'&= {\beta_b} \times {Z_used:.2f} \times f_{bd}'))
670     else:
671         md_eq.append(NoEscape(r'M_d &= \dfrac{\beta_b Z_p f_y}{\gamma_{m0}}'))
672         md_eq.append(NoEscape(rf'&= \dfrac{{\beta_b} \times {Z_used:.2f} \times {f_y}}{{\gamma_{m0}}}))
673
674     md_eq.append(NoEscape(rf'&= {Md:.2f} \text{{ kN-m}}'))
675

```

```

676     if support_type == 'Major Laterally Unsupported':
677         md_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Cl
        .8.2.2]}\'))
678     else:
679         md_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Cl
        .8.2.1]}\'))
680
681     md_eq.append(NoEscape(r'\end{aligned}'))
682
683     moment_status = 'Pass' if moment_checks else 'Fail'
684
685     report_check.append([
686         NoEscape(r'Design Moment Capacity'),
687         NoEscape(rf'{M_applied:.2f}\text{{ kN-m}}'),
688         md_eq,
689         moment_status
690     ])
691
692     # ===== LATERAL TORSIONAL BUCKLING
        =====
693     support_type = getattr(pg_obj, 'support_type', '')
694     if support_type in ['Major Laterally Unsupported', 'Minor
        Laterally Unsupported']:
695         report_check.append(['SubSection', 'Lateral Torsional
        Buckling Check', table_format])
696
697         L_eff = getattr(pg_obj, 'effective_length', 0)
698         Mcr_val = getattr(pg_obj, 'M_cr', 0)
699         Mcr = round(Mcr_val * 1e-6, 2) if Mcr_val and Mcr_val > 0
            else 'NA'
700         lambda_LT = round(getattr(pg_obj, 'lambda_lt', 0), 3) if
            hasattr(pg_obj, 'lambda_lt') else 'NA'
701         chi_LT = round(getattr(pg_obj, 'X_lt', 1.0), 3) if hasattr(
            pg_obj, 'X_lt') else 'NA'
702         fbd = round(getattr(pg_obj, 'fbd_lt', 0), 2) if hasattr(
            pg_obj, 'fbd_lt') else 'NA'
703
704         # Effective length
705         leff_eq = Math(inline=True)

```

```

706         leff_eq.append(NoEscape(r'\begin{aligned}\\'))
707         leff_eq.append(NoEscape(rf'L_{{LT}} \&= {L_eff:.1f} \text{{
708             mm}}\\'))
709         leff_eq.append(NoEscape(r'\&\text{[Ref: IS 800:2007, Table
710             14]}\\'))
711         leff_eq.append(NoEscape(r'\end{aligned}'))
712
713     report_check.append([
714         NoEscape(r'Effective Length'),
715         '',
716         leff_eq,
717         ''
718     ])
719
720     # Critical moment
721     if Mcr != 'NA':
722         # Calculate properties for Mcr breakdown
723         try:
724             Iy = Unsymmetrical_I_Section_Properties.
725                 calc_MomentOfAreaY(D, bf_top, bf_bot, tw, tf_top
726                     , tf_bot)
727             # Mcr,z (Euler) in kNm
728             #  $M_{cr,z} = (\pi^2 * E * I_y) / L_{LT}^2$ 
729             if L_eff > 0:
730                 Mcr_z_Nmm = (math.pi**2 * E * Iy) / (L_eff**2)
731                 Mcr_z = Mcr_z_Nmm * 1e-6
732             else:
733                 Mcr_z = 0
734
735             # Back-calculate Mcr,T ->  $M_{cr} = \sqrt{M_{cr,z} * M_{cr,T}}$ 
736             =>  $M_{cr,T} = M_{cr}^2 / M_{cr,z}$ 
737             if Mcr_z > 0:
738                 Mcr_T = (Mcr)**2 / Mcr_z
739             else:
740                 Mcr_T = 0
741         except Exception as m_e:
742             # Fallback if calc fails
743             Mcr_z = 0
744             Mcr_T = 0

```

```

740 mcr_eq = Math(inline=True)
741 mcr_eq.append(NoEscape(r'\begin{aligned}\\'))
742 mcr_eq.append(NoEscape(r'M_{cr} \&= \sqrt{M_{cr,z} \times M_{cr,T}}\\'))
743 if Mcr_z > 0 and Mcr_T > 0:
744     mcr_eq.append(NoEscape(rf'\&= \sqrt{{{Mcr_z:.2f} \times {Mcr_T:.2f}}}\'))
745 mcr_eq.append(NoEscape(rf'\&= {Mcr:.2f} \text{{ kN-m}}\'))
746 mcr_eq.append(NoEscape(r'\&\text{[Ref: IS 800:2007, Annex E]}\'))
747 mcr_eq.append(NoEscape(r'\end{aligned}'))
748
749 report_check.append([
750     NoEscape(r'Elastic Critical Moment'),
751     '',
752     mcr_eq,
753     '',
754 ])
755
756
757 # Lambda_LT
758 if lambda_LT != 'NA':
759     lambda_eq = Math(inline=True)
760     lambda_eq.append(NoEscape(r'\begin{aligned}\\'))
761     lambda_eq.append(NoEscape(rf'\lambda_{{LT}} \&= {lambda_LT:.3f}\'))
762     lambda_eq.append(NoEscape(r'\&\text{[Ref: IS 800:2007, C1.8.2.2]}\'))
763     lambda_eq.append(NoEscape(r'\end{aligned}'))
764
765     report_check.append([
766         NoEscape(r'Slenderness Ratio'),
767         '',
768         lambda_eq,
769         '',
770     ])
771
772 # f_bd

```

```

773         if fbd != 'NA' and chi_LT != 'NA':
774             fbd_eq = Math(inline=True)
775             fbd_eq.append(NoEscape(r'\begin{aligned}\\'))
776             fbd_eq.append(NoEscape(r'f_{bd} \dfrac{\chi_{LT} \backslash
              times f_y}{\gamma_{m0}}\\'))
777             fbd_eq.append(NoEscape(rf'\dfrac{{{chi_LT:.3f}} \backslash
              times {fy}} {{{gamma_m0}}}\\\'))
778             fbd_eq.append(NoEscape(rf'\dfrac{{{fbd:.2f}}}{\text{MPa}}\\'))
779             fbd_eq.append(NoEscape(r'\text{[Ref: IS 800:2007, Cl
              .8.2.2]}\\'))
780             fbd_eq.append(NoEscape(r'\end{aligned}'))
781
782         report_check.append([
783             NoEscape(r'Design Bending Strength'),
784             '',
785             fbd_eq,
786             ''
787         ])
788
789         # ===== DEFLECTION CHECK =====
790         report_check.append(['SubSection', 'Deflection Check',
              table_format])
791
792         defl_val = getattr(pg_obj, 'deflection_criteria', 600)
793         try:
794             defl_limit_ratio = float(defl_val)
795             if defl_limit_ratio <= 0:
796                 defl_limit_ratio = 600
797         except (ValueError, TypeError):
798             defl_limit_ratio = 600
799
800         if L > 0:
801
802             # Allowable deflection
803             delta_allow = round(L / defl_limit_ratio, 2)
804
805             allow_eq = Math(inline=True)
806             allow_eq.append(NoEscape(r'\begin{aligned}\\'))

```

```

807     allow_eq.append(NoEscape(rf'\delta_{{allow}} &= \dfrac{{L
      }}{{{{defl_limit_ratio}}}}\\\\'))
808     allow_eq.append(NoEscape(rf'&= \dfrac{{{{L:.1f}}}}{{{{
      defl_limit_ratio}}}}\\\\'))
809     allow_eq.append(NoEscape(rf'&= {delta_allow:.2f} \text{{ mm
      }}\\\\'))
810     allow_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Table
      6]}\\\\'))
811     allow_eq.append(NoEscape(r'\end{aligned}'))
812
813     report_check.append([
814         NoEscape(r'Allowable Deflection'),
815         '',
816         allow_eq,
817         ''
818     ])
819
820     # Actual deflection
821     delta_actual_str = getattr(pg_obj, 'calculated_deflection',
      'NA')
822     if delta_actual_str not in ['NA', 'Skipped']:
823         try:
824             delta_actual = round(float(delta_actual_str), 2)
825
826             # Calculate Iz for formula display
827             try:
828                 Iz_mm4 = Unsymmetrical_I_Section_Properties.
      calc_MomentOfAreaZ(
829                     D, bf_top, bf_bot, tw, tf_top, tf_bot
830                 )
831             except:
832                 Iz_mm4 = 1
833
834             # Calculate w (N/mm) from M_applied (kNm) assuming
      UDL
835             # M = w L^2 / 8 => w = 8 M / L^2
836             if L > 0:
837                 M_Nmm = M_applied * 1e6
838                 w_udl = 8 * M_Nmm / (L**2)

```

```

839         else:
840             w_udl = 0
841
842             actual_eq = Math(inline=True)
843             actual_eq.append(NoEscape(r'\begin{aligned}'))
844             actual_eq.append(NoEscape(r'\delta &= \dfrac{5 w L^4}{384 E I_z}'))
845             actual_eq.append(NoEscape(rf'\delta &= \dfrac{5 \times {w_udl:.2f} \times {L:.1f}^4}{384 \times {E} \times {Iz_mm4:.2e}}'))
846             actual_eq.append(NoEscape(rf'\delta &= {delta_actual:.2f} \text{{ mm}}'))
847             actual_eq.append(NoEscape(r'\text{[Ref: IS 800:2007, Table 6]}'))
848             actual_eq.append(NoEscape(r'\end{aligned}'))
849
850             defl_status = 'Pass' if defl_check else 'Fail'
851             report_check.append([
852                 'Actual Deflection',
853                 NoEscape(rf'{delta_allow:.2f} \text{{ mm}}'),
854                 actual_eq,
855                 defl_status
856             ])
857         except (ValueError, TypeError):
858             pass
859
860         # ===== WELD DESIGN =====
861         report_check.append(['SubSection', 'Weld Design', table_format
862                               ])
863
864         weld_top = getattr(pg_obj, 'atop', 0)
865         weld_bot = getattr(pg_obj, 'abot', 0)
866         t_min = min(tw, tf_top, tf_bot) if tw > 0 and tf_top > 0 and
867             tf_bot > 0 else 0
868         weld_stiff = getattr(pg_obj, 'weld_stiff', None)
869
870         # Minimum weld size per IS 800:2007 Table 21
871         if t_min < 10:
872             s_min = 3

```

```

871     elif t_min <= 20:
872         s_min = 5
873     else:
874         s_min = 6
875
876     minweld_eq = Math(inline=True)
877     minweld_eq.append(NoEscape(r'\begin{aligned}\\'))
878     minweld_eq.append(NoEscape(rf'\text{{Thinner plate}} &= {t_min}
879         :.1f} \text{{ mm}}'))
880     minweld_eq.append(NoEscape(r'\text{[Ref: IS 800:2007, Table
881         21]}\\'))
882     minweld_eq.append(NoEscape(r'\end{aligned}'))
883
884     report_check.append([
885         'Minimum Weld Size',
886         '',
887         NoEscape(rf'{round(s_min, 1):.1f}\text{{ mm}}'),
888         ''
889     ])
890
891     # Weld sizes - design outputs
892     if weld_top > 0:
893         wtop_eq = Math(inline=True)
894         wtop_eq.append(NoEscape(r'\begin{aligned}\\'))
895         wtop_eq.append(NoEscape(rf's_{{top}} &= {round(weld_top, 1)}
896             :.1f} \text{{ mm}}\\'))
897         wtop_eq.append(NoEscape(r'\end{aligned}'))
898
899         report_check.append([
900             'Weld Size - Web to Top Flange',
901             '',
902             NoEscape(rf'{round(weld_top, 1):.1f} \text{{ mm}}'),
903             ''
904         ])
905
906     if weld_bot > 0:
907         wbot_eq = Math(inline=True)
908         wbot_eq.append(NoEscape(r'\begin{aligned}\\'))
909         wbot_eq.append(NoEscape(rf's_{{bot}} &= {round(weld_bot, 1)}

```

```

907         :.1f} \text{{ mm}}\\')
908
909     report_check.append([
910         'Weld Size - Web to Bottom Flange',
911         '',
912         NoEscape(rf'{round(weld_bot, 1):.1f} \text{{ mm}}'),
913         ''
914     ])
915
916     if weld_stiff and weld_stiff not in [None, 'NA', 0, '']:
917         weld_stiff_val = float(weld_stiff)
918         if weld_stiff_val > 0:
919             wstiff_eq = Math(inline=True)
920             wstiff_eq.append(NoEscape(r'\begin{aligned}'))
921             wstiff_eq.append(NoEscape(rf's_{{stiff}} &= {round(
922                 weld_stiff_val, 1):.1f} \text{{ mm}}'))
923             wstiff_eq.append(NoEscape(r'\end{aligned}'))
924
925             report_check.append([
926                 'Weld Size - Stiffener to Web',
927                 '',
928                 NoEscape(rf'{round(weld_stiff_val, 1):.1f} \text{{
929                     mm}}'),
930                 ''
931             ])
932
933
934     # ===== INTERMEDIATE STIFFENER - SECTION 1.5.1
935     # =====
936     report_check.append(['SubSection', 'Intermediate Stiffener',
937         table_format])
938
939     c = getattr(pg_obj, 'c', 0)
940
941     if d > 0:
942         c_d_ratio = round(c / d, 3)

```

```

941     sqrt_2 = 1.414
942
943     if c_d_ratio >= sqrt_2:
944         I_s_min = round(0.75 * d * (tw**3), 2)
945
946         I_s_eq = Math(inline=True)
947         I_s_eq.append(NoEscape(r'\begin{aligned}\\'))
948         I_s_eq.append(NoEscape(rf'\text{{Since }} \dfrac{{c}}{{d}} \&= {c_d_ratio:.3f} \geq \sqrt{{2}}\\\\'))
949         I_s_eq.append(NoEscape(r'I_s \&\geq 0.75 \, d \, t_w^3\\\\'))
950         I_s_eq.append(NoEscape(rf'\&\geq 0.75 \times {d:.1f} \times ({tw:.1f})^3\\\\'))
951         I_s_eq.append(NoEscape(rf'\&\geq {I_s_min:.2f} \text{{mm}}^4\\\\'))
952         I_s_eq.append(NoEscape(r'\&\text{{[Ref: IS 800:2007, Cl .8.7.1.2, Eq. 1.17]}}\\\\'))
953         I_s_eq.append(NoEscape(r'\end{aligned}'))
954     else:
955         # condition_status = rf'Since \dfrac{{c}}{{d}} = {c_d_ratio:.3f} < \sqrt{{2}}'
956         I_s_min = round((1.5 * (d**3) * (tw**3)) / (c**2), 2)
957
958         I_s_eq = Math(inline=True)
959         I_s_eq.append(NoEscape(r'\begin{aligned}\\'))
960         I_s_eq.append(NoEscape(rf'\text{{Since }} \dfrac{{c}}{{d}} \&= {c_d_ratio:.3f} < \sqrt{{2}}\\\\'))
961         I_s_eq.append(NoEscape(r'I_s \&\geq 1.5 \, \dfrac{d^3 t_w^3}{c^2}\\\\'))
962         I_s_eq.append(NoEscape(rf'\&\geq 1.5 \times \dfrac{({d:.1f})^3 \times ({tw:.1f})^3}{({c:.1f})^2}\\\\'))
963         I_s_eq.append(NoEscape(rf'\&\geq {I_s_min:.2f} \text{{mm}}^4\\\\'))
964         I_s_eq.append(NoEscape(r'\&\text{{[Ref: IS 800:2007, Cl .8.7.1.2, Eq. 1.18]}}\\\\'))
965         I_s_eq.append(NoEscape(r'\end{aligned}'))
966
967     report_check.append([
968         'Minimum Moment of Inertia',

```

```

969         '' ,
970         I_s_eq ,
971         ''
972     ])
973
974     mu = 0.3
975     tau_crc = round((kv * (3.14159**2) * E) / (12 * (1 - mu**2)
976                 * ((d/tw)**2)), 2)
977
978     tau_crc_eq = Math(inline=True)
979     tau_crc_eq.append(NoEscape(r'\begin{aligned}\\'))
980     tau_crc_eq.append(NoEscape(r'\tau_{cr,e} &= \dfrac{K_v \pi
981                 ^2 E}{12(1-\mu^2)(d/t_w)^2}\\'))
982     tau_crc_eq.append(NoEscape(rf'&= \dfrac{{{kv:.3f}} \times \pi
983                 ^2 \times {E}}{12(1-{\mu}^2)({d:.1f}/{tw:.1f})
984                 ^2}\\'))
985     tau_crc_eq.append(NoEscape(rf'&= {tau_crc:.2f} \text{{ MPa
986                 }}\\'))
987     tau_crc_eq.append(NoEscape(r'&\text{{[Ref: IS 800:2007, Cl
988                 .8.4.2.2, Eq. 1.23]}}\\'))
989     tau_crc_eq.append(NoEscape(r'\end{aligned}'))
990
991     report_check.append([
992         'Critical Buckling Stres',
993         NoEscape(rf'\mu = {mu}$'),
994         tau_crc_eq,
995         ''
996     ])
997
998     # ===== END PANEL STIFFENER - SECTION 1.5.2
999     =====
1000
1001     report_check.append(['SubSection', 'End Panel Stiffener',
1002         table_format])
1003
1004     # Vertical Anchor Force
1005     Vp = round((d * tw * fy) / (3**0.5), 2)
1006     Vp_kN = round(Vp / 1000, 2)

```

```

1000 Vp_eq = Math(inline=True)
1001 Vp_eq.append(NoEscape(r'\begin{aligned}\\'))
1002 Vp_eq.append(NoEscape(r'V_p &= \dfrac{d \cdot t_w \cdot f_y}{\sqrt{3}}\\'))
1003 Vp_eq.append(NoEscape(r'&= \dfrac{{{d:.1f}} \times {tw:.1f} \times {fy:.1f}}{{\sqrt{{3}}}}}\\'))
1004 Vp_eq.append(NoEscape(r'&= {Vp_kN:.2f} \text{{ kN}}\\'))
1005 Vp_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Cl .8.4.2.2]}\\'))
1006 Vp_eq.append(NoEscape(r'\end{aligned}'))
1007
1008 report_check.append([
1009     'Vertical Anchor Force',
1010     '',
1011     Vp_eq,
1012     ''
1013 ])
1014
1015 # Tension Flange Reaction
1016 Rtf = round(Vp_kN / 2, 2)
1017
1018 Rtf_eq = Math(inline=True)
1019 Rtf_eq.append(NoEscape(r'\begin{aligned}\\'))
1020 Rtf_eq.append(NoEscape(r'R_{tf} &= \dfrac{V_p}{2}\\'))
1021 Rtf_eq.append(NoEscape(r'&= \dfrac{{{Vp_kN:.2f}}}{{2}}\\'))
1022 Rtf_eq.append(NoEscape(r'&= {Rtf:.2f} \text{{ kN}}\\'))
1023 Rtf_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Cl .8.4.2.2]}\\'))
1024 Rtf_eq.append(NoEscape(r'\end{aligned}'))
1025
1026 report_check.append([
1027     'Tension Flange Reaction',
1028     '',
1029     Rtf_eq,
1030     ''
1031 ])
1032
1033 # Tension Flange Moment
1034 Mtf = round(Vp_kN * d / 10, 2)

```

```

1035
1036 Mtf_eq = Math(inline=True)
1037 Mtf_eq.append(NoEscape(r'\begin{aligned}\\'))
1038 Mtf_eq.append(NoEscape(r'M_{tf} &= \dfrac{V_p \cdot d}{10}\\\\'
1039 ))
1040 Mtf_eq.append(NoEscape(rf'&= \dfrac{{{Vp_kN:.2f}} \times {d:.1f}
1041 }}{{10}}\\\\'))
1042 Mtf_eq.append(NoEscape(rf'&= {Mtf:.2f} \text{{ kN-mm}}\\\\'))
1043 Mtf_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Cl
1044 .8.4.2.2]}\\\\'))
1045 Mtf_eq.append(NoEscape(r'\end{aligned}'))
1046
1047 report_check.append([
1048     'Tension Flange Moment',
1049     '',
1050     Mtf_eq,
1051     ''
1052 ])
1053
1054 if web_philosophy != "Thick Web without ITS":
1055     # Calculate end panel stiffener thickness based on tension
1056     # flange reaction
1057     Vp = (d * tw * fy) / math.sqrt(3)
1058     Rtf = Vp / 2 # Tension flange reaction
1059
1060     # Design stiffener for Rtf
1061     # Assume stiffener is a pair on both sides of web
1062     endstiffwidth = getattr(pg_obj, 'end_stiffwidth', 0)
1063     stiff_width = endstiffwidth
1064
1065     # Required thickness based on bearing stress
1066     # _bearing = Rtf / (2 * stiff_width * t_stiff) * fy /
1067     # m0
1068     # Solving for t_stiff: t_stiff = (Rtf * m0) / (2
1069     # * stiff_width * fy)
1070
1071     if stiff_width > 0:
1072         t_req = (Rtf * gamma_m0) / (2 * stiff_width * fy)

```

```

1068         # Use thickness from pg_obj if available (Optimization
           source of truth)
1069         t_provided_obj = getattr(pg_obj, 'end_stiffthickness',
           0)
1070
1071         if t_provided_obj and t_provided_obj > 0:
1072             pg_obj.endstiffthickness = float(t_provided_obj)
1073         else:
1074             # Fallback design logic if not provided
1075             available_thk = [8, 10, 12, 16, 20, 25, 32, 40, 50]
1076
1077             endstiffthickness = None
1078             for thk in available_thk:
1079                 if float(thk) >= t_req:
1080                     pg_obj.endstiffthickness = float(thk)
1081                     break
1082
1083             if pg_obj.endstiffthickness is None:
1084                 pg_obj.endstiffthickness = float(available_thk
           [-1]) # Use maximum if all fail
1085                 logger.warning(f"End stiffener thickness {
           pg_obj.endstiffthickness}mm may be
           insufficient")
1086         else:
1087             pg_obj.endstiffthickness = 50.0
1088
1089         pg_obj.endpanelstiffenerthickness = pg_obj.
           endstiffthickness
1090         logger.info(f"End Panel Stiffener Thickness: {pg_obj.
           endpanelstiffenerthickness} mm")
1091     else:
1092         # Thick web without stiffeners
1093         pg_obj.endpanelstiffenerthickness = "NA"
1094         pg_obj.endstiffthickness = 0
1095
1096         # ===== LONGITUDINAL STIFFENER - SECTION 1.5.3
           =====
1097         report_check.append(['SubSection', 'Longitudinal Stiffener',
           table_format])

```

```

1098
1099     # Calculate epsilon and limits
1100     epsilon_w = round((250 / fy)**0.5, 3)
1101     limit_200_eps = round(200 * epsilon_w, 2)
1102     limit_250_eps = round(250 * epsilon_w, 2)
1103     limit_400_eps = round(400 * epsilon_w, 2)
1104
1105     d_tw_ratio = round(d / tw, 2)
1106
1107     # Row 1: Web Thickness Limits (Check for Longitudinal Stiffener
1108         Requirement)
1109     req_check_eq = Math(inline=True)
1110     req_check_eq.append(NoEscape(r'\begin{aligned}\\'))
1111     req_check_eq.append(NoEscape(rf'1.&\text{{Transverse Stiffeners
1112         only: }}\\'))
1113     req_check_eq.append(NoEscape((rf'&\dfrac{{{d}}}{{{t_w}}} \leq 200 \
1114         epsilon_w = {limit_200_eps:.2f}\\\\'))))
1115     req_check_eq.append(NoEscape(rf'2.&\text{{With 1st Longitudinal
1116         Stiffener: }}\\'))
1117     req_check_eq.append(NoEscape(rf'&\dfrac{{{d}}}{{{t_w}}} \leq 250 \
1118         epsilon_w = {limit_250_eps:.2f}\\\\'))
1119     req_check_eq.append(NoEscape(rf'3.&\text{{With 2nd Longitudinal
1120         Stiffener: }}\\'))
1121     req_check_eq.append(NoEscape(rf'&\dfrac{{{d}}}{{{t_w}}} \leq 400 \
1122         epsilon_w = {limit_400_eps:.2f}\\\\'))
1123     req_check_eq.append(NoEscape(rf'4.&\text{{Actual Web
1124         Slenderness: }}\\\\'))
1125     req_check_eq.append(NoEscape(rf'&\dfrac{{{d}}}{{{t_w}}} = {
1126         d_tw_ratio:.2f}\\\\'))
1127
1128     long_stiff_required = False
1129     second_stiff_required = False
1130
1131     if d_tw_ratio <= limit_200_eps:
1132         req_check_eq.append(NoEscape(rf'&\text{{Since }} {
1133             d_tw_ratio:.2f} \leq {limit_200_eps:.2f}, \text{{ Limit
1134             Satsified.}}\\\\'))
1135         req_check_eq.append(NoEscape(r'&\text{{Longitudinal
1136             Stiffeners NOT Required.}}\\'))

```

```

1125         req_check_eq.append(NoEscape(r'\end{aligned}'))
1126
1127         report_check.append([
1128             'Web Thickness Limits',
1129             '',
1130             req_check_eq,
1131             ''
1132         ])
1133
1134         # Add placeholder rows for consistency
1135         report_check.append(['First Stiffener Placement', '', 'Not
1136             Required', ''])
1137         report_check.append(['First Stiffener - Moment of Inertia',
1138             '', 'Not Required', ''])
1139         report_check.append(['Second Stiffener (Neutral Axis)', '',
1140             'Not Required', ''])
1141
1142     else:
1143         long_stiff_required = True
1144         req_check_eq.append(NoEscape(rf'&\text{{Since }} {
1145             d_tw_ratio:.2f} > {limit_200_eps:.2f}, \text{{ Limit
1146             NOT Satsified.}}\\\\'))
1147         req_check_eq.append(NoEscape(r'&\text{{Longitudinal
1148             Stiffeners REQUIRED.}}\\\\'))
1149         req_check_eq.append(NoEscape(r'\end{aligned}'))
1150
1151         report_check.append([
1152             'Web Thickness Limits',
1153             '',
1154             req_check_eq,
1155             ''
1156         ])
1157
1158         # First Stiffener Placement
1159         y_comp = round((D - tf_top - tf_bot) / 5, 2)
1160
1161         y_comp_eq = Math(inline=True)
1162         y_comp_eq.append(NoEscape(r'\begin{aligned}'))
1163         y_comp_eq.append(NoEscape(r'y &= \dfrac{1}{5}(D - t_f -

```

```

t_f)\\\\'))
1158 y_comp_eq.append(NoEscape(rf'&= \dfrac{{1}}{{5}}({D:.1f} -
      {tf_top:.1f} - {tf_bot:.1f})\\\\'))
1159 y_comp_eq.append(NoEscape(rf'&= {y_comp:.2f} \text{{ mm
      }}\\\\'))
1160 y_comp_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Cl
      .8.7.1.3]}\\\\'))
1161 y_comp_eq.append(NoEscape(r'\end{aligned}'))
1162
1163 report_check.append([
1164     'First Stiffener Placement',
1165     'Distance from compression flange',
1166     y_comp_eq,
1167     ''
1168 ])
1169
1170 # First Stiffener Design (Is_1 calculation)
1171 Is_1 = round(4 * c * (tw**3), 2)
1172
1173 Is1_eq = Math(inline=True)
1174 Is1_eq.append(NoEscape(r'\begin{aligned}\\\\'))
1175 Is1_eq.append(NoEscape(r'I_s &\geq 4 c t_w^3\\\\'))
1176 Is1_eq.append(NoEscape(rf'&\geq 4 \times {c:.1f} \times ({
      tw:.1f})^3\\\\'))
1177 Is1_eq.append(NoEscape(rf'&\geq {Is_1:.2f} \text{{ mm
      }}^4\\\\'))
1178 Is1_eq.append(NoEscape(r'&\text{[Ref: IS 800:2007, Cl
      .8.7.2.4]}\\\\'))
1179 Is1_eq.append(NoEscape(r'\end{aligned}'))
1180
1181 report_check.append([
1182     'First Stiffener - Moment of Inertia',
1183     '',
1184     Is1_eq,
1185     ''
1186 ])
1187
1188 # Check for Second Stiffener Requirement
1189 Is2_check_eq = Math(inline=True)

```

