



Summer Fellowship Report

On

Development of Thermodynamic Models and Functions in
OpenModelica

Submitted by

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Chapter 1

Introduction

“OpenModelica” is a free and open-source modelling environment that uses “Modelica” modelling language. It follows equation oriented approach. OpenModelica can be used for modelling, simulation, optimization and analysis of complex steady state and dynamic systems. Modelica modelling language allows users to express a system in the form of equations. OpenModelica compiles expressions, equations, functions and algorithms into efficient C code. The generated C code is combined with a library of utility functions, a run-time library, and a numerical Differential-Algebraic Equation (DAE) solver. OpenModelica Connection Editor, called as OMEdit is the integrated Graphical User Interface (GUI) in OpenModelica for graphical modelling and editing. OMEdit consists of several libraries for various domains like Electrical, Magnetic, Math, Thermal, etc. It provides various user friendly features like representation of a model in the form of block diagrams. OMEdit can be used for creating custom models and for editing or drawing connections between the model interfaces. It also allows users to plot graphs between parameters of the model simulated.

Chapter 2

Background

OMEdit, the integrated Graphical User Interface (GUI) of OpenModelica consists of libraries across various domains such as Electrical, Thermal, Math, Mechanics, etc. that can be used to develop models of a physical system or process. However, OMEdit does not contain libraries for modelling of chemical process systems. This limits the use of OpenModelica for modelling chemical process systems. Hence, it becomes necessary to build models or packages that aids in modelling of chemical process systems. An essential requirement is the availability of thermodynamic packages to estimate fluid properties. The main aim of this work is to develop standard thermodynamic packages in OpenModelica. In this work, a thermodynamic package, namely "Extended UNIQUAC developed in OpenModelica. In order to develop thermodynamic packages in OpenModelica, properties such as critical temperature, critical pressure, acentric factor, molecular weight, etc. of the components that constitutes the system are required. For now, we are not using the electrolytes present in DWSIM but relying only on the current database of OpenModelica. The developed thermodynamic packages can be used to calculate fugacity coefficient and activity coefficient of solutions. This package was designed for the use of electrolytic solutions which involve water as well as some limited number of ionic compounds.

Chapter 3

Entropy Function

3.1 Description

We can think of Entropy as a measure of randomness or disorder in an isolated system. Entropy can be measured in two possible ways i.e. absolute entropy and relative entropy. Absolute entropy can be measured using statistical method, whereas the relative entropy is more related with the heat involved in the process, thus making it a thermodynamic process. Entropy is a state function just like Enthalpy, Internal Energy, thus independent of path. Entropy of a system is maximum when it reaches equilibrium, thus the change in entropy becomes zero. Under isothermal conditions, the total entropy of a system in reversible process is zero while in an irreversible process it is never zero, this is not the case with change in Internal Energy which remains zero for both processes.

3.2 Equations

Entropy equation for an ideal gas can be derived using the first law of thermodynamics

$$dU = dq + dw$$

at constant volume, $W = 0$
thus

$$dU_v = dq_v = nc_v dT$$

Assuming a monoatomic gas, where only translational energies are present ,

$$c_v = \frac{3}{2}R$$

here, R can be substituted with equation of state for ideal gases and thus

$$dU_v = \frac{3}{2}pV \frac{dT}{T}$$

Integrating the equation gives,

$$\Delta U_v = \frac{3}{2}pV \int_{T_i}^{T_f} \frac{dT}{T} = \frac{3}{2}pV \ln \frac{T_f}{T_i}$$

Employing equation of state in the above equation,

$$\Delta U_v = nc_v T \ln \frac{T_f}{T_i}$$

This equation contains the expression of entropy for constant volume.