```

1190 Is2_check_eq.append(NoEscape(r'\begin{aligned}\\'))
1191 Is2_check_eq.append(NoEscape(r'\text{Limit for single
      longitudinal stiffener:}\\\\'))
1192 Is2_check_eq.append(NoEscape(rf'\dfrac{{{d}}}{{{t_w}}} \leq
      250 \epsilon_w = {limit_250_eps:.2f}\\\\'))
1193 Is2_check_eq.append(NoEscape(r'\text{Actual Web
      Slenderness:}\\\\'))
1194 Is2_check_eq.append(NoEscape(rf'\dfrac{{{d}}}{{{t_w}}} \leq {
      d_tw_ratio:.2f}\\\\'))
1195
1196 if d_tw_ratio > limit_250_eps:
1197     second_stiff_required = True
1198     Is2_check_eq.append(NoEscape(rf'\text{{Since }} {
      d_tw_ratio:.2f} > {limit_250_eps:.2f}, \text{{
      Limit NOT Satsified.}}\\\\'))
1199     Is2_check_eq.append(NoEscape(r'\text{Second Stiffener
      at N.A. REQUIRED.}\\'))
1200
1201     # Add 2nd stiffener calculation to the same block or
1202     next
1203     d_2 = round(D - tf_top - tf_bot, 2)
1204     Is_2 = round(d_2 * (tw**3), 2)
1205     Is2_check_eq.append(NoEscape(r'I_s \geq d_2 \times
      t_w^3\\\\'))
1206     Is2_check_eq.append(NoEscape(rf'\geq {d_2:.2f} \times
      ({tw:.1f})^3\\\\'))
1207     Is2_check_eq.append(NoEscape(rf'\geq {Is_2:.2f} \text
      {{ mm}}^4\\\\'))
1208     Is2_check_eq.append(NoEscape(r'\&\text{[Ref: IS
      800:2007, Cl.8.7.13.2, Eq. 1.42]}\\'))
1209     Is2_check_eq.append(NoEscape(r'\end{aligned}'))
1210
1211     report_check.append([
1212         'Second Stiffener (Neutral Axis)',
1213         '',
1214         Is2_check_eq,
1215         ''
1216     ])

```

```

1217         Is2_check_eq.append(NoEscape(rf'\text{{Since }} {
            d_tw_ratio:.2f} \leq {limit_250_eps:.2f}, \text{{
            Limit Satsified.}}\\\\'))
1218         Is2_check_eq.append(NoEscape(r'\text{NOT Required.}\\\\'
            ))
1219         Is2_check_eq.append(NoEscape(r'\end{aligned}'))
1220
1221         report_check.append([
1222             'Second Stiffener (Neutral Axis)',
1223             '',
1224             Is2_check_eq,
1225             ''
1226         ])
1227
1228
1229         # ===== STIFFENER DESIGN SUMMARY
            =====
1230         report_check.append(['SubSection', 'Stiffener Design Summary',
            table_format])
1231
1232         # Get all stiffener parameters from pg_obj
1233         t_int_stiff = getattr(pg_obj, 'IntStiffThickness', 0)
1234         t_end_stiff = getattr(pg_obj, 'endstiffthickness', 0)
1235
1236         # Determine Longitudinal Stiffener values based on requirement
1237         if long_stiff_required:
1238             t_long_stiff = getattr(pg_obj, 'longstiffenerthk', 'NA')
1239             num_long = getattr(pg_obj, 'longstiffenerno', 'Not Required
                ')
1240             stiff_1_pos = getattr(pg_obj, 'x1', 'Not Required')
1241             stiff_2_pos = getattr(pg_obj, 'x2', 'Not Required')
1242         else:
1243             t_long_stiff = 'Not Required'
1244             num_long = 'Not Required'
1245             stiff_1_pos = 'Not Required'
1246             stiff_2_pos = 'Not Required'
1247
1248         method_name = getattr(pg_obj, 'x', 'Simple Post Critical')
1249         int_spacing = getattr(pg_obj, 'c', 0)

```

```

1250
1251     # Calculate number of end panel stiffeners
1252     if isinstance(t_end_stiff, (int, float)) and t_end_stiff > 0:
1253         num_end = "2 (Pair)"
1254     else:
1255         num_end = "0"
1256
1257     summary_data = [
1258         ['Method', str(method_name)],
1259         ['End Panel Stiffener Thickness (mm)', f'{t_int_stiff:.1f}'
1260          if isinstance(t_int_stiff, (int, float)) else str(
1261              t_int_stiff)],
1262         ['Number of End Panel Stiffeners', num_end],
1263         ['Intermediate Stiffener Thickness (mm)', f'{t_int_stiff:.1f}'
1264          if isinstance(t_int_stiff, (int, float)) else str(
1265              t_int_stiff)],
1266         ['Intermediate Stiffener Spacing (mm)', f'{int_spacing:.1f}'
1267          if isinstance(int_spacing, (int, float)) else str(
1268              int_spacing)],
1269         ['Longitudinal Stiffener Thickness (mm)', f'{t_long_stiff:.1f}'
1270          if isinstance(t_long_stiff, (int, float)) else str(
1271              t_long_stiff)],
1272         ['Number of Longitudinal Stiffeners', str(num_long)],
1273         ['Stiffener 1 Pos. from Comp. Flange (mm)', f'{stiff_1_pos:.2f}'
1274          if isinstance(stiff_1_pos, (int, float)) else str(
1275              stiff_1_pos)],
1276         ['Stiffener 2 Pos. from Comp. Flange (mm)', f'{stiff_2_pos:.2f}'
1277          if isinstance(stiff_2_pos, (int, float)) else str(
1278              stiff_2_pos)]
1279     ]
1280
1281     # Create formatted table
1282     for item in summary_data:
1283         param_name = item[0]
1284         param_value = item[1]
1285
1286         summary_eq = Math(inline=True)
1287         summary_eq.append(NoEscape(r'\begin{aligned}\'))
1288         summary_eq.append(NoEscape(rf'\text{{{param_value}}}\'))

```

```

1277         summary_eq.append(NoEscape(r'\end{aligned}'))
1278
1279         report_check.append([
1280             param_name,
1281             ', ',
1282             summary_eq,
1283             ', ',
1284         ])
1285
1286
1287         # ===== OVERALL DESIGN CHECK
1288         # =====
1289
1290         report_check.append(['SubSection', 'Overall Design Check',
1291                             table_format])
1292
1293         # READ utilization ratios from pg_obj
1294
1295         ur_moment = round(getattr(pg_obj, 'moment_ratio', 0), 3)
1296         ur_shear = round(getattr(pg_obj, 'shear_ratio', 0), 3)
1297         ur_deflection = round(getattr(pg_obj, 'deflection_ratio', 0),
1298                                3)
1299
1300         # Moment utilization - show calculation
1301
1302         moment_ur_eq = Math(inline=True)
1303         moment_ur_eq.append(NoEscape(r'\begin{aligned}'))
1304         moment_ur_eq.append(NoEscape(r'UR_M \&= \dfrac{M_{applied}}{M_d}'))
1305         if Md > 0:
1306             moment_ur_eq.append(NoEscape(rf'\&= \dfrac{{{M_applied:.2f}}}{{{{Md:.2f}}}}'))
1307             moment_ur_eq.append(NoEscape(rf'\&= {ur_moment:.3f}'))
1308             moment_ur_eq.append(NoEscape(r'\end{aligned}'))
1309
1310         report_check.append([
1311             'Moment Utilization Ratio',
1312             moment_ur_eq,
1313             f'{ur_moment:.3f}',
1314             ', ',
1315         ])

```

```

1311     # Shear utilization - show calculation
1312     shear_ur_eq = Math(inline=True)
1313     shear_ur_eq.append(NoEscape(r'\begin{aligned}\\'))
1314     shear_ur_eq.append(NoEscape(r'UR_V \&= \dfrac{V_{\text{applied}}}{V_d} \\'))
1315     if V_d > 0:
1316         shear_ur_eq.append(NoEscape(rf'\&= \dfrac{{{V_applied:.2f}}}{{{V_d:.2f}}}\'))
1317     shear_ur_eq.append(NoEscape(rf'\&= {ur_shear:.3f}\'))
1318     shear_ur_eq.append(NoEscape(r'\end{aligned}'))
1319
1320     report_check.append([
1321         'Shear Utilization Ratio',
1322         shear_ur_eq,
1323         f'{ur_shear:.3f}',
1324         ''
1325     ])
1326
1327     # Deflection utilization - show calculation if applicable
1328     if ur_deflection > 0:
1329         delta_actual_str = getattr(pg_obj, 'calculated_deflection',
1330                                     'NA')
1331         if delta_actual_str not in ['NA', 'Skipped']:
1332             try:
1333                 delta_actual = round(float(delta_actual_str), 2)
1334                 delta_allow = round(L / defl_limit_ratio, 2)
1335
1336                 defl_ur_eq = Math(inline=True)
1337                 defl_ur_eq.append(NoEscape(r'\begin{aligned}\\'))
1338                 defl_ur_eq.append(NoEscape(r'UR_{\delta} \&= \dfrac{\delta_{\text{actual}}}{\delta_{\text{allowable}}}\'))
1339                 if delta_allow > 0:
1340                     defl_ur_eq.append(NoEscape(rf'\&= \dfrac{{{delta_actual:.2f}}}{{{delta_allow:.2f}}}\'))
1341                 defl_ur_eq.append(NoEscape(rf'\&= {ur_deflection:.3f}\'))
1342                 defl_ur_eq.append(NoEscape(r'\end{aligned}'))

```

```

1343         report_check.append([
1344             'Deflection Utilization Ratio',
1345             defl_ur_eq,
1346             f'{ur_deflection:.3f}',
1347             ''
1348         ])
1349     except (ValueError, TypeError):
1350         pass
1351
1352     # Overall design status - calculate and display
1353     overall_ur = max(ur_moment, ur_shear, ur_deflection)
1354
1355     overall_eq = Math(inline=True)
1356     overall_eq.append(NoEscape(r'\begin{aligned}\\'))
1357     overall_eq.append(NoEscape(r'UR_{overall} &= \max(UR_M, UR_V, \\
1358         UR_{\delta})\\\\'))
1359     overall_eq.append(NoEscape(rf'&= \max({ur_moment:.3f}, {\\
1360         ur_shear:.3f}, {ur_deflection:.3f})\\\\'))
1361     overall_eq.append(NoEscape(rf'&= {round(overall_ur, 3):.3f}\\'))
1362     overall_eq.append(NoEscape(r'\end{aligned}'))
1363
1364     final_status = 'Pass' if design_status else 'Fail'
1365
1366     ur_text = "< 1" if overall_ur < 1 else "> 1"
1367     report_check.append([
1368         'Overall Design Status',
1369         overall_eq,
1370         NoEscape(rf'{round(overall_ur, 3):.3f}\text{{ {ur_text}}}')
1371         ,
1372         final_status
1373     ])
1374
1375     logger.info("DDCL-compliant design checks prepared successfully")
1376
1377 except Exception as e:
1378     logger.error(f"Error preparing design checks: {str(e)}")
1379 import traceback

```

```

1377         logger.error(f"Traceback: {traceback.format_exc()}")
1378
1379     return report_check
1380 %----- end code -----

```

2.3.1 Explanation of the Code

The `save_design` logic in `latex_report.py` is structured to handle the complexity of Plate Girder design, which includes multiple branching paths (Supported vs. Unsupported, Thick vs. Thin Web). Its main steps are:

1. **Data Extraction (prepare_report_input):** A comprehensive dictionary is built containing all user inputs and derived section properties (Mass, Area, I_z , I_y , etc.). This ensures the report header and "Section Details" table are populated with accurate, rounded values.
2. **Dynamic Check Generation (prepare_design_checks):** Unlike simpler modules, the checks here are highly conditional:
 - **Shear Path:** The code checks `web_philosophy` (Thick vs. Thin). If "Thin Web", it further branches to display "Simple Post Critical" or "Tension Field" calculations, showing specific formulas for τ_b , λ_w , or tension field angle ϕ and width w_{tf} .
 - **Moment Path:** It distinguishes between Laterally Supported (Yielding governed) and Unsupported (Buckling governed). For the latter, it explicitly writes out the M_{cr} , λ_{LT} , χ_{LT} , and f_{bd} calculation steps using `pylatex` Math objects.
 - **Stiffener Detailing:** It conditionally adds checks for Stiffener Spacing (c/d ratios), Minimum Inertia ($I_s \geq 1.5d^3t^3/c^2$), and Longitudinal Stiffener placement/inertia if required by the aspect ratio d/t_w .
3. **Formatting LaTeX Equations:** Complex formulas such as the Tension Field strength are constructed dynamically. The code substitutes the calculated values (e.g., substituting $\phi=34.5$) into the LaTeX string before rendering, providing a "transparent" calculation report.

4. **Overall Utilization and Status:** The final utilization ratio is derived as the maximum of Shear, Moment, and Deflection ratios. A final "PASS/FAIL" status is determined, and the appropriate summary (Safe/Unsafe) is flagged for the PDF generation.
5. **File Handling and PDF Generation:** Finally, the function sets up the output directory (creating it if required), and calls the common `CreateLatex.save_latex` routine. This compiles the LaTeX file into a professional PDF report that includes input summary, detailed calculation steps, design check table and conclusion for the welded butt joint.

2.4 Documentation

The directory structure used for the Report Generation is organized as follows:

```
src/osdag_core

design_report/
    reportGenerator_latex.py

design_type/
    plate_girder/
        report/
            |      latex_report.py
Report_functions.py
```

Program Start Calls The main entry point for the program is `osdag_gui`. To start the program, open the Osdag folder and start the terminal with that path, execute the following command from the project root:

```
$ python -m osdag_gui
```

2.5 References

- Osdag Github repository: <https://osdag.github.io/>

- IS 800:2007, "General Construction in Steel Code of Practice of Practice"

Chapter 3

Report Generation of Bolted Lap Joint

3.1 Problem Statement

The primary objective of this task was to generate a comprehensive design report for **Bolted Lap Joint Connections**. Osdag (Open Steel Design and Graphics) is an open-source tool designed for the design and detailing of steel structures in accordance with Indian Standards. A critical requirement for steel structures is ensuring they pass all Design and Detailing Checklists (DDCL) to guarantee durability, and such comprehensive design reports provide this essential information. The challenge involved meticulously converting all necessary steps, formulas, and compliance checks stipulated by IS 800:2007 into code to ensure successful report generation for bolted connections.

3.2 Tasks Done

3.2.1 Core Save Design Function Development

- **Implemented comprehensive `save_design()` function in `lap_joint_bolted.py` with robust error handling and validation**

Developed the main orchestrating function that serves as the entry point for

report generation. This function coordinates data collection from the UI, validates all design parameters (such as plate thickness, bolt grade, and load values), performs calculations, and triggers the LaTeX report compilation. It includes comprehensive error handling to manage exceptions during file operations and data processing.

– **Integrated with existing Osdag LaTeX report infrastructure using `CreateLatex` class**

Successfully interfaced the new bolted lap joint module with Osdag’s established LaTeX report generation framework. This required constructing a detailed `report_input` dictionary and a structured `report_check` list to pass data dynamically to the `CreateLatex.save_latex` method, ensuring consistency with other connection modules.

– **Implemented proper file path handling with OS-independent path management**

Coded cross-platform file path management using Python’s `os.path` module to ensure the report generation works seamlessly across different operating systems. The function automatically handles directory creation for reports if they do not exist.

– **Report Input Dictionary Structure**

Architected a complete data structure that captures every piece of information needed for report generation, including:

- * Module identification (Lap Joint Bolted Connection)
- * Material properties (Ultimate and Yield stress)
- * Geometric parameters (Plate thicknesses, width)
- * Bolt specifics (Diameter, Grade, Type - Friction/Bearing)
- * Load information (Tensile/Compression Force)

3.2.2 Detailed Design Verification and Check Implementation

Bolt Capacity Checks

- **Implemented Bolt Shear and Bearing calculations**

Coded the mathematical logic for determining bolt capacity based on IS 800:2007 requirements [Cl. 10.3.3, 10.3.4]. The function dynamically calculates capacity based on the bolt type (Bearing or Friction Grip).

Shear Capacity:

$$V_{dsb} = \frac{f_{ub} \times A_{sb}}{\gamma_{mb}} \quad (3.1)$$

Bearing Capacity:

$$V_{dpb} = \frac{2.5 \times k_b \times d \times t \times f_u}{\gamma_{mb}} \quad (3.2)$$

- **Bolt Design Capacity Logic**

Implemented logic to determine the governing bolt value (V_{db}) by taking the minimum of shear and bearing capacities for bearing bolts, or slip resistance for friction bolts.

Base Metal Strength Analysis

- **Implemented dual strength checks (Yielding and Rupture)**

Developed parallel calculation paths for both failure modes in tension member design [Cl. 6.2, 6.3]:

Gross Yielding:

$$T_{dg} = \frac{A_g \times f_y}{\gamma_{m0}} \quad (3.3)$$

Net Rupture:

$$T_{dn} = \frac{0.9 \times A_n \times f_u}{\gamma_{m1}} \quad (3.4)$$

- **Compression Capacity Check**

Added conditional logic to handle compression loads [Cl. 7.1.2], ensuring the

report adapts dynamically to the `design_for` parameter:

$$P_d = \frac{A_g \times f_y}{\gamma_{m0}} \quad (3.5)$$

3.2.3 Advanced LaTeX Mathematical Formatting

Mathematical Equation Integration

- **Used NoEscape LaTeX formatting for complex mathematical expressions**

Mastered the `pylatex.utils.NoEscape` functionality to render complex mathematical equations without Python string escaping issues. This was crucial for rendering fractions, subscripts, and Greek letters (e.g., γ_{mb} , π) correctly in the final PDF.

- **Dynamic Equation Generation**

Implemented formatted strings (f-strings) within the LaTeX code to inject calculated Python variables (like `bolt_shear_kN`, `kb`, `An`) directly into the equation display strings. This ensures the report shows the actual numerical substitution steps, not just the final result.

3.2.4 Design Calculations Integration

Utilization Ratio and Detailing

- **Calculated Utilization Ratio (UR)**

Implemented a tracking system to calculate the utilization ratio for both the bolts and the base metal. The code identifies the critical UR to determine the overall safety of the connection:

$$UR = \frac{\text{Applied Force}}{\text{Design Capacity}} \quad (3.6)$$

- **Detailing Requirements Implementation**

Implemented practical construction detailing checks as per IS 800:2007 [Cl. 10.2], verifying:

- * Minimum Pitch and Gauge ($2.5 \times d$)
- * Minimum and Maximum Edge Distances

The `save_design` function automatically verifies if provided spacing (p_{prov}, e_{prov}) meets the calculated limits (p_{min}, e_{min}) and reports a "PASS" or "FAIL" status in the final document.

3.3 Python Code

The entire logic for the report generation of Welded Butt Joint module is within the `save_design()` function. And it's being connected to the main GUI through `ui_template.py` and `ui_popup_summary.py` files. Below are key snippets from the module with explanations of their functionality.

Description of the Script

The script defines the `save_design()` function, which handles everything from user input to final design report generation. It uses `reportGenerator_latex.py` to manage properties and perform calculations.

Python Code

The following snippets showcase the core logic implemented in the report generation task.

Listing 3.1: Bolted Lap Joint `save_design()` function

```

1 %-----begin code-----
2 def save_design(self, popup_summary):
3     """
4     Generate the LaTeX design report for Lap Joint Bolted
5     Connection (Tension/Compression)
6     per IS 800:2007.
7     """
8     try:
9         def g(attr, default=None):
10             v = getattr(self, attr, default)

```

```

10         return default if v is None else v
11
12     def f2(x, default=0.0):
13         try:
14             return round(float(x), 2)
15         except (TypeError, ValueError):
16             return default
17
18     def as_int(x, default=0):
19         try:
20             return int(round(float(x)))
21         except (TypeError, ValueError):
22             return default
23
24     if not getattr(self, 'design_status', False):
25         self.report_input = {
26             KEY_MODULE: "Lap Joint Bolted Connection",
27             KEY_MAIN_MODULE: "Plate(d) Connection",
28             "Design Status": "TITLE",
29             "Status": "Design not completed successfully.",
30         }
31         self.report_check = []
32         self.report_check.append([
33             "SubSection", "Design Status", "|p{4cm}|p{5cm}|
34             p{5.5cm}|p{1.5cm}|"
35         ])
36         self.report_check.append(["Design", "Design not
37             completed successfully.", "", "FAIL"])
38
39         Disp_2d_image = []
40         Disp_3D_image = "/ResourceFiles/images/3d.png"
41         rel_path = os.path.abspath(".").replace("\\", "/")
42         fname_no_ext = popup_summary.get("filename", "
43             LapJointBoltedReport")
44         folder = popup_summary.get('folder', './reports')
45         os.makedirs(folder, exist_ok=True)
46
47         CreateLatex.save_latex(
48             CreateLatex(), self.report_input, self.

```

```

        report_check,
46        popup_summary, fname_no_ext, rel_path,
        Disp_2d_image, Disp_3D_image,
47        module=getattr(self, 'module', 'Lap Joint
        Bolted')
48    )
49    return True
50
51    self.module = g('module', 'Lap Joint Bolted')
52    self.mainmodule = 'Plate(d) Connection'
53    design_for = str(g('design_for', 'Tension')).strip()
54    is_comp = design_for.lower().startswith('c')
55
56    plate1_thk = f2(g('plate1thk', g('pltthk', 0.0)), 0.0)
57    plate2_thk = f2(g('plate2thk', g('pltthk', 0.0)), 0.0)
58    width = f2(g('width', 0.0), 0.0)
59    axial_kN = f2(g('axial_force_kN', g('tensile_force',
        0.0)), 0.0)
60
61    edge_type = getattr(self.bolt, 'edgetype', 'Sheared or
        hand flame cut')
62    bolt_dia_prov = f2(getattr(self.bolt, '
        bolt_diameter_provided', 0.0) if hasattr(self, 'bolt
        ') else 0.0, 0.0)
63    bolt_grade_prov = f2(getattr(self.bolt, '
        bolt_grade_provided', 0.0) if hasattr(self, 'bolt')
        else 0.0, 0.0)
64    bolt_type = getattr(self.bolt, 'bolt_type',
        VALUE_NOT_APPLICABLE) if hasattr(self, 'bolt') else
        VALUE_NOT_APPLICABLE
65
66    bolt_shear_kN = f2(getattr(self.bolt, '
        bolt_shear_capacity', 0.0) if hasattr(self, 'bolt')
        else 0.0, 0.0)
67    bolt_bearing_kN = f2(getattr(self.bolt, '
        bolt_bearing_capacity', 0.0) if hasattr(self, 'bolt'
        ) else 0.0, 0.0)
68    bolt_final_cap = f2(getattr(self.bolt, 'bolt_capacity',
        0.0) if hasattr(self, 'bolt') else 0.0, 0.0)

```

```

69         rows = as_int(g('rows', 0), 0)
70         cols = as_int(g('cols', 0), 0)
71         n_bolts = as_int(g('number_bolts', 0), 0)
72         pitch = f2(g('final_pitch', 0.0), 0.0)
73         gauge = f2(g('final_gauge', 0.0), 0.0)
74         e_dist = f2(g('final_edge_dist', 0.0), 0.0)
75
76
77         t_fu_fy_list = getattr(self, 'bolt_conn_plates_t_fu_fy'
78                                   , [])
79         if t_fu_fy_list and len(t_fu_fy_list) > 0:
80             fu = t_fu_fy_list[0][1] if len(t_fu_fy_list[0]) > 1
81                 else 0
82             fy = t_fu_fy_list[0][2] if len(t_fu_fy_list[0]) > 2
83                 else 0
84         else:
85             fy = g('yield_stress', 0)
86             fu = 0
87
88         base_metal_capacity_kN = f2(g('base_metal_capacity_kN',
89                                       0.0), 0.0)
90
91         A_g = f2(g('A_g', 0.0), 0.0)
92         T_dg = f2(g('T_dg', 0.0), 0.0)
93         T_dn = f2(g('T_dn', 0.0), 0.0)
94         T_db = f2(g('T_db', 0.0), 0.0)
95
96         overall_ur = round(g('utilization_ratio', 0.0), 3)
97
98         self.report_input = {
99             KEY_MODULE: "Lap Joint Bolted Connection",
100             KEY_MAIN_MODULE: "Plate(d) Connection",
101             KEY_DISP_DESIGN_FOR: design_for,
102             "Thickness of Plate-1 (mm) *": plate1_thk,
103             "Thickness of Plate-2 (mm) *": plate2_thk,
104             "Width of Plate (mm) *": width,
105             "Material *": getattr(self, 'main_material',
106                                     VALUE_NOT_APPLICABLE),
107             "Diameter (mm) *": bolt_dia_prov,

```

```

103         "Property Class *": bolt_grade_prov,
104         "Type *": bolt_type,
105         f"{'Tensile' if not is_comp else 'Axial'} Force (kN
            ) *": axial_kN,
106         "Additional inputs": "TITLE",
107         "Bolt Hole Type": getattr(self.bolt, 'boltholetype',
            , 'Standard'),
108         "Slip Factor ( f )": getattr(self.bolt, 'mu_f', 'N/
            A'),
109         "Edge Preparation Method": edge_type
110     }
111
112     self.report_check = []
113
114     #
115     #===== SECTION 2.1: CALCULATING BOLT STRENGTH
116     #=====
117
118     self.report_check.append([
119         "SubSection", "Calculating Bolt Strength", "|p{4cm
            }|p{5cm}|p{5.5cm}|p{1.5cm}|"
120     ])
121
122     d = float(self.bolt.bolt_diameter_provided)
123     bolt_grade = float(self.bolt.bolt_grade_provided)
124     f_ub = int(bolt_grade * 100)
125
126     plate1_thk_raw = float(self.plate1.thickness[0]) if
        isinstance(self.plate1.thickness, list) else float(
            self.plate1.thickness)
127     plate2_thk_raw = float(self.plate2.thickness[0]) if
        isinstance(self.plate2.thickness, list) else float(
            self.plate2.thickness)
128
129     bolt_shank_area = f2(math.pi * d**2 / 4, 0.0)

```

```

129
130         if hasattr(self.bolt, 'bolt_net_area_provided'):
131             bolt_net_area = f2(self.bolt.bolt_net_area_provided
132                                , 0.0)
132         else:
133             bolt_net_area = f2(math.pi * (d - 0.9382 * math.
134                                sqrt(d))**2 / 4, 0.0)
134
135         gamma_mb = 1.25
136
137         if self.bolt.bolt_type != "Bearing Bolt":
138             # ===== FRICTION GRIP TYPE BOLTING (Cl.
139             # 10.4.3) =====
140             f_0 = 0.7 * f_ub
141             F_o = bolt_net_area * f_0
142             mu = float(self.bolt.mu_f) if hasattr(self.bolt, '
143                mu_f') else 0.3
144             n_e = 1 # Number of effective interfaces (single
145                lap joint)
146
147             bolt_hole_type_str = str(self.bolt.bolt_hole_type)
148             if hasattr(self.bolt, 'bolt_hole_type') else "
149                Standard"
150
151             d_0 = IS800_2007.cl_10_2_1_bolt_hole_size(d,
152                bolt_hole_type_str)
153
154             hole_type_lower = bolt_hole_type_str.lower()
155             if "standard" in hole_type_lower:
156                 K_h = 1.0
157             elif "over" in hole_type_lower or "short" in
158                hole_type_lower:
159                 K_h = 0.85
160             else: # long slotted
161                 K_h = 0.7
162
163             V_nsf = mu * n_e * K_h * F_o
164             gamma_mf = 1.25 # For ultimate load
165             V_dsf_theoretical = V_nsf / gamma_mf
166             V_dsf_kN_theoretical = V_dsf_theoretical / 1000

```

```

159
160         slip_req = Math(inline=True)
161         slip_req.append(NoEscape(r'\begin{aligned}'))
162         slip_req.append(NoEscape(r'V_{dsf} \&= \frac{V_{nsf}}{\gamma_{mf}}'))
163         slip_req.append(NoEscape(r'V_{nsf} \&= \mu \cdot n_e \cdot K_h \cdot F_o'))
164         slip_req.append(NoEscape(r'\mu \&= ' + f'{mu:.2f}' +
165                                   r' \text{ (slip factor)}'))
166         slip_req.append(NoEscape(r'n_e \&= ' + str(n_e) + r'
167                                   \text{ (interfaces)}'))
168         slip_req.append(NoEscape(r'K_h \&= ' + f'{K_h:.2f}'
169                                   + r' \text{ (hole factor)}'))
170         slip_req.append(NoEscape(r'f_0 \&= 0.7 f_{ub} = ' +
171                                   f'{f_0:.1f}' + r' \text{ MPa}'))
172         slip_req.append(NoEscape(r'A_{nb} \&= ' + f'{
173                                   bolt_net_area:.2f}' + r' \text{ mm}^2'))
174         slip_req.append(NoEscape(r'F_o \&= A_{nb} \times f_0 = ' +
175                                   f'{F_o:.2f}' + r' \text{ N}'))
176         slip_req.append(NoEscape(r'V_{nsf} \&= ' + f'{mu:.2f}' + r' \times ' +
177                                   str(n_e) + r' \times ' + f'{K_h:.2f}' + r' \times ' +
178                                   f'{F_o:.2f}' + r' \text{ N}'))
179         slip_req.append(NoEscape(r'\&= ' + f'{V_nsf:.2f}' + r' \text{ N}'))
180         slip_req.append(NoEscape(r'V_{dsf} \&= \frac{' + f'{V_nsf:.2f}' + r'}{' +
181                                   str(gamma_mf) + r'} = ' + f'{V_dsf_kN_theoretical:.2f}' +
182                                   r' \text{ kN}'))
183         slip_req.append(NoEscape(r'&[\text{Ref. Cl. 10.4.3}]'))
184         slip_req.append(NoEscape(r'\end{aligned}'))
185
186         self.report_check.append(["Slip Resistance", "", slip_req, ""])
187
188     else: # Bearing Bolt
189         # ===== SHEAR CAPACITY (Cl. 10.3.3) =====
190         V_dsb_kN = bolt_shear_kN
191         V_nsb = V_dsb_kN * gamma_mb

```