$$\Delta S_v = nc_v \ln \frac{T_f}{T_i}$$

Internal Energy then,

$$\Delta U_v = \Delta q_v = T \Delta S_v$$

At constant temperature the heat term is zero,

$$dU_T = dw = -pdV$$

Substituting equation of state and integrating the above equation we get,

$$\Delta U_T = -nRT \int_{V_i}^{V_f} \frac{dV}{V} = -nRT \ln \frac{V_f}{V_i}$$

Hence, the expression of entropy for constant temperature

$$\Delta S_T = nR \ln \frac{V_f}{V_i}$$

Thus, internal energy becomes,

$$\Delta U_T = \Delta w = -T \Delta S_T$$

$$\Delta U_T = \Delta q_v + \Delta w = \Delta U_v + \Delta U_T = T \Delta S_v - T \Delta S_T = T(\Delta S_v - \Delta S_T)$$

$$\Delta Q = \Delta q_v - \Delta w = T \Delta S_v - (-T \Delta S_T) = T(\Delta S_v + \Delta S_T)$$

Summing the two parts,

$$\Delta S = \Delta S_v + \Delta S_T$$

Heat equation then,

$$\Delta Q = T \Delta S$$

Finally,

$$\Delta S = \frac{\Delta Q}{T}$$

3.3 Development

The equation is basically obtained from Maxwell's relations

$$Sm(T, P) = Sm(T_0, P_0) + \int_{T_0}^T \frac{C_{pm}}{T} dT - R \ln(P/P_0)$$

$$C_{pm} = Cp_0 + Cp_1 * T + Cp_2 * T^2 + Cp_3 * T^3$$

The routine of this equation was basically referred from the DWSIM source code, which is available on GitHub as well as on Visual Studio. The code previously developed on OpenModelica had two separate equations for entropy. The equations involved are liquid phase entropy and gas phase entropy out of which the liquid phase entropy had a correction term missing. After searching through the code of entropy function in visual basic we across a term which involved liquid density as well as temperature and pressure. This term was added to the previous equation of liquid phase entropy equation and there was a significant improvement in the accuracy of the values obtained.

3.4 Table

Compound	OpenModelica (kJ/kg K)	DWSIM (kJ/kg K)	Error Percentage
Benzene - Toluene	-1.32887	-1.3284	0.04%
Acetone - 1-Propanol	-2.10373	-2.1037	0.00%
N-Octane - N-Nonane	-1.14877	-1.14862	0.01%

Chapter 4

Extended UNIQUAC

4.1 Description

Extended UNIQUAC (Universal QuasiChemical) is a thermodynamic (activity coefficient) model, specially designed for electrolyte solutions (both aqueous solutions and mixed solvents). The model has proven itself applicable for calculations of vapor-liquid-liquid-solid equilibria and of thermal properties in aqueous solutions containing electrolytes and non-electrolytes. The extended UNIQUAC model consists of three terms: a combinatorial or entropic term, a residual or enthalpic term and an electrostatic term. The combinatorial and the residual terms are identical to the terms used in the traditional UNIQUAC equation (ref 3 and 4). The electrostatic term corresponds to the extended Debye-Hückel law. The combinatorial, entropic term is independent of temperature and only depends on the relative sizes of the species.

4.2 Equations

As said earlier, the extended UNIQUAC model consists of three terms: a combinatorial or entropic term, a residual or enthalpic term and an electrostatic term. They are:

$$G^{ex} = G_{combinatorial}^{ex} + G_{residual}^{ex} + G_{ExtendedDebye-Huckel}^{ex}$$

$$\frac{G_{combinatorial}^{ex}}{RT} = \sum x_i \ln \frac{\phi_i}{x_i} - \frac{z}{2} \sum q_i x_i \ln \frac{\phi_i}{\theta_i}$$

$$\phi_i = \frac{x_i r_i}{\sum_j x_j r_j}; \theta_i = \frac{x_i q_i}{\sum_j x_j q_j}$$

$$\frac{G_{residual}^{ex}}{RT} = - \sum_i (x_i q_i \ln (\sum_j \theta_j \psi_{ji}))$$

$$\psi_{ji} = \exp^{-(u_{ji} - u_{ii})/T}$$

$$u_{ji} = u_{ij} = u_{ij}^0 + u_{ij}^T(T - 298.15)$$

$$\ln\gamma_i^C = \ln\frac{\phi_i}{x_i} + 1 - \frac{\phi_i}{x_i} - \frac{z}{2}q\left[\ln\frac{\phi_i}{\theta_i} + 1 - \frac{\phi_i}{\theta_i}\right]$$

$$\ln\gamma_i^R = q_i\left[1 - \ln\left(\sum_j \theta_j\psi_{ji}\right) - \sum_j \frac{\theta_i\phi_{ij}}{\sum_k \theta_k\psi_{kj}}\right]$$

$$\ln\gamma_i^{C\infty} = \ln\frac{r_i}{r_w} + 1 - \frac{r_i}{r_w} - \frac{z}{2}q_i\left[\ln\frac{r_iq_w}{r_wq_i} + 1 - \frac{r_iq_w}{r_wq_i}\right]$$

$$\ln\gamma_i^{R\infty} = q_i[1 - \ln\psi_{wi} - \psi_{iw}]$$

$$\ln\gamma_w^{DH} = \frac{2}{3}M_wAI^{\frac{3}{2}}\sigma(bI^{\frac{1}{2}})$$

$$\sigma(x) = \frac{3}{x^3}1 + x - \frac{1}{1+x} - 2\ln(1+x)$$

$$\ln\gamma_i^{*DH} = -Z_i^2 \frac{A\sqrt{I}}{1+b\sqrt{I}}$$

$$A = [1.131 + 1.335 * 10^{-03}(T - 273.15) + 1.164 * 10^{-05}(T - 273.15)^2](kg/kmol)$$

$$\ln\gamma_w = \ln\gamma_w^C + \ln\gamma_w^R + \ln\gamma_w^{DH}$$

$$\ln\gamma_i^* = \ln\frac{\gamma_i^C}{\gamma_i^{C\infty}} + \ln\frac{\gamma_i^R}{\gamma_i^{R\infty}} + \ln\gamma_i^{*DH}$$

4.3 Development

This model is quite similar to the UNIQUAC model when we consider the residual and combinatorial terms in the model, and in addition to that we have used an electrostatic term which is also called as Debye-Huckel Law term. This term is used for calling out the interaction parameters of the ionic elements which will be used during the simulation for instance a two component system containing *water - Na⁺ or Na⁺ - I⁻* for which interaction parameters are completely different from that of other compounds(organic mostly) and thus the need of Debye-Huckel Law arises.

If at all the compounds contain organic/water elements then the system would basically call out the UNIQUAC interaction parameters. Thus, in OpenModelica we will use the UNIQUAC interaction parameters only as for now since we don't have the ionic element database and their corresponding parameters. Here, the mixture will comprise of water and organic compound because of which the interaction parameters of the mixture will become zero, this will cause residual term in the activity

coefficient to become zero, as of now we are not using ionic compounds thus the Debye-Huckel term will also cease to exist. Hence, we will be left with only combinatorial term which will give us the activity coefficient and hence the fugacity coefficient.

4.4 Table

	Activity Coefficient		Fugacity Coefficient		Error %age
	OpenModelica	DWSIM	OpenModelica	DWSIM	
Methanol	1.04062	1.0694536	1.71366	1.90565	11.20350595
Ethanol	1.07305	1.119691256	1.03971	1.18511	13.9846688
Water	1.25837	1.2065084	0.539727	0.556549	3.116760881

Chapter 5

Conclusion

Entropy function contains liquid and gas entropy equations, out of which the liquid equation was missing the liquid density correction factor which was forced upon in DWSIM, we added that term to the liquid entropy formula and figured out the output values in OpenModelica as well as DWSIM and compared them.

Extended UNIQUAC model is used for electrolytic compounds to obtain activity coefficients and fugacity coefficients respectively. If we use compounds other than ions, provided they contain water we can still use the model. But there will be a difference between the Extended UNIQUAC and UNIQUAC results. This difference is due to the reduction of the residual term in Extended model when we use organic compounds with water and ions are not present. We have implemented the same in the OpenModelica.

There was an erroneous routine followed in the calculation of the residual term in UNIQUAC thermodynamic model which was giving inaccurate values of fugacity coefficients that was also solved.