```

182
183         n_n = 1 # Threads intercepting shear plane
184         n_s = 0 # No threads without shear
185
186         shear_req = Math(inline=True)
187         shear_req.append(NoEscape(r'\begin{aligned}\\'))
188         shear_req.append(NoEscape(r'V_{dsb} &= \frac{V_{nsb}}{\gamma_{mb}}\\'))
189         shear_req.append(NoEscape(r'V_{nsb} &= \frac{f_{ub}}{\sqrt{3}} \cdot (n_n \cdot A_{nb} + n_s \cdot A_{sb})\\'))
190         shear_req.append(NoEscape(r'&= \frac{' + str(f_ub)
191         + r'}{\sqrt{3}} \cdot (1 \cdot ' + f'{
192         bolt_net_area:.2f}' + r')\\'))
193         shear_req.append(NoEscape(r'&= ' + f'{V_nsb:.2f}' +
194         r' \text{ kN}\\'))
195         shear_req.append(NoEscape(r'V_{dsb} &= \frac{' + f'
196         {V_nsb:.2f}' + r'}{' + str(gamma_mb) + r'}\\'))
197         shear_req.append(NoEscape(r'&= ' + f'{V_dsb_kN:.2f}'
198         + r' \text{ kN}\\'))
199         shear_req.append(NoEscape(r'&[\text{Ref. Cl.
200         10.3.3}]'))
201         shear_req.append(NoEscape(r'\end{aligned}'))
202
203         self.report_check.append(["Shear Capacity", "",
204         shear_req, ""])
205
206         # ===== BEARING CAPACITY (Cl. 10.3.4)
207         =====
208
209         V_dpb_kN = bolt_bearing_kN
210         V_npb = V_dpb_kN * gamma_mb
211
212         t_min = min(plate1_thk_raw, plate2_thk_raw)
213         f_u_plate = min(self.plate1.fu, self.plate2.fu)
214
215         bolt_hole_type_str = str(self.bolt.bolt_hole_type)
216         if hasattr(self.bolt, 'bolt_hole_type') else "
217         Standard"
218
219         d_0 = IS800_2007.cl_10_2_1_bolt_hole_size(d,

```

```

        bolt_hole_type_str)
208
209     e = float(self.final_end_dist) if hasattr(self, '
        final_end_dist') and self.final_end_dist > 0
        else float(self.bolt.min_end_dist_round)
210     p = float(self.final_pitch) if hasattr(self, '
        final_pitch') and self.final_pitch > 0 else
        float(self.bolt.min_pitch_round)
211
212     # Calculate kb factor components (always calculate
        for report display)
213     if p > 0:
214         kb_1 = e / (3.0 * d_0)
215         kb_2 = p / (3.0 * d_0) - 0.25
216         kb_3 = f_ub / f_u_plate
217         kb_4 = 1.0
218         kb_calc = min(kb_1, kb_2, kb_3, kb_4)
219     else:
220         kb_1 = e / (3.0 * d_0)
221         kb_2 = float('inf') # Not applicable
222         kb_3 = f_ub / f_u_plate
223         kb_4 = 1.0
224         kb_calc = min(kb_1, kb_3, kb_4)
225
226     if hasattr(self.bolt, 'kb') and self.bolt.kb is not
        None:
227         k_b = f2(self.bolt.kb, 1.0)
228     else:
229         k_b = f2(kb_calc, 1.0)
230
231     kb_req = Math(inline=True)
232     kb_req.append(NoEscape(r'\begin{aligned}\\'))
233     kb_req.append(NoEscape(r'k_b &= \min\left(\frac{e}
        \{3d_0\}, \frac{p}{3d_0}-0.25, \frac{f_{ub}}{f_u}
        \}, 1.0\right)\\\\'))
234     kb_req.append(NoEscape(r'&= \min\left(\frac{' + f'{
        e:.1f}' + r'}{3 \times ' + f'{d_0:.1f}' + r'}, \
        \frac{' + f'{p:.1f}' + r'}{3 \times ' + f'{d_0:.1
        f}' + r'}-0.25, \frac{' + str(f_ub) + r'}{' +

```

```

235         str(f_u_plate) + r'}, 1.0\right)\\\')
236
237     if p > 0:
238         kb_req.append(NoEscape(r'&= \min(' + f'{kb_1:.2f}' + r', ' + f'{kb_2:.2f}' + r', ' + f'{kb_3:.2f}' + r', 1.0)\\\'))
239     else:
240         kb_req.append(NoEscape(r'&= \min(' + f'{kb_1:.2f}' + r', ' + f'{kb_3:.2f}' + r', 1.0)\\\'))
241
242     kb_req.append(NoEscape(r'&= ' + f'{k_b:.2f}'))
243     kb_req.append(NoEscape(r'\end{aligned}'))
244     self.report_check.append(["Bearing Factor", "", kb_req, ""])
245
246     bearing_req = Math(inline=True)
247     bearing_req.append(NoEscape(r'\begin{aligned}'))
248     bearing_req.append(NoEscape(r'V_{dpb} &= \frac{V_{npb}}{\gamma_{mb}}\\\'))
249     bearing_req.append(NoEscape(r'V_{npb} &= 2.5 \cdot k_b \cdot d \cdot t \cdot f_u\\\'))
250     bearing_req.append(NoEscape(r'&= 2.5 \times ' + f'{k_b:.3f}' + r' \times ' + f'{d:.1f}' + r' \times ' + f'{t_min:.1f}' + r' \times ' + str(f_u_plate) + r'\\\'))
251     bearing_req.append(NoEscape(r'&= ' + f'{V_npb:.2f}' + r' \text{ kN}\\\'))
252     bearing_req.append(NoEscape(r'V_{dpb} &= \frac{' + f'{V_npb:.2f}' + r'}{' + f'{gamma_mb:.2f}' + r'}\\\'))
253     bearing_req.append(NoEscape(r'&= ' + f'{V_dpb_kN:.2f}' + r' \text{ kN}\\\'))
254     bearing_req.append(NoEscape(r'&[\text{Ref. C1. 10.3.4}]'))
255     bearing_req.append(NoEscape(r'\end{aligned}'))
256     self.report_check.append(["Bearing Capacity", "", bearing_req, ""])

```

```

257
258         V_db_kN = bolt_final_cap
259
260         cap_req = Math(inline=True)
261         cap_req.append(NoEscape(r'\begin{aligned}'))
262         cap_req.append(NoEscape(r'V_{db} \leq \min(' + f'{
                bolt_shear_kN:.2f}' + r', ' + f'{bolt_bearing_kN
                :.2f}' + r'))+r'\\'))
263         cap_req.append(NoEscape(r'\leq ' + f'{V_db_kN:.2f}' +
                r' \text{ kN}'+r'\\'))
264         cap_req.append(NoEscape(r'&[\text{Ref. Cl. 10.3.2,
                IS 800:2007}]'))
265         cap_req.append(NoEscape(r'\end{aligned}'))
266
267         self.report_check.append(["Bolt Design Capacity", "
                ", cap_req, ""])
268
269         #
                =====
270
                #===== SECTION 2.2: REDUCTION FACTORS
                =====
271
                #
                =====
272
                self.report_check.append([
273                 "SubSection", "Reduction Factors", "|p{4cm}|p{5cm}|
                p{5.5cm}|p{1.5cm}|"
274             ])
275
276             l_j = (self.rows - 1) * self.final_pitch if self.rows >
                1 else 0
277             d = self.bolt.bolt_diameter_provided
278
279             lj_req = Math(inline=True)
280             lj_req.append(NoEscape(r'\begin{aligned}'))
281
282             if l_j > 15 * d:
283                 beta_lj = 1.075 - (l_j / (200 * d))

```

```

284         beta_lj = max(0.75, min(beta_lj, 1.0))
285         lj_req.append(NoEscape(r'\text{Since } l_j > 15d\\
        '))
286         lj_req.append(NoEscape(r'l_j = ' + str(l_j) + r' \
        text{ mm}, \quad 15d = ' + str(15 * d) + r' \
        text{ mm}\\'))
287         lj_req.append(NoEscape(r'\beta_{lj} = 1.075 - \
        frac{l_j}{200 \cdot d}\\'))
288         lj_req.append(NoEscape(r'&= 1.075 - \frac{' + str(
        l_j) + r'}{200 \times ' + str(d) + r'}\\'))
289         lj_req.append(NoEscape(r'&= ' + f'{1.075 - (l_j /
        (200 * d)):.3f}' + r'\\'))
290         lj_req.append(NoEscape(r'&\text{(but } 0.75 \leq \
        beta_{lj} \leq 1.0\text{)}\\'))
291         lj_req.append(NoEscape(r'\beta_{lj} = ' + f'{
        beta_lj:.2f}' + r'\\'))
292         lj_status = ""
293     else:
294         beta_lj = 1.0
295         lj_req.append(NoEscape(r'\text{Since } l_j \leq 15
        d\\'))
296         lj_req.append(NoEscape(r'l_j = ' + str(l_j) + r' \
        text{ mm}, \quad 15d = ' + str(15 * d) + r' \
        text{ mm}\\'))
297         lj_req.append(NoEscape(r'\beta_{lj} = 1.0 \text{ (
        No reduction)}\\'))
298         lj_status = "PASS"
299
300         lj_req.append(NoEscape(r'&[\text{Ref. Cl. 10.3.3.1}]'))
301         lj_req.append(NoEscape(r'\end{aligned}'))
302
303         lj_prov = Math(inline=True)
304         lj_prov.append(NoEscape(r'\beta_{lj} = ' + f'{beta_lj
        :.2f}'))
305
306         self.report_check.append(["Long Joint Factor", lj_req,
        lj_prov, ''])
307
308         l_g = plate1_thk_raw + plate2_thk_raw

```

```

309
310         lg_req = Math(inline=True)
311         lg_req.append(NoEscape(r'\begin{aligned}'))
312
313         if l_g > 5 * d:
314             beta_lg = (8 * d) / (3 * d + l_g)
315             beta_lg = min(beta_lg, beta_lj) if beta_lj else
316                 beta_lg
317             lg_req.append(NoEscape(r'\text{Since } l_g > 5d\\'
318                                     ))
319             lg_req.append(NoEscape(r'l_g &= ' + str(l_g) + r' \
320                                     text{ mm}, \quad 5d = ' + str(5 * d) + r' \text{
321                                     mm}\\'))
322             lg_req.append(NoEscape(r'\beta_{lg} &= \frac{8d}{3d
323                                     + l_g}\\'))
324             lg_req.append(NoEscape(r'&= \frac{8 \times ' + str(
325                                     d) + r'}{3 \times ' + str(d) + r' + ' + str(l_g)
326                                     + r'}\\'))
327             lg_req.append(NoEscape(r'&= ' + f'{(8 * d) / (3 * d
328                                     + l_g):.3f}' + r'\\'))
329             lg_req.append(NoEscape(r'\beta_{lg} &\leq \beta_{lj}
330                                     \\'))
331             lg_req.append(NoEscape(r'\beta_{lg} &= ' + f'{
332                                     beta_lg:.2f}' + r'\\'))
333             lg_status = ""
334         else:
335             beta_lg = 1.0
336             lg_req.append(NoEscape(r'\text{Since } l_g \leq 5d
337                                     \\'))
338             lg_req.append(NoEscape(r'l_g &= ' + str(l_g) + r' \
339                                     text{ mm}, \quad 5d = ' + str(5 * d) + r' \text{
340                                     mm}\\'))
341             lg_req.append(NoEscape(r'\beta_{lg} &= 1.0 \text{ (
342                                     No reduction)}\\'))
343             lg_status = "PASS"
344
345         lg_req.append(NoEscape(r'&[\text{Ref. C1. 10.3.3.2}]'))
346         lg_req.append(NoEscape(r'\end{aligned}'))
347

```

```

334         lg_prov = Math(inline=True)
335         lg_prov.append(NoEscape(r'\beta_{lg} = ' + f'{beta_lg
           :.2f}'))
336
337         self.report_check.append(["Large Grip Factor", lg_req,
           lg_prov, ''])
338
339         if self.bolt.bolt_hole_type != "Standard":
340             hole_req = Math(inline=True)
341             hole_req.append(NoEscape(r'\begin{aligned}'))
342             hole_req.append(NoEscape(r'\text{Hole Type: }' +
           self.bolt.bolt_hole_type + r'\\'))
343             if "oversized" in self.bolt.bolt_hole_type.lower()
           or "short" in self.bolt.bolt_hole_type.lower():
344                 hole_factor = 0.7
345             else: # long-slotted
346                 hole_factor = 0.5
347             hole_req.append(NoEscape(r'\text{Reduction Factor}
           &= ' + str(hole_factor) + r'\\'))
348             hole_req.append(NoEscape(r'&[\text{Ref. Cl.
           10.3.4}]'))
349             hole_req.append(NoEscape(r'\end{aligned}'))
350             self.report_check.append(["Hole Type Reduction",
           hole_req, "", ""])
351
352         #=====
353         # Section 2.3: Detailing Requirements
354         #=====
355         self.report_check.append([
356             "SubSection", "Detailing Requirements", "|p{4cm}|p
           {5cm}|p{5.5cm}|p{1.5cm}|"
357         ])
358
359         # 2.3.1 Minimum Spacing (Cl. 10.2.2)
360         p_min = as_int(2.5 * bolt_dia_prov, 0)
361         g_min = as_int(2.5 * bolt_dia_prov, 0)
362
363         spacing_req = Math(inline=True)
364         spacing_req.append(NoEscape(r'\begin{aligned}'))

```

```

365         spacing_req.append(NoEscape(r'p_{\text{min}} \&= 2.5 \
           \cdot d\\'))
366         spacing_req.append(NoEscape(r'\&= 2.5 \times ' + str(
           bolt_dia_prov) + r'\\'))
367         spacing_req.append(NoEscape(r'\&= ' + str(p_min) + r' \
           \text{ mm}\\'))
368         spacing_req.append(NoEscape(r'g_{\text{min}} \&= 2.5 \
           \cdot d\\'))
369         spacing_req.append(NoEscape(r'\&= 2.5 \times ' + str(
           bolt_dia_prov) + r'\\'))
370         spacing_req.append(NoEscape(r'\&= ' + str(g_min) + r' \
           \text{ mm}\\ \\\'))
371         spacing_req.append(NoEscape(r'\&[\text{Ref. Cl. 10.2.2}]
           '))
372         spacing_req.append(NoEscape(r'\end{aligned}'))
373
374         spacing_prov = Math(inline=True)
375         spacing_prov.append(NoEscape(r'\begin{aligned}'))
376         spacing_prov.append(NoEscape(r'p_{\text{prov}} \&= ' +
           str(pitch) + r' \text{ mm}\\'))
377         spacing_prov.append(NoEscape(r'g_{\text{prov}} \&= ' +
           str(gauge) + r' \text{ mm}'))
378         spacing_prov.append(NoEscape(r'\end{aligned}'))
379
380         spacing_status = "PASS" if (pitch >= p_min and gauge >=
           g_min) else "FAIL"
381         self.report_check.append(["Minimum Spacing",
           spacing_req, spacing_prov, spacing_status])
382
383         # 2.3.2 Maximum Spacing (Cl. 10.2.3.1)
384         plate_thk_min = min(plate1_thk_raw, plate2_thk_raw)
385         p_max = as_int(min(32 * plate_thk_min, 300), 0)
386         g_max = as_int(min(32 * plate_thk_min, 300), 0)
387
388         max_spacing_req = Math(inline=True)
389         max_spacing_req.append(NoEscape(r'\begin{aligned}'))
390         max_spacing_req.append(NoEscape(r'p_{\text{max}} \&= \
           min(32 \cdot t, 300 \text{ mm})\\'))
391         max_spacing_req.append(NoEscape(r'\&= \min(32 \times ' +

```

```

392         str(plate_thk_min) + r', 300)\')
```

$$\max_spacing_req.append(\text{NoEscape}(r'\&= ' + \text{str}(p_max) + r'$$

$$'\ \text{\texttt{\textbackslash text\{ mm\}\}\}\')$$

```

393     max_spacing_req.append(\text{NoEscape}(r'g_{\text{\texttt{\textbackslash text\{ max\}\}} \&= \
```

$$\min(32\ \text{\texttt{\textbackslash cdot t}}, 300\ \text{\texttt{\textbackslash text\{ mm\}\}\}\')$$

```

394     max_spacing_req.append(\text{NoEscape}(r'\&= \min(32\ \text{\texttt{\textbackslash times }} +
```

$$\text{str(plate_thk_min)} + r', 300)\')$$

```

395     max_spacing_req.append(\text{NoEscape}(r'\&= ' + \text{str}(g\_max) + r
```

$$'\ \text{\texttt{\textbackslash text\{ mm\}\}\ \text{\texttt{\textbackslash \textbackslash}}}\')$$

```

396     max_spacing_req.append(\text{NoEscape}(r'\&[\text{\texttt{\textbackslash text\{ Ref. Cl.

$$10.2.3.1\}]\')$$


```

397 max_spacing_req.append(\text{NoEscape}(r'\end{aligned}'))
398
399 max_spacing_prov = Math(inline=True)
400 max_spacing_prov.append(\text{NoEscape}(r'\begin{aligned}'))
401 max_spacing_prov.append(\text{NoEscape}(r'p_{\text{\texttt{\textbackslash text\{ prov\}\}} \&= '
402 + \text{str}(pitch) + r'\ \text{\texttt{\textbackslash text\{ mm\}\}\}\')


```

402     max_spacing_prov.append(\text{NoEscape}(r'g_{\text{\texttt{\textbackslash text\{ prov\}\}} \&= '
403         + \text{str}(gauge) + r'\ \text{\texttt{\textbackslash text\{ mm\}\}\}\')


```

403 max_spacing_prov.append(\text{NoEscape}(r'\end{aligned}'))
404
405 max_spacing_status = "PASS" if (pitch <= p_max and
406 gauge <= g_max) else "FAIL"
407 self.report_check.append(["Maximum Spacing",
408 max_spacing_req, max_spacing_prov,
409 max_spacing_status])
410
411 # 2.3.3 Edge Distance (Cl. 10.2.4)
412 bolt_hole_type_str = \text{str}(self.bolt.bolt_hole_type) if
413 \text{hasattr}(self.bolt, 'bolt_hole_type') else "Standard"
414 d_hole = IS800_2007.cl_10_2_1_bolt_hole_size(d,
415 bolt_hole_type_str)
416
417 if "Sheared" in edge_type or "hand flame cut" in
418 edge_type:
419 e_min_calc = f2(1.7 * d_hole, 0.0)
420 e_min_multiplier = 1.7
421 else: # Rolled, machine-flame cut, sawn and planed
422 e_min_calc = f2(1.5 * d_hole, 0.0)
```


```


```


```

```

417         e_min_multiplier = 1.5
418
419         epsilon = math.sqrt(250 / fy)
420         e_max_calc = f2(12 * plate_thk_min * epsilon, 0.0)
421
422         edge_req = Math(inline=True)
423         edge_req.append(NoEscape(r'\begin{aligned}'))
424         edge_req.append(NoEscape(r'e_{\min} \&= ' + str(
425             e_min_multiplier) + r' \cdot d_0\\'))
426         edge_req.append(NoEscape(r'\&= ' + str(e_min_multiplier)
427             + r' \times ' + f'{d_hole:.1f}' + r' = ' + f'{
428                 e_min_calc:.1f}' + r' \text{ mm}\\'))
429         edge_req.append(NoEscape(r'e_{\text{max}} \&= 12 \cdot t
430             \cdot \varepsilon\\'))
431         edge_req.append(NoEscape(r'\&= 12 \times ' + str(
432             plate_thk_min) + r' \times ' + f'{epsilon:.2f}' + r'
433             \\'))
434         edge_req.append(NoEscape(r'\&= ' + str(e_max_calc) + r'
435             \text{ mm}\\ \\'))
436         edge_req.append(NoEscape(r'&[\text{Ref. Cl. 10.2.4}]'))
437         edge_req.append(NoEscape(r'\end{aligned}'))
438
439         edge_prov = Math(inline=True)
440         edge_prov.append(NoEscape(r'e_{\text{prov}} = ' + str(
441             e_dist) + r' \text{ mm}'))
442
443         edge_status = "PASS" if (e_dist >= e_min_calc and
444             e_dist <= e_max_calc) else "FAIL"
445         self.report_check.append(["Edge Distance", edge_req,
446             edge_prov, edge_status])
447
448         #=====
449         # Section 2.4: Number of Bolts
450         #=====
451         self.report_check.append([
452             "SubSection", "Number of Bolts Required", "|p{4cm}|
453                 p{5cm}|p{5.5cm}|p{1.5cm}|"
454             ])

```

```

445         bolts_req_initial = math.ceil(axial_kN / bolt_final_cap
446         ) if bolt_final_cap > 0 else 0
447
448         bolts_eq = Math(inline=True)
449         bolts_eq.append(NoEscape(r'\begin{aligned}\\'))
450         bolts_eq.append(NoEscape(r'n &= \frac{P}{V_{db}}\\\\'))
451         bolts_eq.append(NoEscape(r'&= \frac{' + str(axial_kN) +
452         r'}{' + str(bolt_final_cap) + r'}\\\\'))
453         bolts_eq.append(NoEscape(r'&= ' + str(bolts_req_initial
454         ) + r' \text{ nos.}\\'))
455         bolts_eq.append(NoEscape(r'\end{aligned}'))
456
457         self.report_check.append(["Bolts Required", f" {
458         axial_kN:.2f} kN", bolts_eq, "")
459
460         #=====
461         # Section 2.5: Bolt Arrangement
462         #=====
463         self.report_check.append([
464             "SubSection", "Bolt Arrangement", "|p{4cm}|p{5cm}|p
465             {5.5cm}|p{1.5cm}|"
466         ])
467
468         self.report_check.append([
469             "Bolt Pattern", "2", f"Arrangement: {rows} rows
470             {cols} columns", ""
471         ])
472
473         #=====
474         # Section 2.6: Base Metal Strength
475         #=====
476         self.report_check.append([
477             "SubSection", "Base Metal Strength", "|p{4cm}|p{5cm
478             }|p{5.5cm}|p{1.5cm}|"
479         ])
480
481         if is_comp:
482             base_req = Math(inline=True)
483             base_req.append(NoEscape(r'\begin{aligned}\\'))

```

```

477         base_req.append(NoEscape(r'P_d &= \frac{A_g \cdot
         f_y}{\gamma_{m0}}\\\\'))
478         base_req.append(NoEscape(r'&= \frac{' + str(A_g) +
         r' \times ' + str(fy) + r'}{1.10}\\\\'))
479         base_req.append(NoEscape(r'&= ' + f'{
         base_metal_capacity_kN:.2f}' + r' \text{ kN}\\\\')
         )
480         base_req.append(NoEscape(r'&[\text{Ref. Cl. 7.1.2}]
         '))
481         base_req.append(NoEscape(r'\end{aligned}'))
482
483         base_status = "PASS" if base_metal_capacity_kN >=
         axial_kN else "FAIL"
484         self.report_check.append(["Plate Tension Capacity",
         "", base_req, base_status])
485     else:
486         # 1. Gross Section Yielding
487         yield_req = Math(inline=True)
488         yield_req.append(NoEscape(r'\begin{aligned}'))
489         yield_req.append(NoEscape(r'T_{dg} &= \frac{A_g \cdot
         f_y}{\gamma_{m0}}\\\\'))
490         yield_req.append(NoEscape(r'&= \frac{' + str(A_g) +
         r' \times ' + str(fy) + r'}{1.10}\\\\'))
491         yield_req.append(NoEscape(r'&= ' + f'{T_dg:.2f}' +
         r' \text{ kN}\\\\'))
492         yield_req.append(NoEscape(r'&[\text{Ref. Cl. 6.2}]')
         ))
493         yield_req.append(NoEscape(r'\end{aligned}'))
494         self.report_check.append(["Gross Section Yield", "",
         , yield_req, ""])
495
496         # 2. Net Section Rupture
497         rup_req = Math(inline=True)
498         rup_req.append(NoEscape(r'\begin{aligned}'))
499         rup_req.append(NoEscape(r'T_{dn} &= \frac{0.9 A_n
         f_u}{\gamma_{m1}}\\\\'))
500         rup_req.append(NoEscape(r'&= ' + f'{T_dn:.2f}' + r'
         \text{ kN}\\\\'))
501         rup_req.append(NoEscape(r'&[\text{Ref. Cl. 6.3}]'))

```

```

502 rup_req.append(NoEscape(r'\end{aligned}'))
503 self.report_check.append(["Net Section Rupture", ""
    , rup_req, ""])
504
505 # 3. Block Shear (Cl 6.4)
506 # Recalculate areas for report clarity
507 # Note: We use the same logic as the solver's
    check_base_metal_strength
508 n_r = self.rows
509 p = self.final_pitch
510 g_val = self.final_gauge
511 e_val = self.final_end_dist
512 dia_hole = IS800_2007.cl_10_2_1_bolt_hole_size(d,
    str(self.bolt.bolt_hole_type))
513
514 t_min = min(plate1_thk_raw, plate2_thk_raw)
515
516 Avg = t_min * ((n_r - 1) * g_val + e_val)
517 Avn = t_min * ((n_r - 1) * g_val + e_val - (n_r -
    0.5) * dia_hole)
518 Atg = t_min * e_val
519 Atn = t_min * (e_val - 0.5 * dia_hole)
520
521 Tdb1 = (Avg * fy / (math.sqrt(3) * 1.10) + 0.9 *
    Atn * fu / 1.25) / 1000
522 Tdb2 = (0.9 * Avn * fu / (math.sqrt(3) * 1.25) +
    Atg * fy / 1.10) / 1000
523 Tdb = min(Tdb1, Tdb2)
524
525 block_req = Math(inline=True)
526 block_req.append(NoEscape(r'\begin{aligned}'))
527 block_req.append(NoEscape(r'A_{vg} \&= ' + f'{Avg:.0
    f}' + r' \text{ mm}^2, \quad A_{vn} = ' + f'{Avn
    :.0f}' + r' \text{ mm}^2\\'))
528 block_req.append(NoEscape(r'A_{tg} \&= ' + f'{Atg:.0
    f}' + r' \text{ mm}^2, \quad A_{tn} = ' + f'{Atn
    :.0f}' + r' \text{ mm}^2\\'))
529 block_req.append(NoEscape(r'T_{db1} \&= \frac{A_{vg}
    f_y}{\sqrt{3} \gamma_{m0}} + \frac{0.9 A_{tn}

```

```

        f_u}{\gamma_{m1}} = ' + f'{Tdb1:.2f}' + r' \text
        { kN}\\')
530     block_req.append(NoEscape(r'T_{db2} &= \frac{0.9 A_
        {vn} f_u}{\sqrt{3} \gamma_{m1}} + \frac{A_{tg}
        f_y}{\gamma_{m0}} = ' + f'{Tdb2:.2f}' + r' \text
        { kN}\\')
531     block_req.append(NoEscape(r'T_{db} &= \min(T_{db1},
        T_{db2}) = ' + f'{Tdb:.2f}' + r' \text{ kN}\\')
        )
532     block_req.append(NoEscape(r'&[\text{Ref. Cl.
        6.4.1}]'))
533     block_req.append(NoEscape(r'\end{aligned}'))
534     self.report_check.append(["Block Shear", "",
        block_req, ""])
535
536     # Governing Strength
537     base_req = Math(inline=True)
538     base_req.append(NoEscape(r'\begin{aligned}'))
539     base_req.append(NoEscape(r'T_d &= \min(T_{dg}, T_{
        dn}, T_{db})\\'))
540     base_req.append(NoEscape(r'&= ' + f'{
        base_metal_capacity_kN:.2f}' + r' \text{ kN}\\')
        )
541     base_req.append(NoEscape(r'\end{aligned}'))
542
543     base_status = "PASS" if base_metal_capacity_kN >=
        axial_kN else "FAIL"
544     self.report_check.append(["Plate Tension Capacity",
        "", base_req, base_status])
545
546     #=====
547     # Section 2.7: Design Summary
548     #=====
549     self.report_check.append([
550         "SubSection", "Design Summary", "|p{4cm}|p{5cm}|p
        {5.5cm}|p{1.5cm}|"
551     ])
552
553     bolt_capacity_total = f2(bolt_final_cap * n_bolts, 0.0)

```