Reference

- B. Sander; P. Rasmussen and Aa. Fredenslund, "Calculation of Solid-Liquid Equilibria in Aqueous Solutions of Nitrate Salts Using an Extended UNIQUAC Equation". *Chemical Engineering Science*, 41(1986)1197-1202
- Thomsen, K., *Aqueous electrolytes: model parameters and process simulation*, Ph.D. Thesis, Department of Chemical Engineering, Technical University of Denmark, 1997.
- GitHub - Source Code DWSIM

Chapter 6

OpenModelica Code

```
1 function SId.FuncENTROPY
2
3   import Modelica.Constants.*;
4
5   input Real AS;
6   input Real VapCp[6];
7   input Real HOV[6];
8   input Real Tb;
9   input Real Tc;
10  input Real T;
11  input Real P;
12  input Real x;
13  input Real y;
14  input Real Phase_Density;
15  output Real Sliq, Svap;
16 protected
17  parameter Real Tref = 298.15, Pref = 101325;
18  Real Entr, Cp[n - 1];
19  parameter Integer n = 10;
20
21 algorithm
22  Entr := 0;
23  for i in 1:n - 1 loop
24    Cp[i] := Simulator.Files.Thermodynamic_Functions.VapCpId(VapCp, 298.15
25      + i * (T - 298.15) / n) / (298.15 + i * (T - 298.15) / n);
26  end for;
27  if T >= Tref then
28    Entr := (T - 298.15) * (Simulator.Files.Thermodynamic_Functions.VapCpId
29      (VapCp, T) / (2 * T) + sum(Cp[:]) +
30      Simulator.Files.Thermodynamic_Functions.VapCpId(VapCp, 298.15) / (2
31      * 298.15)) / n;
32  else
33    Entr := -(T - 298.15) * (
34      Simulator.Files.Thermodynamic_Functions.VapCpId(VapCp, T) / (2 * T)
35      + sum(Cp[:]) + Simulator.Files.Thermodynamic_Functions.VapCpId(
36      VapCp, 298.15) / (2 * 298.15)) / n;
37  end if;
38  if x > 0 and y > 0 then
39    Sliq := Entr - R * log(P / Pref) - R * log(x) - HV(HOV, Tc, T) / T + P
40      /1000/Phase_Density/T;
41    Svap := Entr - R * log(P / Pref) - R * log(y);
42  elseif x <= 0 and y <= 0 then
43    Sliq := 0;
44    Svap := 0;
45  elseif x == 0 then
46    Sliq := 0;
```

```

39     Svap := Entr - R * log(P / Pref) - R * log(y);
40 elseif y == 0 then
41     Sliq := Entr - R * log(P / Pref) - R * log(x) - HV(HOV, Tc, T) / T + P
        /1000/Phase_Density/T;
42     Svap := 0;
43 else
44     Sliq := 0;
45     Svap := 0;
46 end if;
47
48 end Sid.FuncENTROPY;

```

```

1 model EXT_UNIQUAC
2 //Libraries
3 import Simulator.Files.*;
4 //Parameter Section
5 //Binary Interaction Parameters
6 //Function :BIP_UNIQUAC is used to obtain the interaction parameters
7 parameter Real a[NOC, NOC] = Thermodynamic_Functions.BIP_UNIQUAC(NOC,
    comp.name);
8 //Uniquac Parameters R and Q called from Chemsep Database
9 parameter Real R[NOC] = comp.UniquacR;
10 parameter Real Q[NOC] = comp.UniquacQ;
11 parameter Integer Z = 10 "Compressibility-Factor";
12 //Variable Section
13 Real tow[NOC, NOC] "Energy interaction parameter";
14 //Intermediate variables to calculate the combinatorial and residual
    part of activity coefficient at the input conditions
15 Real r(each start=2, min=0,max=1), q(each start=2);
16 Real teta[NOC];
17 Real S[NOC](each start = 1);
18 Real sum[NOC];
19 //Activity Coefficients
20 Real gammac[NOC](each start = 1.2) "Combinatorial Part of activity
    coefficient at input conditions";
21 Real gammar[NOC](each start = 1.2) "Residual part of activity
    coefficient at input conditions";
22 Real gamma_new[NOC](each start = 1.2);
23 Real gamma[NOC](each start = 1.2) "Activity coefficient with Poynting
    correction";
24 //Fugacity coefficient
25 Real phil[NOC](each start = 0.5) "Fugacity coefficient at the input
    conditions";
26 //Dew Point Calculation Variables
27 // Real dewLiqMolFrac[NOC](each start=0.5, each min=0, each max=1);
28 //Intermediate variables to calculate the combinatorial and residual
    part of activity coefficient at dew point
29 // Real r_dew(start=2), q_dew(start=2);
30 // Real teta_dew[NOC](each start=2);
31 // Real S_dew[NOC](each start = 1);
32 // Real sum_dew[NOC](each start=2);
33 //Activity Coefficients
34 // Real gammac_dew[NOC](each start = 5) "Combinatorial Part of activity
    coefficient at dew point";
35 // Real gammar_dew[NOC](each start = 2.5) "Residual part of activity
    coefficient at dew point";
36 // Real gammaDew_old[NOC](each start = 2.2) "Combinatorial Part of
    activity coefficient (without correction)";
37 Real gammaDew[NOC](each start = 2.2) "Activity coefficient at dew point"
    ;
38 //Fugacity coefficient
39 Real vapfugcoeff_dew[NOC] "Vapour Fugacity coefficient at dew point";
40 // Real phil_dew[NOC](each start = 0.5);

```

```

41 // Real PCF_dew[NOC] "Poynting Correction Factor";
42 //Bubble Point Calculation Variables
43 //Intermediate variables to calculate the combinatorial and residual
    part of activity coefficient at bubble point
44 // Real r_bubl(start=2), q_bubl(start=2);
45 // Real teta_bubl[NOC];
46 // Real S_bubl[NOC];
47 // Real sum_bubl[NOC];
48 // Activity Coefficients
49 // Real gammac_bubl[NOC](each start = 2) "Combinatorial Part of activity
    coefficent at bubble point";
50 // Real gammar_bubl[NOC](each start = 1) "Residual part of activity
    coefficent at bubble point";
51 // Real gammaBubl_old[NOC](each start = 1) "Combinatorial Part of
    activity coefficient (without correction)";
52 Real gammaBubl[NOC](each start = 1) "Activity coefficient at bubble point
    ";
53 //Fugacity coefficient
54 Real liqfugcoeff_bubl[NOC];
55 //Real phil_bubl[NOC](each start = 0.5) "Liquid Phase Fugacity
    coefficient";
56 // Real PCF_bubl[NOC] "Poynting Correction Factor";
57 //Phase Envelope
58 Real Psat[NOC](each unit = "Pa") "Saturated Vapour Pressure at the
    input temperature";
59 Real PCF[NOC] "Poynting correction factor";
60 Real K[NOC](each start = 0.7) "Distribution Coefficient";
61 //Residual Energy Parameters
62 Real resMolSpHeat[3], resMolEnth[3], resMolEntr[3];
63 //Transport Properties at the input conditions
64 Real Density[NOC](each unit = "kmol/m^3");
65 Real A[NOC], B[NOC], D[NOC], E[NOC], Ff[NOC];
66 Real C[NOC];
67 // Real A_bubl[NOC], B_bubl[NOC], C_bubl[NOC], D_bubl[NOC], E_bubl[NOC],
    F_bubl[NOC];
68 // Real A_dew[NOC], B_dew[NOC], C_dew[NOC], D_dew[NOC], E_dew[NOC], F_dew[NOC
    ];
69 //

```

```

70 //Equation Section
71 equation
72 //Fugacity coefficients set to 1 since the model type is Activity
    Coefficient
73 for i in 1:NOC loop
74     gammaBubl[i] = 1;
75     gammaDew[i] = 1;
76     liqfugcoeff_bubl[i] = 1;
77     vapfugcoeff_dew[i] = 1;
78 end for;
79
80
81
82 //Calculation of Intermediate parameters to evaluate combinatorial and
    residual part of the activity coefficient
83 //Note : compMolFrac is the referenced from "Material Stream" model
84
85     r = sum(compMolFrac[2, :] .* R[:]);
86     q = sum(compMolFrac[2, :] .* Q[:]);
87
88     //Calculation of Energy interaction parameter at the input tempetraure
89 //Function :Tow_UNIQUAC is used to instantiated
90     tow = Simulator.Files.Thermodynamic_Functions.Tow_UNIQUAC(NOC, a, T);
91 //Calculation of Combinatorial and Residual Activity coefficient