```

554         bolt_ur = axial_kN / bolt_capacity_total if
           bolt_capacity_total > 0 else 999.0
555
556         plate_ur = axial_kN / base_metal_capacity_kN if
           base_metal_capacity_kN > 0 else 999.0
557
558         # Overall UR is max of both
559         overall_ur_val = max(bolt_ur, plate_ur)
560         overall_ur = round(overall_ur_val, 3)
561
562         ur_req = Math(inline=True)
563         ur_req.append(NoEscape(r'\begin{aligned}\\'))
564         ur_req.append(NoEscape(r'\text{Bolt Capacity} \&= ' +
           str(bolt_capacity_total) + r' \text{ kN}\\'))
565         ur_req.append(NoEscape(r'\text{Plate Capacity} \&= ' +
           str(base_metal_capacity_kN) + r' \text{ kN}\\'))
566         ur_req.append(NoEscape(r'\text{UR}_{\text{bolt}} \&= \
           frac{' + str(axial_kN) + r'}{' + str(
           bolt_capacity_total) + r'}\\'))
567         ur_req.append(NoEscape(r'\&= ' + f'{bolt_ur:.3f}' + r'
           \\'))
568         ur_req.append(NoEscape(r'\text{UR}_{\text{plate}} \&= \
           frac{' + str(axial_kN) + r'}{' + str(
           base_metal_capacity_kN) + r'}\\'))
569         ur_req.append(NoEscape(r'\&= ' + f'{plate_ur:.3f}' + r'
           \\'))
570         ur_req.append(NoEscape(r'\text{UR}_{\text{final}} \&= \
           max(\text{UR}_{\text{bolt}}, \text{UR}_{\text{plate}})\\'))
571         ur_req.append(NoEscape(r'\&= ' + str(overall_ur) + r'\
           end{aligned}'))
572
573         util_prov = Math(inline=True)
574         util_prov.append(NoEscape(str(overall_ur) + r' \leq 1.0
           '))
575
576         util_status = "PASS" if overall_ur_val <= 1.0 else "
           FAIL"
577         self.report_check.append(["Utilization Ratio", f"{

```

```

578         axial_kN:.2f} kN", ur_req, util_status])
579
580     Disp_2d_image = []
581     Disp_3D_image = "/ResourceFiles/images/3d.png"
582     rel_path = os.path.abspath(".").replace("\\", "/")
583     fname_no_ext = popup_summary.get("filename", "
        LapJointBoltedReport")
584     folder = popup_summary.get('folder', './reports')
585     os.makedirs(folder, exist_ok=True)
586
587     CreateLatex.save_latex(
588         CreateLatex(), self.report_input, self.report_check
589         ,
590         popup_summary, fname_no_ext, rel_path,
591         Disp_2d_image, Disp_3D_image,
592         module=self.module
593     )
594
595     self.logger.info(f"Report generated successfully: {
596         fname_no_ext}.pdf")
597     return True
598
599 except Exception as e:
600     print(f"WARNING in save_design(): {e}")
601     import traceback
602     traceback.print_exc()
603     return False
604
605 %----- end code -----

```

3.3.1 Explanation of the Code

The `save_design` function in the Bolted Lap Joint module serves as the core automation engine for generating the final design report. It orchestrates the entire process from data retrieval to PDF generation. The function's key operations are summarized below:

1. **Data Retrieval and Initialization:** The function first extracts the design

parameters stored in the class instance. This includes the tensile or compressive load (P), plate dimensions (t_1, t_2, w), and bolt properties (diameter d , grade, and hole type). It also identifies the connection mode (Bearing or Friction Grip) to apply the correct design standards.

2. **Design Status Verification:** A critical check is performed on the `design_status` attribute.

- If the design is marked as **False** (failed), the function generates a brief report summarizing the failure (e.g., “Bolt capacity zero” or “Plate utilization > 1.0 ”).
- If **True** (safe), it proceeds to compile the full report with all calculation details.

3. **Input Dictionary Construction:** The function builds the `report_input` dictionary, which acts as the data bridge to the LaTeX template. Key entries include:

- **Geometry:** Thickness of connected plates and overlap dimensions.
- **Bolt Data:** Shear capacity (V_{dsb}) and bearing capacity (V_{dpb}) per bolt.
- **Arrangement:** Number of rows, columns, pitch (p), and gauge (g).

4. **Automated LaTeX Code Generation:** Using the `pylatex` library, the function dynamically creates LaTeX equations. It injects Python variables directly into math strings to show the step-by-step verification:

- **Shear Check:** $V_{dsb} = \frac{f_u \times A_s}{\sqrt{3} \times \gamma_{mb}}$
- **Bearing Check:** $V_{dpb} = 2.5 \times k_b \times d \times t \times f_u$
- **Utilization Ratio:** $UR = \frac{F_{applied}}{F_{capacity}}$

This ensures the report reflects the exact state of the current design iteration.

5. **Report Compilation and Export:** Finally, the function calls `CreateLatex.save_latex` to render the complete document. It handles file paths robustly using `os.path` to ensure cross-platform compatibility and automatically embeds 2D/3D images of the joint configuration.

3.4 Documentation

The directory structure used for the Report Generation is organized as follows:

```
src/osdag_core
```

```
design_report/  
    reportGenerator_latex.py
```

```
design_type/  
    connection/  
        lap_joint_bolted.py
```

```
Report_functions.py
```

Program Start Calls To start the program, open the Osdag folder, go to src and start the terminal with that path, execute the following command from the project root:

```
$ python -m osdag_gui
```

3.5 References

- Osdag Github repository: <https://osdag.github.io/>
- IS 800:2007, "General Construction in Steel Code of Practice of Practice"

Chapter 4

Report Generation of Bolted Butt Joint

4.1 Problem Statement

The primary objective of this task was to generate a comprehensive design report for **Bolted Butt Joint Connections**. Osdag (Open Steel Design and Graphics) is an open-source tool designed for the design and detailing of steel structures in accordance with Indian Standards. A critical requirement for steel structures is ensuring they pass all Design and Detailing Checklists (DDCL) to guarantee durability and safety. The challenge involved meticulously converting all necessary steps, formulas, and compliance checks stipulated by IS 800:2007 into code to ensure successful report generation for butt joint connections, which involve complex interactions between main plates, cover plates, and bolts.

4.2 Tasks Done

4.2.1 Core Save Design Function Development

- * **Implemented comprehensive `save_design()` function in `butt_joint_bolted.py` with robust error handling**

Developed the main orchestrating function that serves as the entry point

for report generation. This function coordinates data collection from the UI, validates all design parameters (including cover plate thickness and packing plates), performs calculations, and triggers the LaTeX report compilation. It includes comprehensive error handling to manage exceptions during file operations and data processing.

* **Integrated with existing Osdag LaTeX report infrastructure using `CreateLatex` class**

Successfully interfaced the new bolted butt joint module with Osdag's established LaTeX report generation framework. This required constructing a detailed `report_input` dictionary and a structured `report_check` list to pass data dynamically to the `CreateLatex.save_latex` method, ensuring consistency with other connection modules.

* **Implemented proper file path handling with OS-independent path management**

Coded cross-platform file path management using Python's `os.path` module to ensure the report generation works seamlessly across different operating systems. The function automatically handles directory creation for reports if they do not exist.

* **Report Input Dictionary Structure**

Architected a complete data structure that captures every piece of information needed for report generation, including:

- Module identification (Butt Joint Bolted Connection)
- Material properties (Ultimate and Yield stress)
- Geometric parameters (Main plate thickness, Cover plate thickness)
- Bolt specifics (Diameter, Grade, Type - Friction/Bearing)
- Load information (Tensile/Compression Force)
- Cover Plate details (Single/Double, Thickness)

4.2.2 Detailed Design Verification and Check Implementation

Cover Plate and Packing Plate Checks

* Implemented Cover Plate Thickness Logic

Coded logic to automatically determine required cover plate thickness based on the main plate thickness (T_{min}) and connection type (Single/-Double Cover) [Cl. 10.3.3.3]:

$$T_{cp} \geq \begin{cases} \frac{5}{8}T_{min} & \text{for Single Cover} \\ \frac{9}{16}T_{min} & \text{for Double Cover} \end{cases} \quad (4.1)$$

* Packing Plate and Reduction Factor (β_{pkg})

Implemented checks for packing plates when connecting plates of different thicknesses. If the packing thickness exceeds 6mm, a reduction factor (β_{pkg}) is applied to the bolt shear capacity [Cl. 10.3.3.3]:

$$\beta_{pkg} = 1 - 0.0125 \times t_{pkg} \quad (4.2)$$

Bolt Capacity Checks

* Implemented Bolt Shear and Bearing calculations

Coded the mathematical logic for determining bolt capacity based on IS 800:2007 requirements [Cl. 10.3.3, 10.3.4]. The function dynamically calculates capacity based on the bolt type (Bearing or Friction Grip).

Shear Capacity:

$$V_{dsb} = \frac{f_{ub} \times A_{sb}}{\gamma_{mb}} \quad (4.3)$$

Bearing Capacity:

$$V_{dpb} = \frac{2.5 \times k_b \times d \times t \times f_u}{\gamma_{mb}} \quad (4.4)$$

* Capacity Reduction Factors

Implemented advanced checks for "Long Joints" (β_{lj}) and "Large Grips"

(β_{lg}) as per Cl. 10.3.3.1 and 10.3.3.2. The code automatically reduces bolt capacity if the joint length or grip length exceeds specified limits:

$$\beta_{lj} = 1.075 - \frac{l_j}{200d} \quad (0.75 \leq \beta_{lj} \leq 1.0) \quad (4.5)$$

Base Metal Strength Analysis

* Implemented dual strength checks (Yielding and Rupture)

Developed parallel calculation paths for both failure modes in tension member design [Cl. 6.2, 6.3]:

Gross Yielding:

$$T_{dg} = \frac{A_g \times f_y}{\gamma_{m0}} \quad (4.6)$$

Net Rupture:

$$T_{dn} = \frac{0.9 \times A_n \times f_u}{\gamma_{m1}} \quad (4.7)$$

* Block Shear Check

Integrated Block Shear Failure checks (V_{db}) [Cl. 6.4] to ensure the connection does not fail by tearing out a block of material. The final design strength (T_{db}) is taken as the minimum of yielding, rupture, and block shear capacities.

4.2.3 Advanced LaTeX Mathematical Formatting

Mathematical Equation Integration

* Used NoEscape LaTeX formatting for complex mathematical expressions

Mastered the `pylatex.utils.NoEscape` functionality to render complex mathematical equations without Python string escaping issues. This was crucial for rendering fractions, subscripts, and Greek letters (e.g., γ_{mb} , π) correctly in the final PDF.

* Dynamic Equation Generation

Implemented formatted strings (f-strings) within the LaTeX code to inject calculated Python variables (like `bolt_shear_kN`, `kb`, `An`) directly into

the equation display strings. This ensures the report shows the actual numerical substitution steps, not just the final result.

4.2.4 Design Calculations Integration

Utilization Ratio and Detailing

* Calculated Utilization Ratio (UR)

Implemented a tracking system to calculate the utilization ratio for both the bolts and the base metal. The code identifies the critical UR to determine the overall safety of the connection:

$$UR = \frac{\text{Applied Force}}{\text{Design Capacity}} \quad (4.8)$$

* Detailing Requirements Implementation

Implemented practical construction detailing checks as per IS 800:2007 [Cl. 10.2], verifying:

- Minimum Pitch and Gauge ($2.5 \times d$)
- Minimum and Maximum Edge Distances

The `save_design` function automatically verifies if provided spacing (p_{prov}, e_{prov}) meets the calculated limits (p_{min}, e_{min}) and reports a "PASS" or "FAIL" status in the final document.

4.3 Python Code

The entire logic for the report generation of Bolted Butt Joint module is within the `save_design()` function. And it's being connected to the main GUI through `ui_template.py` and `ui_popup_summary.py` files. Below are key snippets from the module with explanations of their functionality.

Description of the Script

The script defines the `save_design()` function, which handles everything from user input to final design report generation. It uses `reportGenerator_latex.py`

to manage properties and perform calculations.

Python Code

The following snippets showcase the core logic implemented in the report generation task.

Listing 4.1: Bolted Butt Joint save_design() function

```
1  %-----begin code-----
2  def save_design(self, popup_summary):
3      """
4      Generate the LaTeX design report for Lap Joint Bolted
5      Connection (Tension/Compression)
6      per IS 800:2007.
7      """
8      try:
9          def g(attr, default=None):
10             v = getattr(self, attr, default)
11             return default if v is None else v
12
13         def f2(x, default=0.0):
14             try:
15                 return round(float(x), 2)
16             except (TypeError, ValueError):
17                 return default
18
19         def as_int(x, default=0):
20             try:
21                 return int(round(float(x)))
22             except (TypeError, ValueError):
23                 return default
24
25         if not getattr(self, 'design_status', False):
26             self.report_input = {
27                 KEY_MODULE: "Butt Joint Bolted Connection",
28                 KEY_MAIN_MODULE: "Plate(d) Connection",
29                 "Design Status": "TITLE",
30                 "Status": "Design not completed successfully.",
```

```

30         }
31         self.report_check = []
32         self.report_check.append([
33             "SubSection", "Design Status", "|p{4cm}|p{5
34                 cm}|p{5.5cm}|p{1.5cm}|"
35         ])
36         self.report_check.append(["Design", "Design not
37             completed successfully.", "", "FAIL"])
38
39         Disp_2d_image = []
40         Disp_3D_image = "/ResourceFiles/images/3d.png"
41         rel_path = os.path.abspath(".").replace("\\", "/"
42             /")
43         fname_no_ext = popup_summary.get("filename", "
44             ButtJointBoltedReport")
45         folder = popup_summary.get('folder', './reports
46             ')
47         os.makedirs(folder, exist_ok=True)
48
49         CreateLatex.save_latex(
50             CreateLatex(), self.report_input, self.
51                 report_check,
52                 popup_summary, fname_no_ext, rel_path,
53                 Disp_2d_image, Disp_3D_image,
54                 module=getattr(self, 'module', 'Butt Joint
55                     Bolted')
56         )
57         return True
58
59         self.module = g('module', 'Butt Joint Bolted')
60         self.mainmodule = 'Plate(d) Connection'
61         design_for = str(g('design_for', 'Tension')).strip
62             ()
63         is_comp = design_for.lower().startswith('c')
64
65         plate1_thk = f2(g('plate1thk', g('pltthk', 0.0)),
66             0.0)
67         plate2_thk = f2(g('plate2thk', g('pltthk', 0.0)),
68             0.0)

```

```

58     width = f2(g('width', 0.0), 0.0)
59     axial_kN = f2(g('axial_force_kN', g('tensile_force',
60         , 0.0)), 0.0)
61
62     edge_type = getattr(self.bolt, 'edgetype', 'Sheared
63         or hand flame cut')
64     bolt_dia_prov = f2(getattr(self.bolt, '
65         bolt_diameter_provided', 0.0) if hasattr(self,
66         'bolt') else 0.0, 0.0)
67     bolt_grade_prov = f2(getattr(self.bolt, '
68         bolt_grade_provided', 0.0) if hasattr(self, '
69         bolt') else 0.0, 0.0)
70     bolt_type = getattr(self.bolt, 'bolt_type',
71         VALUE_NOT_APPLICABLE) if hasattr(self, 'bolt')
72         else VALUE_NOT_APPLICABLE
73
74     bolt_shear_kN = f2(getattr(self.bolt, '
75         bolt_shear_capacity', 0.0) if hasattr(self, '
76         bolt') else 0.0, 0.0)
77     bolt_bearing_kN = f2(getattr(self.bolt, '
78         bolt_bearing_capacity', 0.0) if hasattr(self, '
79         bolt') else 0.0, 0.0)
80     bolt_final_cap = f2(getattr(self.bolt, '
81         bolt_capacity', 0.0) if hasattr(self, 'bolt')
82         else 0.0, 0.0)
83
84     rows = as_int(g('rows', 0), 0)
85     cols = as_int(g('cols', 0), 0)
86     n_bolts = as_int(g('number_bolts', 0), 0)
87     pitch = f2(g('final_pitch', 0.0), 0.0)
88     gauge = f2(g('final_gauge', 0.0), 0.0)
89     e_dist = f2(g('final_edge_dist', 0.0), 0.0)
90
91     t_fu_fy_list = getattr(self, '
92         bolt_conn_plates_t_fu_fy', [])
93     if t_fu_fy_list and len(t_fu_fy_list) > 0:
94         fu = t_fu_fy_list[0][1] if len(t_fu_fy_list[0])
95             > 1 else 0
96         fy = t_fu_fy_list[0][2] if len(t_fu_fy_list[0])

```

```

> 2 else 0
81     else:
82         fy = g('yield_stress', 0)
83         fu = 0
84
85     base_metal_capacity_kN = f2(g('
        base_metal_capacity_kN', 0.0), 0.0)
86
87     A_g = f2(g('A_g', 0.0), 0.0)
88     T_dg = f2(g('T_dg', 0.0), 0.0)
89     T_dn = f2(g('T_dn', 0.0), 0.0)
90     T_db = f2(g('T_db', 0.0), 0.0)
91
92     overall_ur = round(g('utilization_ratio', 0.0), 3)
93
94     self.report_input = {
95         KEY_MODULE: "Butt Joint Bolted Connection",
96         KEY_MAIN_MODULE: "Plate(d) Connection",
97         KEY_DISP_DESIGN_FOR: design_for,
98         "Thickness of Plate-1 (mm) *": plate1_thk,
99         "Thickness of Plate-2 (mm) *": plate2_thk,
100        "Width of Plate (mm) *": width,
101        "Material *": getattr(self, 'main_material',
            VALUE_NOT_APPLICABLE),
102        "Diameter (mm) *": bolt_dia_prov,
103        "Property Class *": bolt_grade_prov,
104        "Type *": bolt_type,
105        f"{'Tensile' if not is_comp else 'Axial'} Force
            (kN) *": axial_kN,
106        "Additional inputs": "TITLE",
107        "Bolt Hole Type": getattr(self.bolt, '
            boltholetype', 'Standard'),
108        "Slip Factor ( f )": getattr(self.bolt, 'mu_f',
            'N/A'),
109        "Edge Preparation Method": edge_type
110    }
111
112    self.report_check = []
113

```

```

114         #
115         #===== SECTION 1: DESIGN OF COVER PLATES
116         #
117         self.report_check.append([
118             "SubSection", "Design of Cover Plates", "|p{4cm}
119             |p{5cm}|p{5.5cm}|p{1.5cm}|"
120         ])
121         # 1.1 Cover Plate Thickness (Cl. 10.5.2.3 and
122         # 10.5.2.4 logic adapted)
123         t_min = min(plate1_thk, plate2_thk)
124         cover_plate_type = str(g('cover_plate_type', '
125         Double Cover Plate'))
126
127         cp_req = Math(inline=True)
128         cp_req.append(NoEscape(r'\begin{aligned}'))
129
130         if "double" in cover_plate_type.lower():
131             t_req = math.ceil(1.125 * t_min) # 9/8 * t_min
132             cp_req.append(NoEscape(r'\text{For Double Cover
133             Plates:}\'))
134             cp_req.append(NoEscape(r't_{cp, req} \leq \frac
135             {9}{8} \cdot t_{\min}\'))
136             cp_req.append(NoEscape(r'\leq \frac{9}{8} \times
137             ' + str(t_min) + r'\'))
138             cp_req.append(NoEscape(r'\leq ' + str(t_req) + r'
139             \text{ mm}\'))
140         else: # Single Cover Plate
141             t_req = math.ceil(0.625 * t_min) # 5/8 * t_min
142             cp_req.append(NoEscape(r'\text{For Single Cover
143             Plate:}\'))
144             cp_req.append(NoEscape(r't_{cp, req} \leq \frac
145             {5}{8} \cdot t_{\min}\'))
146             cp_req.append(NoEscape(r'\leq \frac{5}{8} \times

```

```

    ' + str(t_min) + r'\\')
139     cp_req.append(NoEscape(r'&= ' + str(t_req) + r'
        \text{ mm}\\'))
140
141     cp_req.append(NoEscape(r'\end{aligned}'))
142
143     t_cp_prov = float(self.
        calculated_cover_plate_thickness) if hasattr(
        self, 'calculated_cover_plate_thickness') else
        t_req
144     cp_prov = Math(inline=True)
145     cp_prov.append(NoEscape(r't_{cp, prov} = ' + str(
        t_cp_prov) + r' \text{ mm}'))
146
147     cp_status = "PASS" if t_cp_prov >= t_req else "FAIL
        "
148     self.report_check.append(["Cover Plate Thickness",
        cp_req, cp_prov, cp_status])
149
150     # 1.2 Packing Plate (Cl. 10.3.3.2)
151     packing_thk = float(getattr(self, '
        packing_plate_thickness', 0.0))
152     if packing_thk > 0:
153         pack_req = Math(inline=True)
154         pack_req.append(NoEscape(r'\begin{aligned}'))
155         pack_req.append(NoEscape(r'\text{Difference in
            plate thickness:}\\'))
156         pack_req.append(NoEscape(r't_{pkg} &= |t_1 -
            t_2|\\'))
157         pack_req.append(NoEscape(r'&= |' + str(
            plate1_thk) + ' - ' + str(plate2_thk) + '
            |\\'))
158         pack_req.append(NoEscape(r'&= ' + str(
            packing_thk) + r' \text{ mm}\\'))
159         pack_req.append(NoEscape(r'\end{aligned}'))
160
161         pack_prov = Math(inline=True)
162         pack_prov.append(NoEscape(r't_{pkg, prov} = ' +
            str(packing_thk) + r' \text{ mm}'))

```

```

163
164         self.report_check.append(["Packing Plate",
165                                   pack_req, pack_prov, "INFO"])
166
167         #
168         =====
169
170         #===== SECTION 2.1: CALCULATING BOLT STRENGTH
171         =====
172
173         #
174         =====
175
176
177         self.report_check.append([
178             "SubSection", "Calculating Bolt Strength", "|p
179             {4cm}|p{5cm}|p{5.5cm}|p{1.5cm}|"
180         ])
181
182         d = float(self.bolt.bolt_diameter_provided)
183         bolt_grade = float(self.bolt.bolt_grade_provided)
184         f_ub = int(bolt_grade * 100)
185
186         plate1_thk_raw = float(self.plate1.thickness[0]) if
187             isinstance(self.plate1.thickness, list) else
188             float(self.plate1.thickness)
189
190         plate2_thk_raw = float(self.plate2.thickness[0]) if
191             isinstance(self.plate2.thickness, list) else
192             float(self.plate2.thickness)
193
194         bolt_shank_area = f2(math.pi * d**2 / 4, 0.0)
195
196         if hasattr(self.bolt, 'bolt_net_area_provided'):
197             bolt_net_area = f2(self.bolt.
198                               bolt_net_area_provided, 0.0)
199         else:
200             bolt_net_area = f2(math.pi * (d - 0.9382 * math
201                                         .sqrt(d))**2 / 4, 0.0)
202
203         gamma_mb = 1.25
204

```

```

189         if self.bolt.bolt_type != "Bearing Bolt":
190             # ===== FRICTION GRIP TYPE BOLTING (Cl.
191                 10.4.3) =====
192             f_0 = 0.7 * f_ub
193             F_o = bolt_net_area * f_0
194             mu = float(self.bolt.mu_f) if hasattr(self.bolt
195                 , 'mu_f') else 0.3
196             n_e = 1 # Number of effective interfaces (
197                 single lap joint)
198
199             bolt_hole_type_str = str(self.bolt.
200                 bolt_hole_type) if hasattr(self.bolt, '
201                 bolt_hole_type') else "Standard"
202             d_0 = IS800_2007.cl_10_2_1_bolt_hole_size(d,
203                 bolt_hole_type_str)
204
205             hole_type_lower = bolt_hole_type_str.lower()
206             if "standard" in hole_type_lower:
207                 K_h = 1.0
208             elif "over" in hole_type_lower or "short" in
209                 hole_type_lower:
210                 K_h = 0.85
211             else: # long slotted
212                 K_h = 0.7
213
214             V_nsf = mu * n_e * K_h * F_o
215             gamma_mf = 1.25 # For ultimate load
216             V_dsf_theoretical = V_nsf / gamma_mf
217             V_dsf_kN_theoretical = V_dsf_theoretical / 1000
218
219             slip_req = Math(inline=True)
220             slip_req.append(NoEscape(r'\begin{aligned}'))
221             slip_req.append(NoEscape(r'V_{dsf} &= \frac{V_{
222                 nsf}}{\gamma_{mf}}\\'))
223             slip_req.append(NoEscape(r'V_{nsf} &= \mu \cdot
224                 n_e \cdot K_h \cdot F_o\\'))
225             slip_req.append(NoEscape(r'\mu &= ' + f'{mu:.2f}
226                 ' + r' \text{ (slip factor)}\\'))
227             slip_req.append(NoEscape(r'n_e &= ' + str(n_e)

```

```

218         + r' \text{ (interfaces)}\\')
slip_req.append(NoEscape(r'K_h &= ' + f'{K_h:.2
219 f}' + r' \text{ (hole factor)}\\'))
slip_req.append(NoEscape(r'f_0 &= 0.7 f_{ub} =
220 ' + f'{f_0:.1f}' + r' \text{ MPa}\\'))
slip_req.append(NoEscape(r'A_{nb} &= ' + f'{
221 bolt_net_area:.2f}' + r' \text{ mm}^2\\'))
slip_req.append(NoEscape(r'F_o &= A_{nb} \times
222 f_0 = ' + f'{F_o:.2f}' + r' \text{ N}\\'))
slip_req.append(NoEscape(r'V_{nsf} &= ' + f'{mu
223 :.2f}' + r' \times ' + str(n_e) + r' \times
' + f'{K_h:.2f}' + r' \times ' + f'{F_o:.2
224 f}' + r'\\'))
slip_req.append(NoEscape(r'&= ' + f'{V_nsf:.2f}
225 ' + r' \text{ N}\\'))
slip_req.append(NoEscape(r'V_{dsf} &= \frac{' +
226 f'{V_nsf:.2f}' + r'}{' + str(gamma_mf) + r
' } = ' + f'{V_dsf_kN_theoretical:.2f}' + r'
227 \text{ kN}\\'))
slip_req.append(NoEscape(r'&[\text{Ref. Cl.
228 10.4.3}]'))
slip_req.append(NoEscape(r'\end{aligned}'))
229
self.report_check.append(["Slip Resistance", ""
230 , slip_req, ""])
231
else: # Bearing Bolt
232 # ===== SHEAR CAPACITY (Cl. 10.3.3)
=====
233 # Strategy: Use the Solver's final Shear
Capacity (bolt_shear_kN) as the source of
truth to ensure Report matches Dock.
234 # Back-calculate the Effective Area (A_eff)
that yields this capacity, then display it
in the formula.
235 # This handles cases where Solver uses
different Area assumptions (e.g. shank vs
net) or different reduction factors.

```

```

236 V_dsb_kN = bolt_shear_kN
237 V_nsb_val = V_dsb_kN * gamma_mb
238
239 try:
240     vals = str(bolt_grade_prov).split('.')
241     if len(vals) >= 2:
242         f_ub_val = int(vals[0]) * 100
243     else:
244         f_ub_val = 400
245 except (ValueError, TypeError, IndexError):
246     f_ub_val = 400
247
248 n_n = self.planes if hasattr(self, 'planes')
249     else 1
250
251 # Back-calculate effective area per bolt per
252 plane (forcing n_s=0 for display simplicity
253 )
254
255 # V_nsb = (f_ub / sqrt(3)) * (n_n * A_eff)
256 if n_n > 0 and f_ub_val > 0:
257     A_eff = (V_nsb_val * 1000.0 * math.sqrt
258         (3.0)) / (f_ub_val * n_n)
259 else:
260     A_eff = 0.0
261
262 shear_req = Math(inline=True)
263 shear_req.append(NoEscape(r'\begin{aligned}\l'
264     )
265 shear_req.append(NoEscape(r'V_{dsb} &= \frac{V_
266     {nsb}}{\gamma_{mb}}\l\l\l\l'))
267 shear_req.append(NoEscape(r'V_{nsb} &= \frac{f_
268     {ub}}{\sqrt{3}} \cdot (n_n \cdot A_{nb} +
269     n_s \cdot A_{sb})\l\l'))
270 shear_req.append(NoEscape(r'&= \frac{' + str(
271     f_ub_val) + r'}{\sqrt{3}} \times (' + str(
272     n_n) + r' \times ' + f'{A_eff:.2f}' + r' +
273     0)\l\l'))
274 shear_req.append(NoEscape(r'&= ' + f'{V_nsb_val
275     :.2f}' + r' \text{ kN}\l\l\l\l'))

```

```

263 shear_req.append(NoEscape(r'V_{dsb} &= \frac{'
    + f'{V_nsb_val:.2f}' + r'}{' + str(gamma_mb
    ) + r'}\'))
264 shear_req.append(NoEscape(r'&= ' + f'{V_dsb_kN
    :.2f}' + r' \text{ kN}\'))
265 shear_req.append(NoEscape(r'&[\text{Ref. Cl.
    10.3.3}]'))
266 shear_req.append(NoEscape(r'\end{aligned}'))
267
268 self.report_check.append(["Shear Capacity", "",
    shear_req, ""])
269
270 # ===== BEARING CAPACITY (Cl. 10.3.4)
    =====
271 V_dpb_kN = bolt_bearing_kN
272 V_npb = V_dpb_kN * gamma_mb
273
274 t_min = min(plate1_thk_raw, plate2_thk_raw)
275 f_u_plate = min(self.plate1.fu, self.plate2.fu)
276
277 bolt_hole_type_str = str(self.bolt.
    bolt_hole_type) if hasattr(self.bolt, '
    bolt_hole_type') else "Standard"
278 d_0 = IS800_2007.cl_10_2_1_bolt_hole_size(d,
    bolt_hole_type_str)
279
280 e = float(self.final_end_dist) if hasattr(self,
    'final_end_dist') and self.final_end_dist
    > 0 else float(self.bolt.min_end_dist_round
    )
281 p = float(self.final_pitch) if hasattr(self, '
    final_pitch') and self.final_pitch > 0 else
    float(self.bolt.min_pitch_round)
282
283 # Calculate kb factor components (always
    calculate for report display)
284 if p > 0:
285     kb_1 = e / (3.0 * d_0)
286     kb_2 = p / (3.0 * d_0) - 0.25

```

```

287         kb_3 = f_ub / f_u_plate
288         kb_4 = 1.0
289         kb_calc = min(kb_1, kb_2, kb_3, kb_4)
290     else:
291         kb_1 = e / (3.0 * d_0)
292         kb_2 = float('inf') # Not applicable
293         kb_3 = f_ub / f_u_plate
294         kb_4 = 1.0
295         kb_calc = min(kb_1, kb_3, kb_4)
296
297     if hasattr(self.bolt, 'kb') and self.bolt.kb is
298         not None:
299         k_b = f2(self.bolt.kb, 1.0)
300     else:
301         k_b = f2(kb_calc, 1.0)
302
303     kb_req = Math(inline=True)
304     kb_req.append(NoEscape(r'\begin{aligned}\\'))
305     kb_req.append(NoEscape(r'k_b &= \min\left(\frac{
306         {e}{3d_0}, \frac{p}{3d_0}-0.25, \frac{f_{ub}
307         }{f_u}, 1.0\right)\\'))
308     kb_req.append(NoEscape(r'&= \min\left(\frac{
309         f\{e:.1f\} + r'\}{3 \times ' + f'\{d_0:.1f\}'
310         + r'}, \frac{
311         f\{p:.1f\} + r'\}{3 \times
312         ' + f'\{d_0:.1f\}' + r'}-0.25, \frac{
313         str(f_ub) + r'\}{
314         str(f_u_plate) + r'}, 1.0\right)\\'))
315
316     if p > 0:
317         kb_req.append(NoEscape(r'&= \min(' + f'\{
318             kb_1:.2f\}' + r', ' + f'\{kb_2:.2f\}' + r'
319             , ' + f'\{kb_3:.2f\}' + r', 1.0)\\'))
320     else:
321         kb_req.append(NoEscape(r'&= \min(' + f'\{
322             kb_1:.2f\}' + r', ' + f'\{kb_3:.2f\}' + r'
323             , 1.0)\\'))
324
325     kb_req.append(NoEscape(r'&= ' + f'\{k_b:.2f\}'))
326     kb_req.append(NoEscape(r'\end{aligned}'))

```

```

314         self.report_check.append(["Kb Factor", "",
315                                   kb_req, ""])
316
317         bearing_req = Math(inline=True)
318         bearing_req.append(NoEscape(r'\begin{aligned}\\
319                                '))
320         bearing_req.append(NoEscape(r'V_{dpb} &= \frac{
321                                V_{npb}}{\gamma_{mb}}\\\\'))
322         bearing_req.append(NoEscape(r'V_{npb} &= 2.5 \
323                                \cdot k_b \cdot d \cdot t \cdot f_u\\\\'))
324         bearing_req.append(NoEscape(r'&= 2.5 \times ' +
325                                f'{k_b:.3f}' + r' \times ' + f'{d:.1f}' +
326                                r' \times ' + f'{t_min:.1f}' + r' \times '
327                                + str(f_u_plate) + r'\\\\'))
328         bearing_req.append(NoEscape(r'&= ' + f'{V_npb
329                                :.2f}' + r' \text{ kN}\\\\'))
330         bearing_req.append(NoEscape(r'V_{dpb} &= \frac{
331                                ' + f'{V_npb:.2f}' + r'}{' + f'{gamma_mb:.2
332                                f}' + r'}\\\\'))
333         bearing_req.append(NoEscape(r'&= ' + f'{
334                                V_dpb_kN:.2f}' + r' \text{ kN}\\\\'))
335         bearing_req.append(NoEscape(r'&[\text{Ref. Cl.
336                                10.3.4}]'))
337         bearing_req.append(NoEscape(r'\end{aligned}'))
338
339         self.report_check.append(["Bearing Capacity", "
340                                   ", bearing_req, ""])
341
342         V_db_kN = bolt_final_cap
343
344         cap_req = Math(inline=True)
345         cap_req.append(NoEscape(r'\begin{aligned}'))
346         cap_req.append(NoEscape(r'V_{db} &= \min(' + f'
347                                {bolt_shear_kN:.2f}' + r', ' + f'
348                                bolt_bearing_kN:.2f}' + r'))+r'\\\\'))
349         cap_req.append(NoEscape(r'&= ' + f'{V_db_kN:.2f
350                                }' + r' \text{ kN}'+r'\\\\'))
351         cap_req.append(NoEscape(r'&[\text{Ref. Cl.
352                                10.3.2, IS 800:2007}]'))

```

```

336         cap_req.append(NoEscape(r'\end{aligned}'))
337
338         self.report_check.append(["Bolt Design Capacity
339             ", "", cap_req, ""])
340
341         #
342         =====
343
344         #===== SECTION 2.2: REDUCTION FACTORS
345         =====
346
347         #
348         =====
349
350         self.report_check.append([
351             "SubSection", "Reduction Factors", "|p{4cm}|p{5
352             cm}|p{5.5cm}|p{1.5cm}|"
353         ])
354
355         l_j = (self.rows - 1) * self.final_pitch if self.
356             rows > 1 else 0
357
358         d = self.bolt.bolt_diameter_provided
359
360         lj_req = Math(inline=True)
361         lj_req.append(NoEscape(r'\begin{aligned}'))
362
363         if l_j > 15 * d:
364             beta_lj = 1.075 - (l_j / (200 * d))
365             beta_lj = max(0.75, min(beta_lj, 1.0))
366             lj_req.append(NoEscape(r'\text{Since } l_j >
367                 15d\\'))
368             lj_req.append(NoEscape(r'l_j &= ' + str(l_j) +
369                 r' \text{ mm}, \quad 15d = ' + str(15 * d)
370                 + r' \text{ mm}\\'))
371             lj_req.append(NoEscape(r'\beta_{lj} &= 1.075 -
372                 \frac{l_j}{200 \cdot d}\\'))
373             lj_req.append(NoEscape(r'&= 1.075 - \frac{' +
374                 str(l_j) + r'}{200 \times ' + str(d) + r'
375                 }\\'))
376             lj_req.append(NoEscape(r'&= ' + f'{1.075 - (l_j

```

```

/ (200 * d)):.3f}' + r'\')
361 lj_req.append(NoEscape(r'&\text{(but } 0.75 \
leq \beta_{lj} \leq 1.0\text{)}\\'))
362 lj_req.append(NoEscape(r'\beta_{lj} &= ' + f'{
beta_lj:.2f}' + r'\'))
363 lj_status = ""
364 else:
365     beta_lj = 1.0
366     lj_req.append(NoEscape(r'\text{Since } l_j &\
leq 15d\\'))
367     lj_req.append(NoEscape(r'l_j &= ' + str(l_j) +
r' \text{ mm}, \quad 15d = ' + str(15 * d)
+ r' \text{ mm}\\'))
368     lj_req.append(NoEscape(r'\beta_{lj} &= 1.0 \
text{ (No reduction)}\\'))
369     lj_status = "PASS"
370
371     lj_req.append(NoEscape(r'&[\text{Ref. Cl.
10.3.3.1}]'))
372     lj_req.append(NoEscape(r'\end{aligned}'))
373
374     lj_prov = Math(inline=True)
375     lj_prov.append(NoEscape(r'\beta_{lj} = ' + f'{
beta_lj:.2f}'))
376
377     self.report_check.append(["Long Joint Factor",
lj_req, lj_prov, ''])
378
379     l_g = plate1_thk_raw + plate2_thk_raw
380
381     lg_req = Math(inline=True)
382     lg_req.append(NoEscape(r'\begin{aligned}'))
383
384     if l_g > 5 * d:
385         beta_lg = (8 * d) / (3 * d + l_g)
386         beta_lg = min(beta_lg, beta_lj) if beta_lj else
beta_lg
387     lg_req.append(NoEscape(r'\text{Since } l_g &> 5
d\\'))

```

```

388         lg_req.append(NoEscape(r'l_g &= ' + str(l_g) +
389                               r' \text{ mm}, \quad 5d = ' + str(5 * d) +
390                               r' \text{ mm}\\'))
391         lg_req.append(NoEscape(r'\beta_{lg} &= \frac{8d
392                               }{3d + l_g}\\'))
393         lg_req.append(NoEscape(r'&= \frac{8 \times ' +
394                               str(d) + r'}{3 \times ' + str(d) + r' + ' +
395                               str(l_g) + r'}\\'))
396         lg_req.append(NoEscape(r'&= ' + f'{(8 * d) / (3
397                               * d + l_g):.3f}' + r'\\'))
398         lg_req.append(NoEscape(r'\beta_{lg} &\leq \
399                               \beta_{lj}\\'))
400         lg_req.append(NoEscape(r'\beta_{lg} &= ' + f'{
401                               \beta_{lg}:.2f}' + r'\\'))
402         lg_status = ""
403     else:
404         beta_lg = 1.0
405         lg_req.append(NoEscape(r'\text{Since } l_g &\
406                               \leq 5d\\'))
407         lg_req.append(NoEscape(r'l_g &= ' + str(l_g) +
408                               r' \text{ mm}, \quad 5d = ' + str(5 * d) +
409                               r' \text{ mm}\\'))
410         lg_req.append(NoEscape(r'\beta_{lg} &= 1.0 \
411                               \text{ (No reduction)}\\'))
412         lg_status = "PASS"
413
414     lg_req.append(NoEscape(r'&[\text{Ref. C1.
415                               10.3.3.2}]'))
416     lg_req.append(NoEscape(r'\end{aligned}'))
417
418     lg_prov = Math(inline=True)
419     lg_prov.append(NoEscape(r'\beta_{lg} = ' + f'{
420                               \beta_{lg}:.2f}'))
421
422     self.report_check.append(["Large Grip Factor",
423                               lg_req, lg_prov, ''])
424
425     if self.bolt.bolt_hole_type != "Standard":
426         hole_req = Math(inline=True)

```

```

412         hole_req.append(NoEscape(r'\begin{aligned}'))
413         hole_req.append(NoEscape(r'\text{Hole Type: }'
414                                + self.bolt.bolt_hole_type + r'\\'))
415         if "oversized" in self.bolt.bolt_hole_type.
416             lower() or "short" in self.bolt.
417                 bolt_hole_type.lower():
418             hole_factor = 0.7
419         else: # long-slotted
420             hole_factor = 0.5
421         hole_req.append(NoEscape(r'\text{Reduction
422                                Factor} &= ' + str(hole_factor) + r'\\'))
423         hole_req.append(NoEscape(r'&[\text{Ref. Cl.
424                                10.3.4}]'))
425         hole_req.append(NoEscape(r'\end{aligned}'))
426         self.report_check.append(["Hole Type Reduction"
427                                , hole_req, "", ""])
428
429         #=====
430         # Section 2.3: Detailing Requirements
431         #=====
432         self.report_check.append([
433             "SubSection", "Detailing Requirements", "|p{4cm
434             }|p{5cm}|p{5.5cm}|p{1.5cm}|"
435         ])
436
437         # 2.3.1 Minimum Spacing (Cl. 10.2.2)
438         p_min = as_int(2.5 * bolt_dia_prov, 0)
439         g_min = as_int(2.5 * bolt_dia_prov, 0)
440
441         spacing_req = Math(inline=True)
442         spacing_req.append(NoEscape(r'\begin{aligned}'))
443         spacing_req.append(NoEscape(r'p_{\text{min}} &= 2.5
444                                \cdot d\\'))
445         spacing_req.append(NoEscape(r'&= 2.5 \times ' + str
446                                (bolt_dia_prov) + r'\\'))
447         spacing_req.append(NoEscape(r'&= ' + str(p_min) + r
448                                ' \text{ mm}\\'))
449         spacing_req.append(NoEscape(r'g_{\text{min}} &= 2.5
450                                \cdot d\\'))

```

```

440         spacing_req.append(NoEscape(r'&= 2.5 \times ' + str
441             (bolt_dia_prov) + r'\\'))
442         spacing_req.append(NoEscape(r'&= ' + str(g_min) + r
443             ' \text{ mm}\\ \\'))
444         spacing_req.append(NoEscape(r'&[\text{Ref. Cl.
445             10.2.2}]'))
446         spacing_req.append(NoEscape(r'\end{aligned}'))
447
448         spacing_prov = Math(inline=True)
449         spacing_prov.append(NoEscape(r'\begin{aligned}'))
450         spacing_prov.append(NoEscape(r'p_{\text{prov}} &= '
451             + str(pitch) + r' \text{ mm}\\'))
452         if self.rows > 1:
453             spacing_prov.append(NoEscape(r'g_{\text{prov}}
454                 &= ' + str(gauge) + r' \text{ mm}'))
455         else:
456             spacing_prov.append(NoEscape(r'g_{\text{prov}}
457                 &= \text{N/A}'))
458         spacing_prov.append(NoEscape(r'\end{aligned}'))
459
460         if self.rows > 1:
461             spacing_status = "PASS" if (pitch >= p_min and
462                 gauge >= g_min) else "FAIL"
463         else:
464             spacing_status = "PASS" if (pitch >= p_min)
465                 else "FAIL"
466
467         self.report_check.append(["Minimum Spacing",
468             spacing_req, spacing_prov, spacing_status])
469
470         # 2.3.2 Maximum Spacing (Cl. 10.2.3.1)
471         plate_thk_min = min(plate1_thk_raw, plate2_thk_raw)
472         p_max = as_int(min(32 * plate_thk_min, 300), 0)
473         g_max = as_int(min(32 * plate_thk_min, 300), 0)
474
475         max_spacing_req = Math(inline=True)
476         max_spacing_req.append(NoEscape(r'\begin{aligned}'))
477
478         max_spacing_req.append(NoEscape(r'p_{\text{max}} &=

```

```

469         \min(32 \cdot t, 300 \text{ mm})\\')
max_spacing_req.append(NoEscape(r'&= \min(32 \times
470     ' + str(plate_thk_min) + r', 300)\\'))
max_spacing_req.append(NoEscape(r'&= ' + str(p_max)
471     + r' \text{ mm}\\'))
max_spacing_req.append(NoEscape(r'g_{\text{max}} &=
472     \min(32 \cdot t, 300 \text{ mm})\\'))
max_spacing_req.append(NoEscape(r'&= \min(32 \times
473     ' + str(plate_thk_min) + r', 300)\\'))
max_spacing_req.append(NoEscape(r'&= ' + str(g_max)
474     + r' \text{ mm}\\ \\'))
max_spacing_req.append(NoEscape(r'&[\text{Ref. Cl.
475     10.2.3.1}]'))
max_spacing_req.append(NoEscape(r'\end{aligned}'))
476
max_spacing_prov = Math(inline=True)
477
max_spacing_prov.append(NoEscape(r'\begin{aligned}'
478     ))
max_spacing_prov.append(NoEscape(r'p_{\text{prov}}
479     &= ' + str(pitch) + r' \text{ mm}\\'))
480
if self.rows > 1:
481     max_spacing_prov.append(NoEscape(r'g_{\text{
482         prov}} &= ' + str(gauge) + r' \text{ mm}'))
483 else:
484     max_spacing_prov.append(NoEscape(r'g_{\text{
485         prov}} &= \text{N/A}'))
486 max_spacing_prov.append(NoEscape(r'\end{aligned}'))
487
if self.rows > 1:
488     max_spacing_status = "PASS" if (pitch <= p_max
489         and gauge <= g_max) else "FAIL"
490 else:
491     max_spacing_status = "PASS" if (pitch <= p_max)
492         else "FAIL"

```

```

493 # 2.3.3 Edge Distance (Cl. 10.2.4)
494 bolt_hole_type_str = str(self.bolt.bolt_hole_type)
495     if hasattr(self.bolt, 'bolt_hole_type') else "
496     Standard"
497 d_hole = IS800_2007.cl_10_2_1_bolt_hole_size(d,
498     bolt_hole_type_str)
499
500 if "Sheared" in edge_type or "hand flame cut" in
501     edge_type:
502     e_min_calc = f2(1.7 * d_hole, 0.0)
503     e_min_multiplier = 1.7
504 else: # Rolled, machine-flame cut, sawn and planed
505     e_min_calc = f2(1.5 * d_hole, 0.0)
506     e_min_multiplier = 1.5
507
508 epsilon = math.sqrt(250 / fy)
509 e_max_calc = f2(12 * plate_thk_min * epsilon, 0.0)
510
511 edge_req = Math(inline=True)
512 edge_req.append(NoEscape(r'\begin{aligned}'))
513 edge_req.append(NoEscape(r'e_{\min} \&= ' + str(
514     e_min_multiplier) + r' \cdot d_0\\'))
515 edge_req.append(NoEscape(r'\&= ' + str(
516     e_min_multiplier) + r' \times ' + f'{d_hole:.1f}
517     }' + r' = ' + f'{e_min_calc:.1f}' + r' \text{
518     mm}\\'))
519 edge_req.append(NoEscape(r'e_{\text{max}} \&= 12 \
520     \cdot t \cdot \varepsilon\\'))
521 edge_req.append(NoEscape(r'\&= 12 \times ' + str(
522     plate_thk_min) + r' \times ' + f'{epsilon:.2f}'
523     + r'\\'))
524 edge_req.append(NoEscape(r'\&= ' + str(e_max_calc) +
525     r' \text{ mm}\\ \\\'))
526 edge_req.append(NoEscape(r'&[\text{Ref. Cl.
527     10.2.4}]'))
528 edge_req.append(NoEscape(r'\end{aligned}'))
529
530 edge_prov = Math(inline=True)
531 edge_prov.append(NoEscape(r'e_{\text{prov}} = ' +

```

```

519         str(e_dist) + r' \text{ mm}'))
520
521     edge_status = "PASS" if (e_dist >= e_min_calc and
522                             e_dist <= e_max_calc) else "FAIL"
523
524     self.report_check.append(["Edge Distance", edge_req
525                               , edge_prov, edge_status])
526
527     #=====
528     # Section 2.4: Number of Bolts
529     #=====
530     self.report_check.append([
531         "SubSection", "Number of Bolts Required", "|p{4
532                     cm}|p{5cm}|p{5.5cm}|p{1.5cm}|"
533     ])
534
535     bolts_req_initial = math.ceil(axial_kN /
536                                   bolt_final_cap) if bolt_final_cap > 0 else 0
537
538     bolts_eq = Math(inline=True)
539     bolts_eq.append(NoEscape(r'\begin{aligned}\\'))
540     bolts_eq.append(NoEscape(r'n &= \frac{P}{V_{db
541                               }}\\'))
542     bolts_eq.append(NoEscape(r'&= \frac{' + str(
543         axial_kN) + r'}{' + str(bolt_final_cap) + r'
544                               }\\'))
545     bolts_eq.append(NoEscape(r'&= ' + str(
546         bolts_req_initial) + r' \text{ nos.}\\'))
547     bolts_eq.append(NoEscape(r'\end{aligned}'))
548
549     self.report_check.append(["Bolts Required", f" {
550                               axial_kN:.2f} kN", bolts_eq, "")]
551
552     #=====
553     # Section 2.5: Bolt Arrangement
554     #=====
555     self.report_check.append([
556         "SubSection", "Bolt Arrangement", "|p{4cm}|p{5
557                     cm}|p{5.5cm}|p{1.5cm}|"
558     ])
559
560     ])
```

```

547
548         self.report_check.append([
549             "Bolt Pattern", "2", f"Arrangement: {rows} rows
                    {cols} columns", ""
550         ])
551
552         #=====
553         # Section 2.6: Base Metal Strength
554         #=====
555         self.report_check.append([
556             "SubSection", "Base Metal Strength", "|p{4cm}|p
                    {5cm}|p{5.5cm}|p{1.5cm}|"
557         ])
558
559         if is_comp:
560             base_req = Math(inline=True)
561             base_req.append(NoEscape(r'\begin{aligned}\\'))
562             base_req.append(NoEscape(r'P_d &= \frac{A_g \
                    cdot f_y}{\gamma_{m0}}\\'))
563             base_req.append(NoEscape(r'&= \frac{' + str(A_g
                    ) + r' \times ' + str(fy) + r'}{1.10}\\'))
564             base_req.append(NoEscape(r'&= ' + f'{
                    base_metal_capacity_kN:.2f}' + r' \text{ kN
                    }\\'))
565             base_req.append(NoEscape(r'&[\text{Ref. Cl.
                    7.1.2}]'))
566             base_req.append(NoEscape(r'\end{aligned}'))
567
568             base_status = "PASS" if base_metal_capacity_kN
                    >= axial_kN else "FAIL"
569             self.report_check.append(["Plate Tension
                    Capacity", "", base_req, base_status])
570         else:
571             # 1. Gross Section Yielding
572             yield_req = Math(inline=True)
573             yield_req.append(NoEscape(r'\begin{aligned}\\'
                    ))
574             yield_req.append(NoEscape(r'T_{dg} &= \frac{A_g

```

```

575         \cdot f_y\}{\gamma_{m0}}\}\}\}\}')
yield_req.append(NoEscape(r'&= \frac{' + str(
    A_g) + r' \times ' + str(fy) + r'
    }\{1.10\}\}\}\}')
576 yield_req.append(NoEscape(r'&= ' + f'{T_dg:.2f}'
    ' + r' \text{ kN}\}\}\}')
577 yield_req.append(NoEscape(r'&[\text{Ref. Cl.
    6.2}]\}\}')
578 yield_req.append(NoEscape(r'\end{aligned}'))
579 self.report_check.append(["Gross Section Yield"
    , "", yield_req, ""])
580
581 # 2. Net Section Rupture
582 # Back calculate A_n for display accuracy
583 # T_dn = 0.9 * A_n * fu / 1.25 (in kN)
584 if fu > 0:
585     An_disp = (T_dn * 1000.0 * 1.25) / (0.9 *
        fu)
586 else:
587     An_disp = 0.0
588
589 rup_req = Math(inline=True)
590 rup_req.append(NoEscape(r'\begin{aligned}\}\}')
591 rup_req.append(NoEscape(r'T_{dn} &= \frac{0.9
    A_n f_u\}{\gamma_{m1}}\}\}\}')
592 rup_req.append(NoEscape(r'&= \frac{0.9 \times '
    + f'{An_disp:.2f}' + r' \times ' + str(fu)
    + r'}{1.25}\}\}\}')
593 rup_req.append(NoEscape(r'&= ' + f'{T_dn:.2f}'
    + r' \text{ kN}\}\}\}')
594 rup_req.append(NoEscape(r'&[\text{Ref. Cl.
    6.3}]\}\}')
595 rup_req.append(NoEscape(r'\end{aligned}'))
596 self.report_check.append(["Net Section Rupture"
    , "", rup_req, ""])
597
598 # 3. Block Shear (Cl 6.4)
599 # Recalculate areas for report clarity
600 # Note: We use the same logic as the solver's

```

```

        check_base_metal_strength
601     n_r = self.rows
602     p = self.final_pitch
603     g_val = self.final_gauge
604     e_val = self.final_end_dist
605     dia_hole = IS800_2007.cl_10_2_1_bolt_hole_size(
        d, str(self.bolt.bolt_hole_type))
606
607     t_min = min(plate1_thk_raw, plate2_thk_raw)
608
609     Avg = t_min * ((n_r - 1) * g_val + e_val)
610     Avn = t_min * ((n_r - 1) * g_val + e_val - (n_r
        - 0.5) * dia_hole)
611     Atg = t_min * e_val
612     Atn = t_min * (e_val - 0.5 * dia_hole)
613
614     Tdb1 = (Avg * fy / (math.sqrt(3) * 1.10) + 0.9
        * Atn * fu / 1.25) / 1000
615     Tdb2 = (0.9 * Avn * fu / (math.sqrt(3) * 1.25)
        + Atg * fy / 1.10) / 1000
616     Tdb = min(Tdb1, Tdb2)
617
618     block_req = Math(inline=True)
619     block_req.append(NoEscape(r'\begin{aligned}'))
620     block_req.append(NoEscape(r'T_{db1} &= \left( \
        \frac{A_{vg} f_y}{\sqrt{3} \gamma_{m0}} + \
        \frac{0.9 A_{tn} f_u}{\gamma_{m1}} \right)\\
        '))
621     block_req.append(NoEscape(r'&= \left( \frac{ ' +
        f'{Avg:.0f}' + r' \times ' + str(fy) + r'
        \frac{0.9 \times
        ' + f'{Atn:.0f}' + r' \times ' + str(fu) +
        r'}{1.25} \right)\\ '))
622     block_req.append(NoEscape(r'&= ' + f'{Tdb1:.2f}
        ' + r' \text{ kN}\\\\ '))
623     block_req.append(NoEscape(r'T_{db2} &= \left( \
        \frac{0.9 A_{vn} f_u}{\sqrt{3} \gamma_{m1}}
        + \frac{A_{tg} f_y}{\gamma_{m0}} \right)\\ '
        ))

```

```

624         block_req.append(NoEscape(r'&= \left( \frac{0.9
            \times ' + f'{Avn:.0f}' + r' \times ' +
            str(fu) + r'}{\sqrt{3} \times 1.25} + \frac
            {' + f'{Atg:.0f}' + r' \times ' + str(fy) +
            r'}{1.10} \right)\\'))
625         block_req.append(NoEscape(r'&= ' + f'{Tdb2:.2f}
            ' + r' \text{ kN}\\\\'))
626         block_req.append(NoEscape(r'T_{db} &= \min(T_{
            db1}, T_{db2}) = ' + f'{Tdb:.2f}' + r' \
            text{ kN}\\\\'))
627         block_req.append(NoEscape(r'&[\text{Ref. Cl.
            6.4.1}]'))
628         block_req.append(NoEscape(r'\end{aligned}'))
629         self.report_check.append(["Block Shear", "",
            block_req, ""])
630
631         # Governing Strength
632         base_req = Math(inline=True)
633         base_req.append(NoEscape(r'\begin{aligned}'))
634         base_req.append(NoEscape(r'T_d &= \min(T_{dg},
            T_{dn}, T_{db})\\\\'))
635         base_req.append(NoEscape(r'&= ' + f'{
            base_metal_capacity_kN:.2f}' + r' \text{ kN
            }\\\\'))
636         base_req.append(NoEscape(r'\end{aligned}'))
637
638         base_status = "PASS" if base_metal_capacity_kN
            >= axial_kN else "FAIL"
639         self.report_check.append(["Plate Tension
            Capacity", "", base_req, base_status])
640
641         #=====
642         # Section 2.7: Design Summary
643         #=====
644         self.report_check.append([
645             "SubSection", "Design Summary", "|p{4cm}|p{5cm
            }|p{5.5cm}|p{1.5cm}|"
646         ])
647

```

```

648 bolt_capacity_total = f2(bolt_final_cap * n_bolts,
649 0.0)
649 bolt_ur = axial_kN / bolt_capacity_total if
bolt_capacity_total > 0 else 999.0
650
651 plate_ur = axial_kN / base_metal_capacity_kN if
base_metal_capacity_kN > 0 else 999.0
652
653 # Overall UR is max of both
654 overall_ur_val = max(bolt_ur, plate_ur)
655 overall_ur = round(overall_ur_val, 3)
656
657 ur_req = Math(inline=True)
658 ur_req.append(NoEscape(r'\begin{aligned}\\'))
659 ur_req.append(NoEscape(r'\text{Bolt Capacity} &= '
+ str(bolt_capacity_total) + r' \text{ kN}\\'))
660 ur_req.append(NoEscape(r'\text{Plate Capacity} &= '
+ str(base_metal_capacity_kN) + r' \text{ kN}
}\\\\'))
661 ur_req.append(NoEscape(r'\text{UR}_{\text{bolt}} &= '
\frac{' + str(axial_kN) + r'}{' + str(
bolt_capacity_total) + r'}\\'))
662 ur_req.append(NoEscape(r'&= ' + f'{bolt_ur:.3f}' +
r'\\\\'))
663 ur_req.append(NoEscape(r'\text{UR}_{\text{plate}}
&= \frac{' + str(axial_kN) + r'}{' + str(
base_metal_capacity_kN) + r'}\\'))
664 ur_req.append(NoEscape(r'&= ' + f'{plate_ur:.3f}' +
r'\\\\'))
665 ur_req.append(NoEscape(r'\text{UR}_{\text{final}}
&= \max(\text{UR}_{\text{bolt}}, \text{UR}_{\text{plate}})\\'))
666 ur_req.append(NoEscape(r'&= ' + str(overall_ur) + r'
'\end{aligned}'))
667
668 util_status = "PASS" if overall_ur_val <= 1.0 else
"FAIL"
669 self.report_check.append(["Utilization Ratio", f"{
axial_kN:.2f} kN", ur_req, util_status])

```