```



```

92
93   for i in 1:NOC loop
94   if(q>0) then
95   teta[i] = compMolFrac[2, i] * Q[i] * (1 / q);
96   elseif(q<0) then
97   teta[i]=0;
98   else
99   teta[i]=0;
100  end if;
101  end for;
102
103  for i in 1:NOC loop
104    if (teta[i]==0) then
105      S[i]=1;
106    else
107      S[i] = sum(teta[:] .* tow[i, :]);
108    end if;
109
110    if(S[i]==1) then
111      sum[i]=sum(teta[:] .* tow[i, :]);
112    else
113      sum[i] = sum(teta[:] .* tow[i, :] ./ S[:]);
114    end if;
115  end for;
116
117  for i in 1:NOC loop
118
119    if(S[i]==1) then
120      C[i] = 0;
121    elseif(S[i]>0 and S[i]<>1) then
122      C[i] = log(S[i]);
123    else
124      C[i]=0;
125    end if;
126
127    (gammar[i]) = exp(Q[i] * (1 - C[i] - sum[i]));
128  end for;
129  // //=====
130  //   equation
131
132  for i in 1:NOC loop
133  if(r>0) then
134  D[i] = R[i]/r;
135  elseif(r<=0) then
136  D[i] =0;
137  else
138  D[i]=0;
139  end if;
140
141  if(q>0) then
142  E[i] = Q[i]/q;
143  elseif(q<=0) then
144  E[i] = 0;
145  else
146  E[i] = 0;
147  end if;
148
149  if(E[i]==0 or D[i]==0) then
150  Ff[i]=0;
151  else
152  Ff[i] = D[i]/E[i];
153  end if;
154
155

```

```

156     if(D[i]>0) then
157     A[i] =log(D[i]);
158     elseif(D[i]==1) then
159     A[i]=0;
160     else
161     A[i]=0;
162     end if;
163
164     if(Ff[i]>0.5) then
165     B[i] =log(Ff[i]);
166     elseif(Ff[i]==1) then
167     B[i]=0;
168     else
169     B[i]=0;
170     end if;
171
172     log(gammac[i])=1-D[i] + A[i] + (-Z / 2 * Q[i] * (1 - Ff[i] + B[i]));
173
174     (gamma[i]) = (gammac[i]) ;// (gammar[i]);
175 end for;
176 //

```

```

177 //Excess Energy parameters are set to 0 since the calculation mode is Ideal
178 resMolSpHeat[:] = zeros(3);
179 resMolEnth[:] = zeros(3);
180 resMolEntr[:] = zeros(3);
181 //Calculation of Saturated vapour pressure and Density at the given input
    condition
182 for i in 1:NOC loop
183     Psat[i] = Simulator.Files.Thermodynamic_Functions.Psat(comp[i].VP, T)
        ;
184     Density[i] = Simulator.Files.Thermodynamic_Functions.Dens(comp[i].
        LiqDen, comp[i].Tc, T, P) * 1E-3;
185 end for;
186 //Calculation of Poynting correction Factor at input conditions,Bubble
    Point and Dew Point
187 //Function :Poynting-CF is called from the Simulator Package
188 PCF[:] = Thermodynamic_Functions.PoyntingCF(NOC, comp[:].Pc, comp[:].
    Tc, comp[:].Racketparam, comp[:].AF, comp[:].MW, T, P, gamma[:],
    Psat[:], Density[:]);
189 phil[:] = gamma[:] .* Psat[:] ./ P .* PCF[:];
190 phil[:] = gamma_new[:] .* Psat[:] ./ P;
191 K[:] = gamma_new[:] .* Psat[:] ./ P;
192 end EXT.UNIQUAC;