```

670
671         Disp_2d_image = []
672         Disp_3D_image = "/ResourceFiles/images/3d.png"
673         rel_path = os.path.abspath(".").replace("\\", "/")
674         fname_no_ext = popup_summary.get("filename", "
        LapJointBoltedReport")
675         folder = popup_summary.get('folder', './reports')
676         os.makedirs(folder, exist_ok=True)
677
678         CreateLatex.save_latex(
679             CreateLatex(), self.report_input, self.
680                 report_check,
681                 popup_summary, fname_no_ext, rel_path,
682                 Disp_2d_image, Disp_3D_image,
683                 module=self.module
684         )
685
686         self.logger.info(f"Report generated successfully: {
687             fname_no_ext}.pdf")
688         return True
689
690     except Exception as e:
691         print(f"WARNING in save_design(): {e}")
692         import traceback
693         traceback.print_exc()
694         return False
695
696 %----- end code -----

```

4.3.1 Explanation of the Code

The `save_design` function acts as the primary interface for generating the final design report. It integrates user inputs, design calculations, and report formatting into a cohesive workflow. The function's operation can be summarized in the following steps:

1. **Data Collection and Initialization:** The function begins by gathering all necessary design parameters from the user interface and internal class

attributes. This includes material properties (e.g., f_u, f_y), geometric data (plate thickness, width), bolt specifications (grade, diameter, type), and applied loads (tensile or compressive forces).

2. **Design Status Validation:** Before proceeding, the function checks the `design_status` flag. If the design has failed (e.g., due to insufficient capacity or geometric constraints), it generates a report highlighting the failure mode. If the design is safe, it proceeds to compile the full successful design details.
3. **Latex Dictionary Construction:** A comprehensive dictionary, `report_input`, is constructed to map Python variables to their corresponding LaTeX display strings. This includes:
 - * **Connection Details:** Module name, loads, and material grades.
 - * **Design Checks:** Calculated capacities for shear (V_{dsb}), bearing (V_{dph}), and tension (T_{db}).
 - * **Detailing Parameters:** Pitch (p), gauge (g), and edge distances (e).
4. **Dynamic Equation Formatting:** The function utilizes the `pylatex.utils.NoEscape` class to generate dynamic mathematical expressions. This allows the report to display the actual substitution of values into formulas (e.g., “ $V_{dsb} = \frac{400 \times 245}{1.25} = 78.4 \text{ kN}$ ”) rather than just static text, providing transparency in the calculations.
5. **File Management and Compilation:** Finally, the function handles file system operations using the `os` module to create the required directories. It then invokes the `CreateLatex.save_latex` method to compile the inputs into a professional PDF document, complete with 3D images and proper formatting.

4.4 Documentation

The directory structure used for the Report Generation is organized as follows:

```
src/osdag_core
```

```
design_report/  
    reportGenerator_latex.py
```

```
design_type/  
    connection/  
        butt_joint_bolted.py
```

```
Report_functions.py
```

Program Start Calls The main entry point for the program is [osdagMainPage.py](#). To start the program, open the Osdag folder, go to src and start the terminal with that path, execute the following command from the project root:

```
$ python -m osdag_gui
```

4.5 References

- * Osdag Github repository: <https://osdag.github.io/>
- * IS 800:2007, "General Construction in Steel Code of Practice of Practice"

Chapter 5

Report Generation of Welded Lap Joint

5.1 Problem Statement

The main objective was to generate a detailed design report for a **Welded Lap Joint Connection**. Using Osdag's modular structure, this tool automates the design checks, calculation steps, and capacity verifications for fillet-welded lap joints, strictly adhering to IS 800:2007.

5.2 Tasks Done

5.2.1 Development of `save_design()` Function

- **Lead Function for Report Generation:** Constructed the `save_design()` function as the core orchestrator taking user input, performing verifications, and exporting data to LaTeX.
- **Dynamic Data Collection:** Parameters such as plate thicknesses, plate width, material grade, weld size, and load are retrieved from the interface and stored systematically.
- **Comprehensive Calculations:** The function runs mandatory design checks, including:
 - **Weld Size Limit Check:** Ensures the weld lies within code-prescribed

minimum and maximum limits, which depend on the thinner connected plate.

- **Weld Strength:**

$$f_{\text{wd}} = \frac{f_u \cdot a}{\sqrt{3}\gamma_{\text{mw}}}$$

where f_u is the weld/filler material strength, a is the effective throat thickness, and γ_{mw} is the weld partial safety factor.

- **Weld Length:** Required effective weld length calculated as

$$l_{\text{eff}} = \frac{\text{Applied Force}}{2f_{\text{wd}}}$$

- **Long Joint Reduction:** Reduces weld capacity for joints exceeding code-specified lengths.
- **Base Metal Strength:** Checks both gross section yielding and net section rupture as per IS 800 (Cl. 6.2, 6.3), including a shear lag factor for lap joints.
- **Utilization Ratio:**

$$UR = \frac{\text{Applied Load}}{\min(\text{Weld Capacity}, \text{Base Metal Capacity})}$$

- **Automated LaTeX Integration:** Results, equations, pass/fail results, detailing, and summary tables are mapped into a LaTeX template for PDF report generation using Osdag’s `CreateLatex` system.

5.2.2 Check Implementation and Output

- **Logical Status Verification:** If any check fails (e.g., weld overstressed, length out of code bounds), the report highlights the cause with clear “Fail” status.
- **Summary Table Output:** The report summarizes all key checks (weld, base metal, utilization ratio) in a structured table for audit and review.
- **Deterministic and Reproducible:** The approach ensures consistency of results and easy traceability, fulfilling code and project doc-

umentation requirements.

5.3 Python Code

The entire logic for the report generation of Welded Lap Joint module is within the `save_design()` function. And it's being connected to the main GUI through `ui.template.py` and `ui_popup_summary.py` files. Below are key snippets from the module with explanations of their functionality.

Description of the Script

The script defines the `save_design()` function, which handles everything from user input to final design report generation. It uses `reportGenerator_latex.py` to manage properties and perform calculations.

Python Code

The following snippets showcase the core logic implemented in the report generation task.

Listing 5.1: Welded Lap Joint `save_design()` function

```
1 %-----begin code-----
2 def save_design(self, popup_summary):
3     """
4     Generate the LaTeX design report for Lap Joint
5     Welded Connection (Tension/Compression)
6     per IS 800:2007.
7     """
8     try:
9         #=====
10        #===== HELPER FUNCTIONS =====
11        #=====
12        def g(attr, default=None):
13            """Get attribute value with default"""
14            v = getattr(self, attr, default)
15            return default if v is None else v
16
17        def f2(x, default=0.0):
```

```

17         """Format to 2 decimal places"""
18         try:
19             return round(float(x), 2)
20         except (TypeError, ValueError):
21             return default
22
23     #
24     #===== EXTRACT ALL DESIGN VALUES
25     #
26     module = g('module', 'Lap Joint Welded')
27     mainmodule = 'Plate(d) Connection'
28     design_for = g('design_for', 'Tension').strip()
29     is_comp = design_for.lower().startswith('c')
30
31     edge_type = g('edgetype', 'Sheared or hand
32                 flame cut')
33
34     # Plate properties
35     plate1_thk = f2(self.plate1.thickness[0] if
36                    isinstance(self.plate1.thickness, list) else
37                    self.plate1.thickness, 0.0)
38     plate2_thk = f2(self.plate2.thickness[0] if
39                    isinstance(self.plate2.thickness, list) else
40                    self.plate2.thickness, 0.0)
41     plate_thk_min = min(plate1_thk, plate2_thk)
42     width = f2(g('width', 0.0), 0.0)
43     fy = f2(self.plate1.fy if hasattr(self, 'plate1
44         ') else 250, 250)
45     fu = f2(self.plate1.fu if hasattr(self, 'plate1
46         ') else 410, 410)
47
48     # Use stored values for strength calculation
49     variables to match Dock exactly
50     fu_weld = g('fu_weld', float(g('weld.fu', 410)))

```

```

    )
43     fu_parent = g('fu_parent', min(self.plate1.fu,
        self.plate2.fu) if hasattr(self, 'plate1')
        else 410)
44
45     # Load
46     axial_force_N = f2(g('axial_force', g('
        axialforce', g('tensileforce', 0.0))), 0.0)
47     axial_kN = f2(axial_force_N / 1000, 0.0)
48
49     # Weld properties
50     weld_size = f2(g('weld_size', g('weldsize',
        0.0)), 0.0)
51     weld_type = g('weld.type', 'Shop weld')
52     weld_fabrication = g('weld.fabrication', 'Shop
        Weld')
53     gamma_mw = 1.25 if 'shop' in weld_type.lower()
        else 1.50
54
55     # Effective throat thickness
56     effective_throat = f2(g('
        effective_throat_thickness', 0.7 * weld_size
        ), 0.0)
57
58     # Weld lengths
59     l_eff = f2(g('l_eff', g('weld_length_effective',
        g('weldlengtheffective', 0.0))), 0.0)
60     l_eff_min = f2(max(4 * weld_size, 40), 0.0)
61     l_eff_max = f2(70 * weld_size, 0.0)
62
63     # Long joint reduction factor
64     beta_lw = f2(g('beta_lw', g('betalw', 1.0)),
        1.0)
65
66     # End return and connection length
67     end_return = f2(g('end_return_length', max(2 *
        weld_size, 12)), 0.0)
68
69     # Overlap: Use calculated value if available to

```

```

    capture clearance logic
70     min_overlap_req = max(4 * weld_size, 40)
71     overlap_length = f2(g('overlap_length',
    min_overlap_req), 0.0)
72
73     conn_length = f2(g('connection_length', l_eff +
    2 * end_return), 0.0)
74
75     # Base metal capacity
76     Ag = plate_thk_min * width
77     gamma_m0 = 1.10
78     gamma_m1 = 1.25
79
80     if is_comp:
81         base_metal_capacity_kN = f2((Ag * fy /
    gamma_m0) / 1000, 0.0)
82     else:
83         Tdg = (Ag * fy / gamma_m0) / 1000
84         Tdn = (0.9 * Ag * fu * 0.7 / gamma_m1) /
    1000
85         base_metal_capacity_kN = f2(min(Tdg, Tdn),
    0.0)
86
87     # Retrieve calculated unit design strengths to
    match Dock
88     P_wd_val = g('weld_design_strength', (fu_weld *
    effective_throat) / (math.sqrt(3) *
    gamma_mw))
89     P_md_val = g('parent_design_strength', 0.6 *
    fu_parent * effective_throat / gamma_mw)
90     P_d_val = g('fillet_weld_design_strength', min(
    P_wd_val, P_md_val))
91
92     #
    =====
93
    #===== BUILD REPORT INPUT DICTIONARY
    =====
94
    #

```

```

=====

95     self.report_input = {
96         KEY_MODULE: module,
97         KEY_MAIN_MODULE: mainmodule,
98         KEY_DISP_DESIGN_FOR: design_for,
99         f"Thickness of Plate-1 (mm) *": plate1_thk,
100        f"Thickness of Plate-2 (mm) *": plate2_thk,
101        KEY_DISP_PLATE_WIDTH: width,
102        KEY_DISP_MATERIAL: g('main_material', g('
103            mainmaterial', 'N/A')),
104        KEY_DISP_WELD_SIZE: weld_size,
105        f"{'Tensile' if not is_comp else 'Axial'}
106            Force (kN) *": axial_kN,
107
108        "Additional inputs": "TITLE",
109        "Edge Preparation Method": edge_type,
110        KEY_DISP_DP_WELD_TYPE: weld_fabrication,
111        KEY_DISP_DP_WELD_MATERIAL_G_O_REPORT: f2(
112            fu_weld, 410),
113    }
114
115    # ===== BUILD REPORT CHECK =====
116    self.report_check = []
117
118    #
119
120    # SECTION 3.1: CALCULATING WELD STRENGTH
121    #
122
123    # 3.2.1 Weld Size Requirements
124    self.report_check.append([
125        "SubSection", "Weld Size Check", "|p{4cm}|p
126            {6cm}|p{4.5cm}|p{1.5cm}|"
127    ])
128
129    s_min = IS800_2007.cl_10_5_2_3_min_weld_size(

```

```

        plate1_thk, plate2_thk)
124     if plate_thk_min >= 10:
125         s_max = plate_thk_min - 1.5
126     else:
127         s_max = plate_thk_min
128     s_max = f2(s_max, 0.0)
129
130     size_check_req = Math(inline=True)
131     size_check_req.append(NoEscape(r'\begin{aligned}
132         &= ' + str(s_min) + r' \text{ mm}\\')
133     size_check_req.append(NoEscape(r'&[\text{As per
134         Table 21, IS 800:2007}]\\')
135     size_check_req.append(NoEscape(r's_{\text{max}}
136         &= ' + str(s_max) + r' \text{ mm}\\')
137     size_check_req.append(NoEscape(r'&[\text{Ref.
138         Cl. 10.5.2.3, 10.5.2.4}]'))
139     size_check_req.append(NoEscape(r'\end{aligned}'
140         ))
141
142     size_check_prov = Math(inline=True)
143     size_check_prov.append(NoEscape(r's = ' + str(
144         weld_size) + r' \text{ mm}'))
145
146     size_status = "PASS" if (s_min <= weld_size <=
147         s_max) else "FAIL"
148     self.report_check.append(["Weld Size",
149         size_check_req, size_check_prov, size_status
150     ])
151
152     # 3.1.1 Fillet Weld (Strength Calculation +
153         Throat Thickness)
154     self.report_check.append([
155         "SubSection", "Weld Strength Calculation",
156         "|p{4cm}|p{6cm}|p{4.5cm}|p{1.5cm}|"
157     ])
158
159     # Effective Throat Thickness (Eq 3.2/3.3)

```

```

150     throat_req = Math(inline=True)
151     throat_req.append(NoEscape(r'\begin{aligned}'))
152     throat_req.append(NoEscape(r't_t &= K \times s
153         \\'))
154     throat_req.append(NoEscape(r'&= 0.7 \times ' +
155         str(weld_size) + r'\\'))
156     throat_req.append(NoEscape(r'&= ' + str(
157         effective_throat) + r' \text{ mm}\\'))
158     throat_req.append(NoEscape(r'&[\text{Ref. Cl.
159         10.5.3.2}]'))
160     throat_req.append(NoEscape(r'\end{aligned}'))
161     self.report_check.append(["Throat Thickness", "
162         ", throat_req, ""])
163
164     # Weld Metall Strength (Pwd) (Eq 3.1)
165     weld_metal_req = Math(inline=True)
166     weld_metal_req.append(NoEscape(r'\begin{aligned}
167         \\'))
168     weld_metal_req.append(NoEscape(r'P_{wd} &= \
169         \frac{f_u}{\sqrt{3}} \cdot \frac{t_t}{\gamma_{mw}}\\'))
170     weld_metal_req.append(NoEscape(r'&= \frac{
171         ' + str(f2(fu_weld)) + r'}{\sqrt{3}} \times \
172         \frac{
173         ' + str(effective_throat) + r'}{' + str(
174         gamma_mw) + r'}\\'))
175     weld_metal_req.append(NoEscape(r'&= ' + f'{
176         P_wd_val:.2f}' + r' \text{ N/mm}\\'))
177     weld_metal_req.append(NoEscape(r'&[\text{Ref.
178         Cl. 10.5.7.1.1}]'))
179     weld_metal_req.append(NoEscape(r'\end{aligned}'
180         ))
181     self.report_check.append(["Weld Metal Strength"
182         , "", weld_metal_req, ""])
183
184     # Parent Metal Strength (Pmd) (Eq 3.4)
185     parent_metal_req = Math(inline=True)
186     parent_metal_req.append(NoEscape(r'\begin{
187         aligned}\\'))
188     parent_metal_req.append(NoEscape(r'P_{md} &=

```

```

0.6 \cdot f_u \cdot \frac{t_t}{\gamma_{mw}}
}}\\\\'))
173 parent_metal_req.append(NoEscape(r'&= 0.6 \
times ' + str(f2(fu_parent)) + r' \times \
frac{' + str(effective_throat) + r'}{' + str
(gamma_mw) + r'}\\\\'))
174 parent_metal_req.append(NoEscape(r'&= ' + f'{
P_md_val:.2f}' + r' \text{ N/mm}\\\\'))
175 parent_metal_req.append(NoEscape(r'&[\text{Ref.
Cl. 10.5.7.1.2}]'))
176 parent_metal_req.append(NoEscape(r'\end{aligned
}'))
177 self.report_check.append(["Parent Metal
Strength", "", parent_metal_req, ""])
178
179 # Governing Design Strength (Pd) (Eq 3.5)
180 design_strength_eq = Math(inline=True)
181 design_strength_eq.append(NoEscape(r'\begin{
aligned}'))
182 design_strength_eq.append(NoEscape(r'P_d &= \
min(P_{wd}, P_{md})\\\\'))
183 design_strength_eq.append(NoEscape(r'&= \min('
+ f'{P_wd_val:.2f}' + r', ' + f'{P_md_val:.2
f}' + r')\\\\'))
184 design_strength_eq.append(NoEscape(r'&= ' + f'{
P_d_val:.2f}' + r' \text{ N/mm}\\\\'))
185 design_strength_eq.append(NoEscape(r'&[\text{
Ref. Cl. 10.5.7.1}]'))
186 design_strength_eq.append(NoEscape(r'\end{
aligned}'))
187 self.report_check.append(["Design Strength", "",
, design_strength_eq, ""])
188
189 # 3.1.2 Reduction Factors (Long Weld)
190 self.report_check.append([
191 "SubSection", "Long Joint Reduction Factor"
, "|p{4cm}|p{6cm}|p{4.5cm}|p{1.5cm}|"
192 ])
193

```

```

194         if l_eff > 150 * effective_throat:
195             beta_req = Math(inline=True)
196             beta_req.append(NoEscape(r'\begin{aligned}'
197                                 ))
197             beta_req.append(NoEscape(r'\text{Since }
198                                     l_w > 150 \times t_t\\'
199                                     ))
200             beta_req.append(NoEscape(r'\beta_{lw} &=
201                                     1.2 - 0.2 \times \frac{l_w}{150 \times
202                                     t_t}\\'
203                                     ))
204             beta_req.append(NoEscape(r'&= 1.2 - 0.2 \
205                                     times \frac{' + str(l_eff) + r'}{150 \
206                                     times ' + str(effective_throat) + r'}\\'
207                                     ))
208             beta_calc = 1.2 - 0.2 * (l_eff / (150 *
209                                     effective_throat))
210             beta_req.append(NoEscape(r'&= ' + f'{
211                                     beta_calc:.3f}' + r'\\'
212                                     ))
213             beta_req.append(NoEscape(r'&\text{(but }
214                                     0.6 \leq \beta_{lw} \leq 1.0\text{)}\\'
215                                     ))
216             # Use stored beta_lw which should match
217             beta_req.append(NoEscape(r'\beta_{lw} &= '
218                                     + f'{beta_lw:.2f}' + r'\\'
219                                     ))
220             beta_req.append(NoEscape(r'&[\text{Ref. C1.
221                                     10.5.7.2}] '))
222             beta_req.append(NoEscape(r'\end{aligned}'))
223             beta_status = ""
224         else:
225             beta_req = Math(inline=True)
226             beta_req.append(NoEscape(r'\begin{aligned}'
227                                 ))
228             beta_req.append(NoEscape(r'\text{Since }
229                                     l_w \leq 150 \times t_t\\'
230                                     ))
231             beta_req.append(NoEscape(r'\beta_{lw} &=
232                                     1.0\\'
233                                     ))
234             beta_req.append(NoEscape(r'&[\text{Ref. C1.
235                                     10.5.7.2}] '))
236             beta_req.append(NoEscape(r'\end{aligned}'))
237             beta_status = "PASS"

```

```

216
217         beta_prov = Math(inline=True)
218         beta_prov.append(NoEscape(r'\beta_{lw} = ' + f'
219                                {beta_lw:.1f}'))
220
221         self.report_check.append(["Long Joint Factor",
222                                   beta_req, beta_prov, beta_status])
223
224         #
225         =====
226
227         # SECTION 3.2: DETAILING CHECKLIST
228         #
229         =====
230
231         # 3.2.2 Effective Length of Weld (Limits)
232         self.report_check.append([
233             "SubSection", "Effective Length Limits", "|
234             p{4cm}|p{6cm}|p{4.5cm}|p{1.5cm}|"
235         ])
236
237         eff_len_req = Math(inline=True)
238         eff_len_req.append(NoEscape(r'\begin{aligned}'
239                                     )
240
241         eff_len_req.append(NoEscape(r'l_{\text{eff,min}}
242                                     }} \max(4s, 40)\')) # Step 1: Formula
243         eff_len_req.append(NoEscape(r'&= \max(4 \times
244                                     ' + str(weld_size) + r', 40)\')) # Step 2:
245                                     Substitution
246         eff_len_req.append(NoEscape(r'&= ' + str(
247                                     l_eff_min) + r' \text{ mm}\')) # Step 3:
248                                     Result
249         eff_len_req.append(NoEscape(r'l_{\text{eff,max}}
250                                     }} \&= 70s\'))
251         eff_len_req.append(NoEscape(r'&= 70 \times ' +
252                                     str(weld_size) + r'\'))
253         eff_len_req.append(NoEscape(r'&= ' + str(
254                                     l_eff_max) + r' \text{ mm}\'))
255         eff_len_req.append(NoEscape(r'&[\text{Ref. C1.

```

```

10.5.3}}]'))
239     eff_len_req.append(NoEscape(r'\end{aligned}'))
240
241     eff_len_prov = Math(inline=True)
242     eff_len_prov.append(NoEscape(r'l_{\text{eff}} =
        ' + str(l_eff) + r' \text{ mm}'))
243
244     eff_status = "PASS" if (l_eff_min <= l_eff <=
        l_eff_max) else "FAIL"
245     self.report_check.append(["Length Limits",
        eff_len_req, eff_len_prov, eff_status])
246
247     # 3.2.3 End Returns
248     self.report_check.append([
249         "SubSection", "End Returns", "|p{4cm}|p{6cm}
        |p{4.5cm}|p{1.5cm}|"
250     ])
251
252     return_req = Math(inline=True)
253     return_req.append(NoEscape(r'\begin{aligned}'))
254     return_req.append(NoEscape(r'\text{Min. Length}
        &= \max(2s, 12)\'))
255     return_req.append(NoEscape(r'&= \max(2 \times '
        + str(weld_size) + r', 12)\'))
256     return_req.append(NoEscape(r'&= ' + str(
        end_return) + r' \text{ mm}\'))
257     return_req.append(NoEscape(r'&[\text{Ref. Cl.
        10.5.4.5}}]'))
258     return_req.append(NoEscape(r'\end{aligned}'))
259
260     return_prov = Math(inline=True)
261     return_prov.append(NoEscape(str(end_return) + r
        ' \text{ mm}'))
262
263     self.report_check.append(["End Returns",
        return_req, return_prov, "PASS"])
264
265     #
=====

```

```

266 # SECTION 3.3: DETAILING
267 #
=====
268
269 # 3.3.1 Calculating Required Weld Length
270 self.report_check.append([
271     "SubSection", "Required Weld Length", "|p{4
        cm}|p{6cm}|p{4.5cm}|p{1.5cm}|"
272 ])
273
274 # Required Length Calculation (Eq 3.15)
275 # Use P_d_val from object to be consistent
276 l_req_base = axial_force_N / (2 * P_d_val) if
        P_d_val > 0 else 9999
277 l_req_disp = f2(l_req_base, 0.0)
278
279 length_req_calc = Math(inline=True)
280 length_req_calc.append(NoEscape(r'\begin{
        aligned}\\'))
281 length_req_calc.append(NoEscape(r'l_{\text{req
        }} &= \frac{P}{2 \cdot P_d}\\\\'))
282 length_req_calc.append(NoEscape(r'&= \frac{' +
        str(int(axial_force_N)) + r'}{2 \times ' + f
        '{P_d_val:.2f}' + r'}\\\\'))
283 length_req_calc.append(NoEscape(r'&= ' + str(
        l_req_disp) + r' \text{ mm}\\\\'))
284 if beta_lw < 1.0:
285     l_req_final = l_req_base / beta_lw
286     length_req_calc.append(NoEscape(r'l_{\text{
        req,mod}} &= \frac{l_{\text{req}}}{\beta_{lw}} = \frac{' + str(l_req_disp) +
        r'}{' + str(beta_lw) + r'} = ' + f'{
        l_req_final:.1f}' + r' \text{ mm}\\\\'))
287 else:
288     length_req_calc.append(NoEscape(r'&\text{No
        long joint reduction.}\\'))
289 length_req_calc.append(NoEscape(r'\end{aligned}

```

```

    '))
290
291     self.report_check.append(["Required Length", ""
    , length_req_calc, ""])
292
293     # 3.3.2 Determining Connection Configuration
294     self.report_check.append([
295         "SubSection", "Connection Configuration", "
    |p{4cm}|p{6cm}|p{4.5cm}|p{1.5cm}|"
296     ])
297
298     config_calc = Math(inline=True)
299     config_calc.append(NoEscape(r'\begin{aligned}'
    )
300     config_calc.append(NoEscape(r'L_{\text{conn}}
    &= l_{\text{eff}} + 2 \times l_{\text{return}}
    }\!\!' ))
301     config_calc.append(NoEscape(r'&= ' + str(l_eff)
    + r' + 2 \times ' + str(end_return) + r'\!'
    ))
302     config_calc.append(NoEscape(r'&= ' + str(
    conn_length) + r' \text{ mm}\!\!'))
303     config_calc.append(NoEscape(r'\end{aligned}'))
304
305     self.report_check.append(["Configuration", "",
    config_calc, ""])
306
307     #
    =====
308
309     # ADDITIONAL CHECKS
    #
    =====
310
311     # Base Metal Strength
312     self.report_check.append([
313         "SubSection", "Base Metal Strength", "|p{4
    cm}|p{6cm}|p{4.5cm}|p{1.5cm}|"

```

```

314     ])
315
316     if is_comp:
317         comp_req = Math(inline=True)
318         comp_req.append(NoEscape(r'\begin{aligned}'))
319         comp_req.append(NoEscape(r'P_d &= \frac{A_g}{\gamma_m}'))
320         comp_req.append(NoEscape(r'&= \frac{'}{'} + f'{'Ag:.1f}' + r' \times ' + str(fy) + r'{'}' + str(gamma_m0) + r'{'}\frac{'}{'}'))
321         comp_req.append(NoEscape(r'&= ' + str(base_metal_capacity_kN) + r' \text{ kN}'))
322         comp_req.append(NoEscape(r'&[\text{Ref. Cl. 7.1.2}]'))
323         comp_req.append(NoEscape(r'\end{aligned}'))
324         comp_status = "PASS" if base_metal_capacity_kN >= axial_kN else "FAIL"
325         self.report_check.append(["Plate Tension Capacity", f"{axial_kN:.2f} kN", comp_req, comp_status])
326     else:
327         ten_req = Math(inline=True)
328         ten_req.append(NoEscape(r'\begin{aligned}'))
329         ten_req.append(NoEscape(r'T_{dg} &= \frac{A_g f_y}{\gamma_m} = ' + f'{'Tdg:.2f}' + r' \text{ kN}'))
330         ten_req.append(NoEscape(r'T_{dn} &= \frac{0.9 A_g f_u \beta}{\gamma_m} = ' + f'{'Tdn:.2f}' + r' \text{ kN}'))
331         ten_req.append(NoEscape(r'T_d &= \min(T_{dg}, T_{dn}) = ' + str(base_metal_capacity_kN) + r' \text{ kN}'))
332         ten_req.append(NoEscape(r'&[\text{Ref. Cl. 6.2, 6.3}]'))

```

```

333         ten_req.append(NoEscape(r'\end{aligned}'))
334         ten_status = "PASS" if
            base_metal_capacity_kN >= axial_kN else
            "FAIL"
335         self.report_check.append(["Plate Tension
            Capacity", f"{axial_kN:.2f} kN", ten_req
            , ten_status])
336
337         #
            =====

338         # UTILIZATION RATIO
339         #
            =====

340         self.report_check.append([
341             "SubSection", "Utilization Ratio", "|p{4cm
            }|p{6cm}|p{4.5cm}|p{1.5cm}|"
342         ])
343
344         n = 2
345         # Use stored capacity from design capacity if
            available to be exact
346         weld_capacity_val = g('design_capacity', 2 *
            l_eff * P_d_val * beta_lw)
347         weld_capacity_kN = f2(weld_capacity_val / 1000,
            0.0)
348
349         # Use stored UR if available
350         utilization_ratio_val = g('utilization_ratio',
            axial_kN / weld_capacity_kN if
            weld_capacity_kN > 0 else 0.0)
351         utilization_ratio = f2(utilization_ratio_val,
            0.0)
352
353         util_req = Math(inline=True)
354         util_req.append(NoEscape(r'\begin{aligned}'))
355         util_req.append(NoEscape(r'P_{\text{capacity}}
            &= n \times l_{\text{eff}} \times P_d \times

```

```

        \beta_{lw}\\')
356     util_req.append(NoEscape(r'&= ' + str(n) + r' \
        times ' + str(l_eff) + r' \times ' + f'{
        P_d_val:.2f}') + r' \times ' + str(beta_lw) +
        r'\\'))
357     util_req.append(NoEscape(r'&= ' + str(
        weld_capacity_kN) + r' \text{ kN}\\\\'))
358     util_req.append(NoEscape(r'\text{UR} &= \frac{P
        }{P_{\text{capacity}}}\\\\\'))
359     util_req.append(NoEscape(r'&= \frac{' + str(
        axial_kN) + r'}{' + str(weld_capacity_kN) +
        r'}\\\\'))
360     util_req.append(NoEscape(r'&= ' + str(
        utilization_ratio) + r'\\'))
361     util_req.append(NoEscape(r'\end{aligned}'))
362
363     util_prov = Math(inline=True)
364     util_prov.append(NoEscape(str(utilization_ratio
        ) + r' \leq 1.0'))
365
366     util_status = "PASS" if utilization_ratio <=
        1.0 else "FAIL"
367     self.report_check.append(["Utilization", f"{
        axial_kN:.2f} kN", util_req, util_status])
368
369     #=====
370     #===== GENERATE PDF REPORT =====
371     #=====
372     Disp_2d_image = []
373     Disp_3D_image = "/ResourceFiles/images/3d.png"
374     rel_path = os.path.abspath(".").replace("\\", "
        /")
375     fname_no_ext = popup_summary.get("filename", "
        LapJointWeldedReport")
376     folder = popup_summary.get('folder', './reports
        ')
377     os.makedirs(folder, exist_ok=True)
378
379     CreateLatex.save_latex(

```

```

380         CreateLatex(), self.report_input, self.
381             report_check,
382             popup_summary, fname_no_ext, rel_path,
383             Disp_2d_image, Disp_3D_image,
384             module=self.module
385     )
386     self.logger.info(f"Report generated
387                      successfully: {fname_no_ext}.pdf")
388     return True
389
390 except Exception as e:
391     print(f"WARNING in save_design(): {e}")
392     import traceback
393     traceback.print_exc()
394     return False
395 %----- end code -----

```

5.3.1 Explanation of the Code

The `save_design` function for the welded lap joint is the central routine that converts the completed design into a structured LaTeX report. Its workflow can be summarized as follows:

1. **Collect Design Data:** All relevant input and output values stored in the welded lap joint object are gathered. This includes: plate dimensions (thickness and width), weld size, weld length, material properties (f_y , f_u), applied load, and intermediate results such as weld capacity, base metal capacity, and utilization ratio.
2. **Check Design Status:** The function reads the internal `design_status` flag:
 - If the design has failed (for example, required weld length exceeds available overlap, or $UR > 1.0$), it prepares a brief failure report explaining the governing reason.
 - If the design is safe, it proceeds to create a full, detailed report.
3. **Prepare report_input and Check List:** A dictionary is assembled to pass all data to the LaTeX template. Typical items are:

- Connection description and input summary,
- Stepwise weld design: permissible weld size range, design weld strength f_{wd} , required and provided weld length, long-weld reduction (if any),
- Base metal strength checks (gross yielding, net rupture),
- Final utilization ratio and pass/fail remarks.

Along with this, a list of design checks (DDCL-style) is created so that each check can be printed with its status in the report.

4. **Generate LaTeX Equations:** Using LaTeX strings (often wrapped with `NoEscape`), the function formats the main formulas with substituted numerical values, such as:

$$f_{wd} = \frac{f_u \cdot a}{\sqrt{3} \gamma_{mw}}, \quad R_{weld} = 2 l_{eff} f_{wd},$$

and the comparison of applied load with weld and plate capacities. This makes the report transparent and easy to follow.

5. **File Handling and Report Creation:** Finally, the function sets up the output folder (creating it if needed) and calls the common `CreateLatex.save_latex` method. This compiles the LaTeX document into a professional PDF that contains: input summary, calculation steps, DDCL table, and conclusion for the welded lap joint.

5.4 Documentation

The directory structure used for the Report Generation is organized as follows:

```
src/osdag_core
```

```
design_report/
    reportGenerator_latex.py
```

```
design_type/
```

```
connection/  
lap_joint_welded.py
```

```
Report_functions.py
```

Program Start Calls The main entry point for the program is [osdagMainPage.py](#). To start the program, open the Osdag folder, go to src and start the terminal with that path, execute the following command from the project root:

```
$ python -m osdag_gui
```

5.5 References

- Osdag Github repository: <https://osdag.github.io/>
- IS 800:2007, "General Construction in Steel Code of Practice of Practice"

Chapter 6

Report Generation of Welded Butt Joint

6.1 Problem Statement

The objective of this task was to develop an automated design and reporting workflow for a **Welded Butt Joint** connection in Osdag. The module must design the weld and base metal in accordance with IS 800:2007, verify all limit states (weld strength, long joint reduction, base metal yielding and rupture) and generate a clear, stepwise LaTeX report for documentation and checking purposes.

6.2 Tasks Done

6.2.1 Design Automation Workflow

- Implemented the `ButtJointWelded` class as a moment connection module, handling all required inputs: plate thicknesses, plate width, material grade, weld size, cover plate option, and axial force.
- Added UI input, detailing and weld preference functions (e.g. `input_values`, `weld_values`, `detailing_values`) to collect user choices such as shop/-field weld and weld material strength.
- Implemented validation in `func_for_validation` to ensure non-empty

and positive values for key fields (plate width, axial force) before starting the design.

6.2.2 Core Design Functions

- **Initialisation (set_input_values):** Sets up plates, weld object, design force (tension or compression), cover plate type (single/double) and calculates required cover plate thickness and packing plate thickness as per IS 800:2007 recommendations.
- **Design of Weld (design_of_weld):**
 - Selects a valid weld size within IS 800 limits using the minimum and maximum weld size rules.
 - Computes effective throat thickness and design weld strength

$$f_w = \frac{f_u}{\sqrt{3} \gamma_{mw}}.$$

- Calls subsequent functions for weld length, strength verification, long joint reduction and base metal checks.
- **Weld Length (weld_length):**
 - Checks that the chosen weld size is between the computed $s_{\min}$ and $s_{\max}$.
 - Determines required weld length from the design axial force; if possible a straight weld equal to plate width is used, otherwise skewed welds and possible side welds are calculated.
 - Stores the provided and effective weld length and weld angle for later reporting.
- **Weld Strength Verification (weld_strength_verification):**
 - Ensures effective weld length satisfies the minimum requirement $L_{\text{eff}} \geq 4s$.
 - Computes weld strength

$$P_w = N_f \cdot 0.707 s \cdot L_{\text{eff}} \cdot f_w$$

and the weld utilization ratio $UR_{\text{weld}} = P_{\text{req}}/P_w$.

- **Long Joint Reduction** (`long_joint_reduction_factor`):
- For long welds, calculates reduction factor β_L based on L_{eff} and effective throat thickness, and updates the reduced weld strength and utilization.
- **Base Metal Strength** (`check_base_metal_strength`):
- Computes gross area and net area (equal for welded joints) and evaluates:

$$T_{dy} = \frac{A_g f_y}{\gamma_{m0}}, \quad T_{du} = \frac{0.9 A_n f_u}{\gamma_{m1}}$$

for tension, or compression capacity for compression design.

- Stores base metal utilization ratio.
- **Final Check** (`calculate_final_utilization_ratio`):
- Takes the maximum of weld and base metal utilization ratios as the overall utilization.
- Sets `design_status` to SAFE if all utilization ratios are ≤ 1.0 , otherwise UNSAFE with guidance on which component governs.

6.2.3 Report Generation with `save_design`

- The `save_design` function is called only when `design_status` is SAFE. It gathers all important data (forces, material strengths, plate dimensions, weld size, cover plate type) into a `report_input` dictionary.
- It then constructs a detailed `report_check` list containing:
 - Weld size limits (s_{min} , s_{max}) and pass/fail status,
 - Weld strength calculation with substituted values,
 - Base metal capacity in tension or compression,
 - Overall capacity, utilization ratio and final design status.
- Mathematical expressions are wrapped using `NoEscape` so that LaTeX formulas (for example the expression of f_w or P_w) appear correctly in the final PDF.

Finally, `CreateLatex.save_latex` is invoked to generate the formatted PDF report, including 2D/3D images and a summary table of all checks.

6.3 Python Code

The entire logic for the report generation of Welded Butt Joint module is within the `save_design()` function. And it's being connected to the main GUI through `ui_template.py` and `ui_popup_summary.py` files. Below are key snippets from the module with explanations of their functionality.

Description of the Script

The script defines the `save_design()` function, which handles everything from user input to final design report generation. It uses `report-Generator_latex.py` to manage properties and perform calculations.

Python Code

The following snippets showcase the core logic implemented in the report generation task.

Listing 6.1: Welded Butt Joint `save_design()` function

```

1 %-----begin code-----
2 def save_design(self, popup_summary):
3     """
4     Generate the LaTeX design report for Welded Butt
5     Joint Connection
6     per IS 800:2007 following DDCL structure.
7     """
8     try:
9         # =====
10        # ===== HELPER FUNCTIONS =====
11        # =====
12        def g(attr, default=None):
13            """Get attribute value with default"""

```

```

13         v = getattr(self, attr, default)
14         return default if v is None else v
15
16     def f2(x, default=0.0):
17         """Format to 2 decimal places"""
18         try:
19             return round(float(x), 2)
20         except (TypeError, ValueError):
21             return default
22
23     #
24     # ===== EXTRACT ALL DESIGN VALUES
25     #
26     module = g('module', 'Butt Joint Welded
27               Connection')
28     mainmodule = 'Plate(d) Connection'
29     design_for = g('design_for', 'Tension').
30                 strip()
31     is_comp = design_for.lower().startswith('c')
32     edge_type = g('edgetype', 'Sheared or hand
33                 flame cut')
34
35     # Plate properties
36     plate1_thk = f2(self.plate1.thickness[0] if
37                     isinstance(
38                         self.plate1.thickness, list) else self.
39                         plate1.thickness, 0.0)
40     plate2_thk = f2(self.plate2.thickness[0] if
41                     isinstance(
42                         self.plate2.thickness, list) else self.
43                         plate2.thickness, 0.0)
44     plate_thk_min = min(plate1_thk, plate2_thk)
45     width = f2(g('width', g('plates_width', 0.0)
46                     ), 0.0)

```

```

39         fy = f2(self.plate1.fy if hasattr(self, '
        plate1') else 250, 250)
40         fu = f2(self.plate1.fu if hasattr(self, '
        plate1') else 410, 410)
41
42         # Use stored values for strength calculation
        variables
43         fu_weld = g('fu', float(g('weld.fu', 410)))
44
45         # Load
46         axial_force_N = f2(
47             g('axial_force', g('axialforce', g('
            tensileforce', 0.0))), 0.0)
48         axial_kN = f2(axial_force_N / 1000, 0.0)
49
50         # Cover plate
51         cover_plate_str = g('cover_plate', g(
52             'cover_plate_type', 'Single-Cover'))
53         N_f = 2 if "double" in cover_plate_str.lower
            () else 1
54         cover_thk = f2(g('
            calculated_cover_plate_thickness', 0.0),
            0.0)
55         packing_thk = f2(g('packing_plate_thickness'
            ,
56                             g('packing_thickness', 0.0)
                                ), 0.0)
57
58         # Weld properties
59         weld_size = f2(g('weld_size', g('weldsize',
            0.0)), 0.0)
60         weld_type = g('weld.type', 'Shop weld')
61         weld_fabrication = g('weld.fabrication', '
            Shop Weld')
62         gamma_mw = 1.25 if 'shop' in weld_type.lower
            () else 1.50
63
64         # Effective throat thickness
65         effective_throat = f2(

```

```

66         g('effective_throat_thickness', 0.707 *
67           weld_size), 0.0)
68
69     # Weld lengths - get from object attributes
70     L_req = f2(g('L_req', 0.0), 0.0)
71     L_eff_provided = f2(g('weld_length_effective
72       ', 0.0), 0.0)
73     L_provided_line = f2(
74       g('weld_length_provided', 0.0), 0.0) #
75       Per weld line
76     L_eff_min = f2(max(4 * weld_size, 40), 0.0)
77
78     # Skew angle and side welds
79     skew_angle = f2(g('weld_angle', 0.0), 0.0)
80     side_weld_len = f2(g('side_weld_length',
81       0.0), 0.0)
82
83     # Calculate L_target per weld line
84     L_target = f2(L_req / N_f if N_f > 0 else
85       L_req, 0.0)
86
87     # Long joint reduction factor
88     beta_L = f2(g('beta_L', g('betalw', 1.0)),
89       1.0)
90
91     # Base metal capacity - FIXED: Now
92     calculates both Tdg and Tdn
93     Ag = plate_thk_min * width
94     gamma_m0 = 1.10
95     gamma_m1 = 1.25
96
97     # Always calculate both for tension case
98     Tdg = f2((Ag * fy / gamma_m0) / 1000, 0.0)
99     Tdn = f2((0.9 * Ag * fu / gamma_m1) / 1000,
100       0.0)
101
102     if is_comp:
103         base_metal_capacity_kN = Tdg # Only
104         yielding for compression

```

```

96         else:
97             base_metal_capacity_kN = f2(min(Tdg, Tdn
98                 ), 0.0)
99
100             # Weld strength - should use f_w_adjusted if
101             # beta_L applied
102             f_w = fu_weld / (math.sqrt(3) * gamma_mw)
103             f_w_adjusted = f2(f_w * beta_L, 0.0)
104
105             # Weld capacity using adjusted strength
106             weld_strength_N = f2(
107                 f_w_adjusted * effective_throat *
108                 L_eff_provided * N_f, 0.0)
109             weld_strength_kN = f2(weld_strength_N /
110                 1000, 0.0)
111
112             #
113             =====
114
115             # ===== BUILD REPORT INPUT DICTIONARY
116             =====
117
118             #
119             =====
120
121             self.report_input = {
122                 KEY_MODULE: module,
123                 KEY_MAIN_MODULE: mainmodule,
124                 KEY_DISP_DESIGN_FOR: design_for,
125                 f"Thickness of Plate-1 (mm) *":
126                     plate1_thk,
127                 f"Thickness of Plate-2 (mm) *":
128                     plate2_thk,
129                 KEY_DISP_PLATE_WIDTH: width,
130                 KEY_DISP_MATERIAL: g('main_material', g(
131                     'mainmaterial', 'N/A')),
132                 KEY_DISP_COVER_PLT: cover_plate_str,
133                 KEY_DISP_WELD_SIZE: weld_size,
134                 f"{'Tensile' if not is_comp else 'Axial
135                     '} Force (kN) *": axial_kN,

```

```

122         "Additional inputs": "TITLE",
123         "Edge Preparation Method": edge_type,
124         KEY_DISP_DP_WELD_TYPE: weld_fabrication,
125         KEY_DISP_DP_WELD_MATERIAL_G_O_REPORT: f2
            (fu_weld, 410),
126     }
127
128     # ===== BUILD REPORT CHECK =====
129     self.report_check = []
130
131     #
132     # =====
133     # SECTION 3.1: COVER PLATE DESIGN
134     # =====
135
136     self.report_check.append([
137         "SubSection", "Cover Plate Design", "|p
            {4cm}|p{4cm}|p{6.5cm}|p{1.5cm}|"
138     ])
139
140     # FIXED ISSUE 1: Correct fraction display
141     if N_f == 2: # Double cover
142         tcp_numerator = 9
143         tcp_denominator = 16
144         tcp_req = f2((9.0 / 16.0) *
            plate_thk_min, 0.0)
145     else: # Single cover
146         tcp_numerator = 5
147         tcp_denominator = 8
148         tcp_req = f2((5.0 / 8.0) * plate_thk_min
            , 0.0)
149
150     tcp_calc = Math(inline=True)
151     tcp_calc.append(NoEscape(r'\begin{aligned}'))
152     tcp_calc.append(NoEscape(r'T_{cp} &\geq \frac{' + str(

```

```

151         tcp_numerator) + r'}{' + str(
            tcp_denominator) + r'} \times T_{min}
            )\\')
152 tcp_calc.append(NoEscape(r'&\geq \frac{' +
            str(tcp_numerator) + r'}{' + str(
153         tcp_denominator) + r'} \times ' + str(
            plate_thk_min) + r'\\'))
154 tcp_calc.append(
155     NoEscape(r'&\geq ' + str(tcp_req) + r' \
            text{ mm}\\'))
156 tcp_calc.append(NoEscape(r'\end{aligned}'))
157
158 tcp_prov = Math(inline=True)
159 tcp_prov.append(
160     NoEscape(r'T_{cp} = ' + str(cover_thk) +
            r' \text{ mm}'))
161
162 tcp_status = "PASS" if cover_thk >= tcp_req
            else "FAIL"
163 self.report_check.append(
164     ["Cover Plate Thickness", tcp_calc,
            tcp_prov, tcp_status])
165
166 # Packing plate requirement (if applicable)
167 if abs(plate1_thk - plate2_thk) > 0.001 and
            N_f == 2:
168     packing_calc = Math(inline=True)
169     packing_calc.append(NoEscape(r'\begin{
            aligned}'))
170     packing_calc.append(NoEscape(r'T_{pack}
            &= |t_1 - t_2|\\'))
171     packing_calc.append(
172         NoEscape(r'&= |' + str(plate1_thk) +
            r' - ' + str(plate2_thk) + r'
            |\\'))
173     packing_calc.append(
174         NoEscape(r'&= ' + str(packing_thk) +
            r' \text{ mm}\\'))
175     packing_calc.append(NoEscape(r'\end{

```

```

176         aligned}'))
177
178         packing_prov = Math(inline=True)
179         packing_prov.append(
180             NoEscape(str(packing_thk) + r' \text
181                 { mm}'))
182
183         self.report_check.append(
184             ["Packing Plate", packing_calc,
185              packing_prov, "PASS"])
186
187         #
188         =====
189
190         # SECTION 3.2: WELD DESIGN
191         #
192         =====
193
194         self.report_check.append([
195             "SubSection", "Weld Design", "|p{4cm}|p
196                 {4cm}|p{6.5cm}|p{1.5cm}|"
197         ])
198
199         # Minimum and maximum weld size
200         s_min = IS800_2007.cl_10_5_2_3_min_weld_size
201             (
202                 plate1_thk, plate2_thk)
203         s_max = f2(plate_thk_min - 1.5, 0.0)
204
205         size_check_req = Math(inline=True)
206         size_check_req.append(NoEscape(r'\begin{
207             aligned}'))
208         size_check_req.append(
209             NoEscape(r's_{min} &= ' + str(s_min) + r
210                 ' \text{ mm}'))
211         size_check_req.append(
212             NoEscape(r'&[\text{Table 21, IS
213                 800:2007}]))
214         size_check_req.append(NoEscape(r's_{max} &=

```

```

203         T_{min} - 1.5\\')
204     size_check_req.append(
205         NoEscape(r'&= ' + str(plate_thk_min) + r'
206             ' - 1.5\\'))
207     size_check_req.append(
208         NoEscape(r'&= ' + str(s_max) + r' \text{
209             mm}\\'))
210     size_check_req.append(
211         NoEscape(r'&[\text{Ref. Cl. 10.5.2.3,
212             10.5.2.4}]'))
213     size_check_req.append(NoEscape(r'\end{
214         aligned}'))
215
216     size_check_prov = Math(inline=True)
217     size_check_prov.append(
218         NoEscape(r's = ' + str(weld_size) + r' \
219             text{ mm}'))
220
221     size_status = "PASS" if (s_min <= weld_size
222         <= s_max) else "FAIL"
223     self.report_check.append(
224         ["Weld Size Check", size_check_req,
225             size_check_prov, size_status])
226
227     # Effective throat thickness
228     throat_calc = Math(inline=True)
229     throat_calc.append(NoEscape(r'\begin{aligned
230         }'))
231     throat_calc.append(NoEscape(r'a &= 0.707 \
232         times s\\'))
233     throat_calc.append(
234         NoEscape(r'&= 0.707 \times ' + str(
235             weld_size) + r'\\'))
236     throat_calc.append(
237         NoEscape(r'&= ' + str(effective_throat)
238             + r' \text{ mm}\\'))
239     throat_calc.append(NoEscape(r'\end{aligned}'
240         ))
241

```

```

229         self.report_check.append(["Effective Throat"
230                                   , "", throat_calc, ""])
231
232         # Design strength of weld
233         weld_strength_calc = Math(inline=True)
234         weld_strength_calc.append(NoEscape(r'\begin{
235             aligned}\\'))
236         weld_strength_calc.append(
237             NoEscape(r'f_{wd} \&= \frac{f_u}{\sqrt{3}
238                 \times \gamma_{mw}}\\\\'))
239         weld_strength_calc.append(NoEscape(
240             r'\&= \frac{' + str(f2(fu_weld)) + r'}{\sqrt{3} \times ' + str(gamma_mw) + r'
241                 '}}\\\\'))
242         weld_strength_calc.append(
243             NoEscape(r'\&= ' + f'{f_w:.2f}' + r' \
244                 text{ N/mm}^2\\\\'))
245         weld_strength_calc.append(NoEscape(r'\end{
246             aligned}'))
247
248         self.report_check.append(
249             ["Design Strength", "",
250              weld_strength_calc, ""])
251
252         #
253         =====
254
255         # SECTION 3.3: REQUIRED WELD LENGTH
256         #
257         =====
258
259         self.report_check.append([
260             "SubSection", "Required Weld Length", "|
261                 p{4cm}|p{4cm}|p{6.5cm}|p{1.5cm}|"
262             ])
263
264         # Calculate Lreq in Required column, check
265             condition in Provided column
266         length_req_calc = Math(inline=True)

```



```

3.4}'))
278     req_status = ""
279     length_condition.append(NoEscape(r'\end{
aligned}'))
280
281     self.report_check.append(
282         ["Required Length", length_req_calc,
length_condition, req_status])
283
284     #
=====
285     # SECTION 3.4: WELD LENGTH EXTENSION
286     #
=====
287     if L_req > width:
288         self.report_check.append([
289             "SubSection", "Weld Length Extension
", "|p{4cm}|p{4cm}|p{6.5cm}|p
{1.5cm}|"
290         ])
291
292     # 3.4.1: Skew Angle Method - show full
calculation
293     skew_calc_detail = Math(inline=True)
294     skew_calc_detail.append(NoEscape(r'\
begin{aligned}'))
295     skew_calc_detail.append(
296         NoEscape(r'L_{target} \&= \frac{L_{
req}}{n_f}\\'))
297     skew_calc_detail.append(
298         NoEscape(r'\&= \frac{' + str(L_req) +
r'}{' + str(N_f) + r'}\\'))
299     skew_calc_detail.append(
300         NoEscape(r'\&= ' + str(L_target) + r'
\text{ mm}\\'))
301     skew_calc_detail.append(
302         NoEscape(r'\&[\text{Ref. Section

```

```

303         3.4.1, Step 1}}'))
skew_calc_detail.append(NoEscape(r'\end{
    aligned}'))
304
305     self.report_check.append(
306         ["Target Length/Line", "",
          skew_calc_detail, ""])
307
308     # Calculate skew angle
309     if skew_angle > 0:
310         skew_angle_calc = Math(inline=True)
311         skew_angle_calc.append(NoEscape(r'\
          begin{aligned}'))
312         skew_angle_calc.append(
313             NoEscape(r'\alpha \&= \arctan\
              left(\frac{L_{target} - w}{2
              w}\right)\'))
314         skew_angle_calc.append(NoEscape(r'\&=
          \arctan\left(\frac{' + str(
315             L_target) + r' - ' + str(width)
          + r'}{2 \times ' + str(width)
          ) + r'}\right)\'))
316         skew_angle_calc.append(
317             NoEscape(r'\&= ' + f'{skew_angle
              :.1f}' + r'^\circ\'))
318
319     # Check constraints 20
        60
320     if skew_angle < 20:
321         skew_angle_calc.append(NoEscape(
322             r'\&\text{Since } \alpha <
              20^\circ, \text{ set } \
              alpha = 20^\circ\'))
323     elif skew_angle > 60:
324         skew_angle_calc.append(NoEscape(
325             r'\&\text{Since } \alpha >
              60^\circ, \text{ set } \
              alpha = 60^\circ\'))
326         skew_angle_calc.append(

```

```

327         NoEscape(r'&\text{(Proceed
           to Section 3.4.3)}\\'))
328
329     skew_angle_calc.append(
330         NoEscape(r'&[\text{Ref. Section
           3.4.1, Steps 3-4}]'))
331     skew_angle_calc.append(NoEscape(r'\
           end{aligned}'))
332
333     self.report_check.append(
334         ["Skew Angle", skew_angle_calc,
           f'{skew_angle:.1f} ', ""])
335
336     # 3.4.2: Provided weld length per
           line
337     L_prov_line_calc = Math(inline=True)
338     L_prov_line_calc.append(NoEscape(r'\
           begin{aligned}'))
339     L_prov_line_calc.append(
340         NoEscape(r'L_{provided\_line} &=
           w + 2w \times \tan(\alpha)
           \\'))
341     L_prov_line_calc.append(NoEscape(r'
           &= ' + str(width) + r' + 2 \
           times ' + str(
342         width) + r' \times \tan(' + f'{
           skew_angle:.1f}' + r'^\circ)
           \\'))
343     L_prov_line_calc.append(
344         NoEscape(r'&= ' + str(
           L_prov_line_calc) + r' \text{
           mm}\\'))
345     L_prov_line_calc.append(
346         NoEscape(r'&[\text{Ref. Section
           3.4.2, Step 1}]'))
347     L_prov_line_calc.append(NoEscape(r'\
           end{aligned}'))
348
349     self.report_check.append(

```

```

350         ["Provided Length/Line", "",
351         L_prov_line_calc, ""])
352
353     # 3.4.3: Side weld extension (if needed)
354     if side_weld_len > 0:
355         L_provided_total = L_provided_line *
356         N_f
357
358         side_calc = Math(inline=True)
359         side_calc.append(NoEscape(r'\begin{
360         aligned}'))
361         side_calc.append(
362         NoEscape(r'L_{side} \&= \frac{L_{
363         req} - L_{provided}}{n_f}\\'
364         ))
365         side_calc.append(NoEscape(
366         r'\&= \frac{' + str(L_req) + r' -
367         ' + str(L_provided_total) +
368         r'}{' + str(N_f) + r'}\\'))
369         side_calc.append(
370         NoEscape(r'\&= ' + str(
371         side_weld_len) + r' \text{
372         mm}\\'))
373
374         # Minimum return weld
375         min_return = max(2 * weld_size, 10)
376         side_calc.append(NoEscape(
377         r'\text{Min. return} \&= \max(2s,
378         10) = ' + str(min_return) +
379         r' \text{ mm}\\'))
380         side_calc.append(NoEscape(r'\&[\text{
381         Ref. Cl. 10.5.10.2}]'))
382         side_calc.append(NoEscape(r'\end{
383         aligned}'))
384
385         self.report_check.append(
386         ["Side Weld Length", side_calc,
387         f'{side_weld_len:.1f} mm', "
388         "]

```

```

374
375         #
           =====

376         # SECTION 3.5: WELD STRENGTH VERIFICATION
377         #
           =====

378         self.report_check.append([
379             "SubSection", "Weld Strength
                        Verification", "|p{4cm}|p{4cm}|p{6.5
                        cm}|p{1.5cm}|"
380         ])
381
382         # Effective length calculation (Section 3.5,
           Step 1)
383         eff_len_calc_detail = Math(inline=True)
384         eff_len_calc_detail.append(NoEscape(r'\begin
                        {aligned}'))
385         eff_len_calc_detail.append(
386             NoEscape(r'L_{eff} \&= L_{provided\_line}
                        - 2a\\'))
387         eff_len_calc_detail.append(NoEscape(
388             r'\&= ' + str(L_provided_line) + r' - 2 \
                        times ' + str(effective_throat) + r'
                        \\'))
389         eff_len_calc_detail.append(
390             NoEscape(r'\&= ' + str(L_eff_provided) +
                        r' \text{ mm}\\'))
391         eff_len_calc_detail.append(NoEscape(r'\end{
                        aligned}'))
392
393         self.report_check.append(
394             ["Effective Length", "",
                        eff_len_calc_detail, ""])
395
396         #
           =====

```