```



```

1 model Mat_Stream
2
3 //1 - Mixture, 2 - Liquid phase, 3 - Gas Phase
4 extends Modelica.Icons.SourcesPackage;
5 import Simulator.Files.*;
6 parameter Integer NOC;
7 parameter Simulator.Files.Chemsep_Database.General_Properties comp[NOC];
8 Real P(min = 0, start = 101325) "Pressure", T(start = 273) "Temperature";
9 Real Ppubl(min = 0, start = sum(comp[:].Pc) / NOC) "Bubble point pressure"
    , Pdew(min = 0, start = sum(comp[:].Pc) / NOC) "dew point pressure";
10 Real liqPhasMolFrac(start = 0.5, min = 0, max = 1) "Liquid Phase mole
    fraction", vapPhasMolFrac(start = 0.5, min = 0, max = 1) "Vapor Phase
    mole fraction", liqPhasMasFrac(start = 0.5, min = 0, max = 1) "
    Liquid Phase mass fraction", vapPhasMasFrac(start = 0.5, min = 0, max
    = 1) "Vapor Phase Mass fraction";
11 Real totMolFlo[3](each min = 0, each start = 100) "Total molar flow",
    totMasFlo[3](each min = 0, each start = 100) "Total Mass Flow", MW

```

```

    [3](each start = 0, each min = 0) "Average Molecular weight of Phases
";
12 Real compMolFrac[3, NOC](each min = 0, each max = 1, each start = 1 / (
    NOC + 1)) "Component mole fraction", compMasFrac[3, NOC](each start =
    1 / (NOC + 1), each min = 0, each max = 1) "Component Mass fraction"
    , compMolFlo[3, NOC](each start = 100, each min = 0) "Component Molar
    flow", compMasFlo[3, NOC](each min = 0, each start = 100) "Component
    Mass Fraction";
13 Real phasMolSpHeat[3] "phase Molar Specific Heat", compMolSpHeat[3, NOC]
    "Component Molar Specific Heat";
14 Real phasMolEnth[3] "Phase Molar Enthalpy", compMolEnth[3, NOC] "
    Component Molar Enthalpy";
15 Real phasMolEntr[3] "Phase Molar Entropy", compMolEntr[3, NOC] "Component
    Molar Entropy";
16 Real Liquid_Phase_Density;
17 Real LiqDens[NOC];
18 Simulator.Files.Connection.matConn inlet(connNOC = NOC) annotation(
19     Placement(visible = true, transformation(origin = {-100, 0}, extent =
        {{-10, -10}, {10, 10}}, rotation = 0), iconTransformation(origin =
        {-100, 0}, extent = {{-10, -10}, {10, 10}}, rotation = 0)));
20 Simulator.Files.Connection.matConn outlet(connNOC = NOC) annotation(
21     Placement(visible = true, transformation(origin = {100, 0}, extent =
        {{-10, -10}, {10, 10}}, rotation = 0), iconTransformation(origin =
        {100, 0}, extent = {{-10, -10}, {10, 10}}, rotation = 0)));
22 equation
23 //Connector equations
24 inlet.P = P;
25 inlet.T = T;
26 inlet.mixMolFlo = totMolFlo[1];
27 inlet.mixMolEnth = phasMolEnth[1];
28 inlet.mixMolEntr = phasMolEntr[1];
29 inlet.mixMolFrac = compMolFrac;
30 inlet.vapPhasMolFrac = vapPhasMolFrac;
31 outlet.P = P;
32 outlet.T = T;
33 outlet.mixMolFlo = totMolFlo[1];
34 outlet.mixMolEnth = phasMolEnth[1];
35 outlet.mixMolEntr = phasMolEntr[1];
36 outlet.mixMolFrac = compMolFrac;
37 outlet.vapPhasMolFrac = vapPhasMolFrac;
38 //


---


39 //Mole Balance
40 totMolFlo[1] = totMolFlo[2] + totMolFlo[3];
41 compMolFrac[1, :] .* totMolFlo[1] = compMolFrac[2, :] .* totMolFlo[2] +
    compMolFrac[3, :] .* totMolFlo[3];
42 //component molar and mass flows
43 for i in 1:NOC loop
44     compMolFlo[:, i] = compMolFrac[:, i] .* totMolFlo[:];
45 end for;
46 if P >= Ppubl then
47 //below bubble point region
48     compMasFrac[3, :] = zeros(NOC);
49     compMasFlo[1, :] = compMasFrac[1, :] .* totMasFlo[1];
50     compMasFrac[2, :] = compMasFrac[1, :];
51 elseif P >= Pdew then
52     for i in 1:NOC loop
53         compMasFlo[:, i] = compMasFrac[:, i] .* totMasFlo[:];
54     end for;
55 else
56 //above dew point region
57     compMasFrac[2, :] = zeros(NOC);
58     compMasFlo[1, :] = compMasFrac[1, :] .* totMasFlo[1];