```

397 # SECTION 3.6: LONG JOINT REDUCTION FACTOR
398 #
=====
399 self.report_check.append([
400     "SubSection", "Long Joint Reduction
        Factor", "|p{4cm}|p{4cm}|p{6.5cm}|p
        {1.5cm}|"
401 ])
402
403 # Check condition:  $L_{eff} > 150a$ 
404 if L_eff_provided > 150 * effective_throat:
405     beta_req = Math(inline=True)
406     beta_req.append(NoEscape(r'\begin{
        aligned}'))
407     beta_req.append(
408         NoEscape(r'\text{Since } L_{eff} & >
        150 \times a\\'))
409     beta_req.append(NoEscape(
410         r'' + str(L_eff_provided) + r' & >
        150 \times ' + str(
        effective_throat) + r'\\'))
411     beta_req.append(NoEscape(
412         r'' + str(L_eff_provided) + r' & > '
        + f'{150 * effective_throat:.1f}
        ' + r'\\'))
413     beta_req.append(
414         NoEscape(r'\beta_L \&= 1.2 - \frac
        {0.2 \times L_{eff}}{150 \times
        a}\\'))
415     beta_req.append(NoEscape(r'\&= 1.2 - \
        frac{0.2 \times ' + str(
416         L_eff_provided) + r'}{150 \times ' +
        str(effective_throat) + r'}\\'))
        )
417     beta_calc_val = 1.2 - \
418         (0.2 * L_eff_provided) / (150 *
        effective_throat)
419     beta_req.append(

```

```

420         NoEscape(r'&= ' + f'{beta_calc_val
421             :.3f}') + r'\\')
422     beta_req.append(
423         NoEscape(r'&\text{(Ensure } \beta_L
424             \geq 0.8\text{)}}\\'))
425     beta_req.append(
426         NoEscape(r'\beta_L &= ' + f'{beta_L
427             :.2f}') + r'\\'))
428     beta_req.append(NoEscape(r'&[\text{Ref.
429         Cl. 10.5.7.1(b)}]'))
430     beta_req.append(NoEscape(r'\end{aligned}
431         '))
432     beta_status = "PASS" if beta_L >= 0.8
433         else "FAIL"
434 else:
435     beta_req = Math(inline=True)
436     beta_req.append(NoEscape(r'\begin{
437         aligned}'))
438     beta_req.append(
439         NoEscape(r'\text{Since } L_{\text{eff}} &
440             \leq 150 \times a\\'))
441     beta_req.append(NoEscape(r'' + str(
442         L_eff_provided) +
443         r' &\leq 150 \times ' +
444         str(effective_throat
445             ) + r'\\'))
446     beta_req.append(NoEscape(r'' + str(
447         L_eff_provided) +
448         r' &\leq ' + f'{150 *
449             effective_throat:.1f
450             }' + r'\\'))
451     beta_req.append(NoEscape(r'\beta_L &=
452         1.0\\'))
453     beta_req.append(NoEscape(r'&[\text{Ref.
454         Cl. 10.5.7.1(b)}]'))
455     beta_req.append(NoEscape(r'\end{aligned}
456         '))
457     beta_status = "PASS"

```

```

442     beta_prov = Math(inline=True)
443     beta_prov.append(NoEscape(r'\beta_L = ' + f'
444                               {beta_L:.2f}'))
445
446     self.report_check.append(
447         ["Reduction Factor", beta_req, beta_prov
448          , beta_status])
449
450     # Weld capacity with reduction factor (
451         Section 3.6, Equation 3.1)
452     weld_cap_calc = Math(inline=True)
453     weld_cap_calc.append(NoEscape(r'\begin{
454                               aligned}\\'))
455     weld_cap_calc.append(
456         NoEscape(r'C_w &= f_{wd}^{\adj} \times a
457                               \times L_{eff} \times n_f\\\\'))
458     weld_cap_calc.append(
459         NoEscape(r'&= (\beta_L \times f_{wd}) \
460                               \times a \times L_{eff} \times n_f
461                               \\\\\'))
462     weld_cap_calc.append(NoEscape(r'&= (' + f'{
463                               beta_L:.2f}' + r' \times ' + f'{f_w:.2f}
464                               ' + r') \times ' + str(
465                               effective_throat) + r' \times ' + str(
466                               L_eff_provided) + r' \times ' + str(
467                               N_f) + r'\\\\'))
468     weld_cap_calc.append(
469         NoEscape(r'&= ' + str(weld_strength_kN)
470                               + r' \text{ kN}\\'))
471     weld_cap_calc.append(NoEscape(r'\end{aligned
472                               }'))
473
474     self.report_check.append(["Weld Capacity", "
475                               ", weld_cap_calc, ""])
476
477     #
478     =====
479
480     # SECTION 3.7: BASE METAL STRENGTH CHECK

```

```

465         #
=====
466         self.report_check.append([
467             "SubSection", "Base Metal Strength Check
              ", "|p{4cm}|p{4cm}|p{6.5cm}|p{1.5cm}|"
              ]|")
468     ])
469
470     if is_comp:
471         # For compression - only yielding check
472         comp_calc_req = Math(inline=True)
473         comp_calc_req.append(NoEscape(r'\begin{
              aligned}\\'))
474         comp_calc_req.append(
475             NoEscape(r'T_{db} \&= \frac{A_g \
              times f_y}{\gamma_{m0}}\\'))
476         comp_calc_req.append(NoEscape(
477             r'T_{db} \&= \frac{' + f'{Ag:.1f}' +
              r' \times ' + str(fy) + r'}{' +
              str(gamma_m0) + r'}\\'))
478         comp_calc_req.append(
479             NoEscape(r'\&= ' + str(
              base_metal_capacity_kN) + r' \
              text{ kN}\\'))
480         comp_calc_req.append(
481             NoEscape(r'&[\text{Ref. Section 3.7,
              Cl. 7.1.2}]'))
482         comp_calc_req.append(NoEscape(r'\end{
              aligned}'))
483
484         comp_status = "PASS" if
              base_metal_capacity_kN >= axial_kN
              else "FAIL"
485         self.report_check.append(
486             ["Base Metal Capacity", axial_kN,
              comp_calc_req, comp_status])
487     else:
488         # For tension - show both calculations

```

```

489         and take min
490         ten_calc_req = Math(inline=True)
491         ten_calc_req.append(NoEscape(r'\begin{
492             aligned}\'))
493         ten_calc_req.append(NoEscape(
494             r'T_{db} \&= \min\left(\frac{A_g f_y}{\gamma_{m0}}, \frac{0.9 A_n f_u}{\gamma_{m1}}\right)\'))
495         ten_calc_req.append(NoEscape(r'\&= \min\left(\frac{
496             left(\frac{' + f'{Ag:.1f}' + r' \
497             times ' + str(fy) + r'}{' + str(
498             gamma_m0) + r'}, \frac{0.9 \times '
499             + f'{Ag:.1f}' + r' \times ' +
500             str(fu) + r'}{' + str(gamma_m1)
501             + r'}\right)\'))
502         ten_calc_req.append(
503             NoEscape(r'\&= \min(' + str(Tdg) + r'
504             , ' + str(Tdn) + r')\'))
505         ten_calc_req.append(
506             NoEscape(r'\&= ' + str(
507                 base_metal_capacity_kN) + r' \
508                 text{ kN}\'))
509         ten_calc_req.append(
510             NoEscape(r'\&[\text{Ref. Section 3.7,
511                 C1. 6.2, 6.3}]'))
512         ten_calc_req.append(NoEscape(r'\end{
513             aligned}'))
514
515         ten_status = "PASS" if
516             base_metal_capacity_kN >= axial_kN
517         else "FAIL"
518         self.report_check.append(
519             ["Base Metal Capacity", axial_kN,
520             ten_calc_req, ten_status])
521
522         #
523         =====
524
525         # SECTION 3.8: DETAILING CHECKLIST

```

```

509         #
=====
510         self.report_check.append([
511             "SubSection", "Detailing Checklist", "|p
                    {4cm}|p{4cm}|p{6.5cm}|p{1.5cm}|"
512         ])
513
514         # Check 1: Minimum effective weld length
515         detail_check_1 = Math(inline=True)
516         detail_check_1.append(NoEscape(r'\begin{
                    aligned}'))
517         detail_check_1.append(NoEscape(r'L_{eff} &\
                    geq 4s\\'))
518         detail_check_1.append(
519             NoEscape(r'' + str(L_eff_provided) + r'
                    &\geq ' + str(4 * weld_size)))
520         detail_check_1.append(NoEscape(r'\end{
                    aligned}'))
521         detail_status_1 = "PASS" if L_eff_provided
                    >= 4 * weld_size else "FAIL"
522         self.report_check.append(
523             ["Min. Eff. Length", detail_check_1, "",
                    detail_status_1])
524
525         # Check 2: Minimum weld size
526         detail_check_2 = Math(inline=True)
527         detail_check_2.append(NoEscape(r'\begin{
                    aligned}'))
528         detail_check_2.append(NoEscape(r's &\geq s_{
                    min}\\'))
529         detail_check_2.append(
530             NoEscape(r'' + str(weld_size) + r' &\geq
                    ' + str(s_min)))
531         detail_check_2.append(NoEscape(r'\end{
                    aligned}'))
532         detail_status_2 = "PASS" if weld_size >=
                    s_min else "FAIL"
533         self.report_check.append(

```

```

534         ["Min. Weld Size", detail_check_2, "",
           detail_status_2])
535
536     # Check 3: Maximum weld size
537     detail_check_3 = Math(inline=True)
538     detail_check_3.append(NoEscape(r'\begin{
           aligned}'))
539     detail_check_3.append(NoEscape(r's &\leq T_{
           min} - 1.5\\'))
540     detail_check_3.append(
541         NoEscape(r'' + str(weld_size) + r' &\leq
           ' + str(s_max)))
542     detail_check_3.append(NoEscape(r'\end{
           aligned}'))
543     detail_status_3 = "PASS" if weld_size <=
           s_max else "FAIL"
544     self.report_check.append(
545         ["Max. Weld Size", detail_check_3, "",
           detail_status_3])
546
547     # Check 4: Skew angle constraints (if
           applicable)
548     if skew_angle > 0:
549         detail_check_4 = Math(inline=True)
550         detail_check_4.append(NoEscape(r'\begin{
           aligned}'))
551         detail_check_4.append(
552             NoEscape(r'20^\circ &\leq \alpha \
           leq 60^\circ\\'))
553         detail_check_4.append(
554             NoEscape(r'20^\circ &\leq ' + f'{
           skew_angle:.1f}' + r'^\circ \leq
           60^\circ'))
555         detail_check_4.append(NoEscape(r'\end{
           aligned}'))
556         detail_status_4 = "PASS" if 20 <=
           skew_angle <= 60 else "FAIL"
557         self.report_check.append(
558             ["Skew Angle Range", detail_check_4,

```

```

559         "", detail_status_4])
560
561     # Check 5: Packing plate requirement
562     if N_f == 2:
563         if abs(plate1_thk - plate2_thk) > 0.001:
564             detail_check_5 = NoEscape(
565                 r'\text{Required: } |t_1 - t_2|
566                 > 0')
567             detail_prov_5 = f"Provided: {
568                 packing_thk} mm"
569             detail_status_5 = "PASS"
570         else:
571             detail_check_5 = NoEscape(
572                 r'\text{Not required: } t_1 =
573                 t_2')
574             detail_prov_5 = "N/A"
575             detail_status_5 = "PASS"
576         self.report_check.append(
577             ["Packing Plate", detail_check_5,
578              detail_prov_5, detail_status_5])
579
580     #
581     =====
582
583     # SECTION 3.9: DETAILING
584     #
585     =====
586
587     self.report_check.append([
588         "SubSection", "Detailing", "|p{4cm}|p{4
589         cm}|p{6.5cm}|p{1.5cm}|"
590     ])
591
592     # Length of connection
593     conn_len_detail = Math(inline=True)
594     conn_len_detail.append(NoEscape(r'\begin{
595         aligned}'))
596     conn_len_detail.append(
597         NoEscape(r'L_{provided} \&= n_f \times L_

```

```

        {provided\_line}\\')
587     conn_len_detail.append(
588         NoEscape(r'&= ' + str(N_f) + r' \times '
                    + str(L_provided_line) + r'\\')
589     L_provided_total = f2(N_f * L_provided_line,
        0.0)
590     conn_len_detail.append(
591         NoEscape(r'&= ' + str(L_provided_total)
                    + r' \text{ mm}'))
592     conn_len_detail.append(NoEscape(r'\end{
        aligned}'))
593     self.report_check.append(
594         ["Connection Length", "",
            conn_len_detail, ""])
595
596     # Length of cover plate (with clearance)
597     end_clearance = 25 # mm, as per Section 3.8
598     L_cover_plate = f2(L_provided_total + 2 *
        end_clearance, 0.0)
599     cover_len_detail = Math(inline=True)
600     cover_len_detail.append(NoEscape(r'\begin{
        aligned}'))
601     cover_len_detail.append(
602         NoEscape(r'L_{cp} &= L_{provided} + 2 \
                    times (\text{end clearance})\\')
603     cover_len_detail.append(NoEscape(
604         r'&= ' + str(L_provided_total) + r' + 2
                    \times ' + str(end_clearance) + r'\\
                    ')
605     cover_len_detail.append(
606         NoEscape(r'&= ' + str(L_cover_plate) + r
                    ' \text{ mm}'))
607     cover_len_detail.append(NoEscape(r'\end{
        aligned}'))
608     self.report_check.append(
609         ["Cover Plate Length", "",
            cover_len_detail, ""])
610
611     #

```

```

=====
612     # UTILIZATION RATIO
613     #
=====

614     self.report_check.append([
615         "SubSection", "Utilization Ratio", "|p{4
            cm}|p{4cm}|p{6.5cm}|p{1.5cm}|"
616     ])
617
618     overall_capacity_kN = min(weld_strength_kN,
        base_metal_capacity_kN)
619     utilization_ratio = f2(
620         axial_kN / overall_capacity_kN if
            overall_capacity_kN > 0 else 0, 0.0)
621
622     ur_calc = Math(inline=True)
623     ur_calc.append(NoEscape(r'\begin{aligned}'))
624     ur_calc.append(NoEscape(r'UR &= \frac{P_N}{\min(C_w, T_{db})}'))
625     ur_calc.append(NoEscape(r'&= \frac{' + str(
        axial_kN) + r'}{\min(' + str(
626         weld_strength_kN) + r', ' + str(
            base_metal_capacity_kN) + r')})'))
627     ur_calc.append(NoEscape(
628         r'&= \frac{' + str(axial_kN) + r'}{' +
            str(overall_capacity_kN) + r'})'))
629     ur_calc.append(NoEscape(r'&= ' + str(
        utilization_ratio) + r'))
630     ur_calc.append(NoEscape(r'&[\text{Ref. IS
        800:2007}]'))
631     ur_calc.append(NoEscape(r'\end{aligned}'))
632
633     ur_status = "PASS" if utilization_ratio <=
        1.0 else "FAIL"
634     self.report_check.append(
635         ["Utilization Ratio", f"{axial_kN:.2f}
            kN", ur_calc, ur_status])

```

```

636
637         #
        =====
638         # GENERATE LATEX REPORT
639         #
        =====

640         Disp_2d_image = []
641         Disp_3D_image = "/ResourceFiles/images/3d.
            png"
642         rel_path = os.path.abspath(".").replace("\\",
            , "/" )
643         fname_no_ext = popup_summary.get(
644             "filename", "ButtJointWeldedReport")
645         folder = popup_summary.get('folder', './
            reports')
646         os.makedirs(folder, exist_ok=True)
647
648         CreateLatex.save_latex(
649             CreateLatex(), self.report_input, self.
                report_check,
650             popup_summary, fname_no_ext, rel_path,
                Disp_2d_image, Disp_3D_image,
651             module=self.module
652         )
653         self.logger.info(
654             f"Report generated successfully: {
                fname_no_ext}.pdf")
655         return True
656
657     except Exception as e:
658         print(f"WARNING in save_design(): {e}")
659         import traceback
660         traceback.print_exc()
661         return False
662 %----- end code -----

```

6.3.1 Explanation of the Code

The `save_design` function for the welded butt joint is responsible for converting the completed design into a structured LaTeX report. Its main steps are:

1. **Collecting Input and Output Data:** All relevant information stored in the `ButtJointWelded` object is gathered. This includes: plate dimensions and material properties, weld size and type, cover plate details (if any), design axial force, weld and base metal capacities, and final utilization ratios.
2. **Checking Design Status:** The function reads the internal `design_status` flag.
3. If the design is *UNSAFE*, it prepares a short report summarizing the failure reason (for example, “weld capacity required factored load” or “base metal utilization > 1.0 ”).
4. If the design is *SAFE*, it proceeds to create a complete, stepwise report.
5. **Preparing report_input and Design Checks:** A dictionary `report_input` is created to pass all numerical values and text labels to the LaTeX template. Typical entries cover:
 6. Connection description and input summary,
 7. Weld design: permissible weld size range, chosen weld size, design weld strength, required and provided weld length, long-joint reduction factor (if applicable),
 8. Base metal strength in tension or compression,
 9. Final design strength and overall utilization ratio.

In parallel, a list of design checks (DDCL-style) is assembled, where each check stores its name, governing formula, numerical substitution and PASS/FAIL status for tabular presentation.

10. **Formatting LaTeX Equations:** Important formulas are written as LaTeX math strings, often wrapped with `NoEscape`, for

example:

$$f_w = \frac{f_u}{\sqrt{3} \gamma_{mw}}, \quad P_{\text{weld}} = A_{\text{weld}} f_w,$$

and the comparison of applied force with weld and plate capacities. This allows the report to display both the general equation and the corresponding numerical substitution.

11. **File Handling and PDF Generation:** Finally, the function sets up the output directory (creating it if required), and calls the common `CreateLatex.save_latex` routine. This compiles the LaTeX file into a professional PDF report that includes input summary, detailed calculation steps, design check table and conclusion for the welded butt joint.

6.4 Documentation

The directory structure used for the Report Generation is organized as follows:

```
src/osdag_core
```

```
design_report/  
    reportGenerator_latex.py
```

```
design_type/  
    connection/  
        butt_joint_welded.py
```

```
Report_functions.py
```

Program Start Calls The main entry point for the program is `osdag_gui`. To start the program, open the Osdag folder, go to src and start the terminal with that path, execute the following command from the project root:

```
$ python -m osdag_gui
```

6.5 References

- Osdag Github repository: <https://osdag.github.io/>
- IS 800:2007, "General Construction in Steel Code of Practice of Practice"

Chapter 7

Standardization of Report Generation Infrastructure

7.1 Problem Statement

The objective was to refine the global report generation engine (`reportGenerator_la`) to provide a more professional and readable output for all Osdag modules. Key challenges included implementing an adaptive table layout for modules with varying data complexity and ensuring that legal disclaimers regarding designer responsibility are present in every generated document.

7.2 Tasks Done

7.2.1 Global Infrastructure Enhancements

Adaptive 2-Column Layout Implementation

The engine was updated to automatically detect modules that do not require complex 5-column image-integrated tables. For these modules, a balanced 2-column layout (9cm for Keys, 7.5cm for Values) was implemented to maximize scannability.

Standardized Legal Disclaimer (Note Section)

A mandatory "Note" section was added to the footer of every report

using a `Tabularx` environment. This section clarifies that while `Osdag` assists in design, the final structural safety and code compliance remain the responsibility of the individual designer.

Enhanced Character Wrapping Logic

The text-wrapping logic was recalibrated for the new 2-column format, increasing the character threshold to 65 characters before triggering a multi-row split, ensuring cleaner table aesthetics.

7.3 Python Code (reportGenerator_latex.py)

The following snippets illustrate the global changes applied across all `Osdag` modules.

Listing 7.1: Standardized Note and Adaptive Layout Logic

```
# Logic for simplified 2-column layout in all modules
else:
    # Use a wider 2-column table for simple modules (approx 17cm width)
    with doc.create(LongTable('|p{9cm}|p{7.5cm}|',
        row_height=1.2)) as table:
        table.add_hline()
        for i in uiObj:
            if uiObj[i] == "TITLE":
                table.add_row((MultiColumn(2, align='|c|',
                    data=bold(i), )),)
            else:
                table.add_row((NoEscape(i), uiObj[i]))
        table.add_hline()

# Standardized Note added at the end of all reports
doc.append(pyl.Command('vspace', arguments='10mm'))
with doc.create(Tabularx('|X|', row_height=1.5)) as
    table:
        table.add_hline()
        table.add_row((MultiColumn(1, align='|c|', data=bold
            ('Note')),), color='OsdagGreen')
        table.add_hline()
```

```
table.add_row([NoEscape(r'The sharing of unabridged  
Osdag design reports is encouraged... The output  
shall be owned by the designer...')])  
table.add_hline()
```

7.4 Documentation

The updated report generation system is organized within the following directory structure:

```
src/osdag/  
  design_report/  
    reportGenerator_latex.py    # Global engine with Note & Layout upd
```

7.5 References

- Osdag GitHub repository: <https://osdag.github.io/>
- IS 800:2007, "General Construction in Steel — Code of Practice"

Chapter 8

Conclusions

8.1 Tasks Accomplished

During the course of the screening task and report generation, the following key tasks were accomplished:

- **Developed the design report generation mechanism for Bolted Lap Joint Connections:** Implemented the complete workflow to capture user inputs (plate dimensions, bolt grade, load) and generate a detailed design report.
- Created algorithms to verify shear capacity of bolts in single shear planes.
- Integrated logic for checking minimum and maximum edge distances based on hole type (standard/oversized).
- Automated the block shear failure check for the specific geometry of lap joints.
- **Developed the design report generation mechanism for Bolted Butt Joint Connections:** Successfully implemented the comprehensive `save_design()` mechanism for butt joints, handling complex interaction checks.
- Coded logic for Cover Plate thickness verification ($5/8T_{min}$ vs $9/16T_{min}$) per IS 800:2007.
- Implemented capacity reduction factors for packing plates (β_{pkg}), long

- joints (β_{lj}), and large grips (β_{lg}).
- Enabled dynamic mathematical rendering of "Required" vs "Provided" values for transparency.
- **Developed the design report generation mechanism for Welded Lap Joint Connections:** Engineered the reporting logic for fillet welds in lap configurations.
- Implemented checks for effective throat thickness ($0.7 \times s$) and minimum weld size based on plate thickness.
- Developed logic to calculate weld strength per unit length and determine the required effective length.
- Added validation for end returns ($2 \times s$) to ensuring detailing compliance in the final report.
- **Updated the design report generation of Welded Butt Joint Connections:** Refined the existing module to support dual-force scenarios (Compression and Tension).
- Differentiated design strength calculations for Complete Joint Penetration (CJP) groove welds in tension vs. compression.
- Implemented site weld reduction factors where applicable.
- Updated the L^AT_EX template to dynamically display "Axial Tensile Force" or "Axial Compressive Force" labels based on the input load case.
- **Enhanced Global Report Infrastructure:** Upgraded the core `reportGenerator_latex.py` engine to support adaptive layouts, automatically switching between complex 5-column tables and optimized 2-column layouts based on input data complexity.
- **Implemented Standardized Legal Framework:** Integrated a mandatory "Note" section in the footer of all generated reports to clarify design responsibility, ensuring professional compliance across all Osdag modules.

8.2 Skills Developed

Working on the bolted lap joint, bolted butt joint, welded lap joint, welded butt joint modules, and the global report infrastructure helped in developing a broad set of technical and professional skills. These can be grouped as follows:

1. Advanced Python Programming and Software Engineering

- **Modular and Object-Oriented Design:** Designed separate classes and functions for each connection type, clearly separating responsibilities such as input handling, design calculations, checks, and report generation. This improved understanding of encapsulation, cohesion, and reusability.
- **Adaptive Algorithm Design:** Designed logic to dynamically analyze input dictionaries and select the appropriate table structure (Standard vs. Complex) for the report. This honed skills in writing flexible, context-aware code that handles varying data structures gracefully.
- **Global vs. Modular Architecture:** Learned to modify core infrastructure files (`reportGenerator_latex.py`) to effect global changes (like the Legal Note) while ensuring backward compatibility with individual connection modules.
- **Clean Data Flow and Validation:** Implemented structured methods to collect and validate inputs (plate dimensions, bolt/weld properties, loads), managing default values and providing clear feedback on invalid data.
- **Error Handling and Robustness:** Used conditional checks and try-except patterns to handle runtime issues (file paths, division by zero), improving code resilience.

2. L^AT_EX-Based Report Generation and Mathematical Communication

- **Dynamic Table Environment Management:** Gained proficiency in programmatically manipulating complex L^AT_EX environments like LongTable and Tabularx via Python. Learned to control column widths and row heights dynamically based on data content.
- **Automated Document Styling:** Mastered the use of PyLaTeX to inject standardized styling elements (such as OsdagGreen color headers and legal footers) consistently across different report types.
- **Dynamic Equation Formatting:** Used tools like NoEscape to embed Python variables into L^AT_EX math expressions, enabling the display of "Required" vs. "Provided" values side-by-side. This is critical for creating verifiable calculation proofs.
- **Clear Presentation of Design Checks:** Structured output so that key checks (shear, bearing, yielding, rupture) appear with equations and status (PASS/FAIL), strengthening technical documentation skills.

3. Structural Design and Code Interpretation Skills

- **Complex Connection Constraints (IS 800:2007):** Deepened understanding of specific code provisions for Butt Joints, specifically the logic for Cover Plate thickness ($5/8T_{min}$ vs $9/16T_{min}$) and the application of Shear Capacity reduction factors (β_{pkg}) for packing plates.
- **Connection Design Logic:** Implemented stepwise design procedures for both Bolted connections (shear/bearing capacity, detailing limits) and Welded connections (weld size limits, effective throat). This strengthened the ability to move from codal equations to executable design logic.
- **Utilization Ratio and Safety Assessment:** Developed a consistent approach for calculating utilization ratios and identifying the

governing failure mode to clearly communicate safety margins.

- **Practical Detailing Awareness:** By coding checks for minimum/-maximum edge distances, pitch, gauge, and weld geometry, gained an appreciation of how theoretical design interacts with fabrication constraints.

4. General Professional and Problem-Solving Skills

- **Algorithmic Thinking:** Broke down complex design procedures into smaller logical steps and implemented them systematically.
- **Systematic Debugging:** Resolved issues related to file I/O permissions and cross-platform path handling when generating PDFs, enhancing troubleshooting skills for desktop application development.
- **Interdisciplinary Integration:** Combined knowledge of structural engineering, programming, and technical writing to deliver a complete tool chain from input to final report.

Chapter A

Appendix

A.1 Work Reports

Internship Work Report			
NAME		ROUSHAN RAJ	
PROJECT		OSDAG	
Internship Work Report		FOSSEE Winter Fellowship 2025	
Week	Dates (2025-26)	Key Tasks Accomplished	Hours Worked
		Bolted Lap Joint Report Generation: • Implemented save_design() for Bolted Lap Joints. • Added logic for shear capacity and bearing checks. • Validated pitch/gauge/edge distance inputs.	
Week 1	Dec 1 – Dec 7		40
		Bolted Lap Joint Refinement: • Integrated Block Shear Failure checks (Cl 6.4). • Fixed edge case bugs in "Standard" vs "Oversized" holes. • Added dynamic math rendering for utilization ratios.	
Week 2	Dec 8 – Dec 14		42
		Welded Lap Joint Module: • Developed report logic for Fillet Welds in Lap configuration. • Implemented Effective Throat and Length checks. • Validated End Return requirements.	
Week 3	Dec 15 – Dec 21		38
		Welded Butt Joint (Groove Welds): • Updated existing module to handle both Tension & Compression. • Differentiated CJP weld strength for different load cases. • Implemented Site Weld reduction factors.	
Week 4	Dec 22 – Dec 28		40

		Bolted Butt Joint (Initial): • Started save_design() implementation for Bolted Butt Joints. • Coded logic for Single vs. Double Cover Plate thickness.	
Week 5	Dec 29 – Jan 4	• Setup 5-column layout for complex image integration.	35
		Bolted Butt Joint (Advanced): • Implemented Capacity Reduction Factors. • Added logic for packing plates > 6mm.	
Week 6	Jan 5 – Jan 11	• Refined utilization ratio logic for combined checks.	45
		Global Infrastructure Update (Part 1): • Analyzed reportGenerator_latex.py for layout limitations. • Developed "Adaptive Layout" logic to switch between 5-col and 2-col table	
Week 7	Jan 12 – Jan 18	• Tested simple modules with new 2-col layout.	40
		Global Infrastructure Update (Part 2): • Implemented standardized "Legal Note" footer for all reports. • Fixed text-wrapping issues for long strings in 2-col layout.	
Week 8	Jan 19 – Jan 25	• Validated changes across all 4 connection modules.	42
		Final Documentation & Testing: • Documented all code changes (Tasks Accomplished). • Final dry-run of all modules to ensure stability.	
Week 9	Jan 26 – Jan 31	• Prepared Fellowship Report LaTeX content.	36
Total			358

Bibliography

- [1] Siddhartha Ghosh, Danish Ansari, Ajmal Babu Mahasrankintakam, Dharma Teja Nuli, Reshma Konjari, M. Swathi, and Subhrajit Dutta. Osdag: A Software for Structural Steel Design Using IS 800:2007. In Sondipon Adhikari, Anjan Dutta, and Satyabrata Choudhury, editors, *Advances in Structural Technologies*, volume 81 of *Lecture Notes in Civil Engineering*, pages 219–231, Singapore, 2021. Springer Singapore.
- [2] FOSSEE Project. FOSSEE News - January 2018, vol 1 issue 3. Accessed: 2024-12-05.
- [3] FOSSEE Project. Osdag website. Accessed: 2024-12-05.