```

```

59     compMasFrac[3, :] = compMasFrac[1, :];
60     end if;
61 //phase molar and mass fractions
62     liqPhasMolFrac = totMolFlo[2] / totMolFlo[1];
63     vapPhasMolFrac = totMolFlo[3] / totMolFlo[1];
64     liqPhasMasFrac = totMasFlo[2] / totMasFlo[1];
65     vapPhasMasFrac = totMasFlo[3] / totMasFlo[1];
66 // Conversion between mole and mass flow
67     for i in 1:NOC loop
68         compMasFlo[:, i] = compMolFlo[:, i] * comp[i].MW;
69     end for;
70     totMasFlo[:] = totMolFlo[:] .* MW[:];
71 //Energy Balance
72     for i in 1:NOC loop
73 // Specific Heat and Enthalpy calculation
74         compMolSpHeat[2, i] = Thermodynamic_Functions.LiqCpId(comp[i].LiqCp, T)
75         ;
76         compMolSpHeat[3, i] = Thermodynamic_Functions.VapCpId(comp[i].VapCp, T)
77         ;
78         compMolEnth[2, i] = Thermodynamic_Functions.HLiqId(comp[i].SH, comp[i].
79             VapCp, comp[i].HOV, comp[i].Tc, T);
80         compMolEnth[3, i] = Thermodynamic_Functions.HVapId(comp[i].SH, comp[i].
81             VapCp, comp[i].HOV, comp[i].Tc, T);
82         (compMolEntr[2, i], compMolEntr[3, i]) = Thermodynamic_Functions.SId(
83             comp[i].AS, comp[i].VapCp, comp[i].HOV, comp[i].Tb, comp[i].Tc, T,
84             P, compMolFrac[2, i], compMolFrac[3, i], Liquid_Phase_Density);
85     end for;
86     for i in 2:3 loop
87         phasMolSpHeat[i] = sum(compMolFrac[i, :] .* compMolSpHeat[i, :]) +
88             resMolSpHeat[i];
89         phasMolEnth[i] = sum(compMolFrac[i, :] .* compMolEnth[i, :]) +
90             resMolEnth[i];
91         phasMolEntr[i] = sum(compMolFrac[i, :] .* compMolEntr[i, :]) +
92             resMolEntr[i];
93     end for;
94     phasMolSpHeat[1] = liqPhasMolFrac * phasMolSpHeat[2] + vapPhasMolFrac *
95         phasMolSpHeat[3];
96     compMolSpHeat[1, :] = compMolFrac[1, :] .* phasMolSpHeat[1];
97     phasMolEnth[1] = liqPhasMolFrac * phasMolEnth[2] + vapPhasMolFrac *
98         phasMolEnth[3];
99     compMolEnth[1, :] = compMolFrac[1, :] .* phasMolEnth[1];
100    phasMolEntr[1] = liqPhasMolFrac * phasMolEntr[2] + vapPhasMolFrac *
101        phasMolEntr[3];
102    compMolEntr[1, :] = compMolFrac[1, :] * phasMolEntr[1];
103 //Bubble point calculation
104    Pbubl = sum(gammaBubl[:] .* compMolFrac[1, :] .* exp(comp[:].VP[2] + comp
105        [:].VP[3] / T + comp[:].VP[4] * log(T) + comp[:].VP[5] .* T.^ comp
106        [:].VP[6]) ./ liqfugcoeff_bubl[:]);
107 //Dew point calculation
108    Pdew = 1 / sum(compMolFrac[1, :] ./ (gammaDew[:] .* exp(comp[:].VP[2] +
109        comp[:].VP[3] / T + comp[:].VP[4] * log(T) + comp[:].VP[5] .* T.^
110        comp[:].VP[6])) .* vapfugcoeff_dew[:]);
111     if P >= Pbubl then
112 //below bubble point region
113         compMolFrac[3, :] = zeros(NOC);
114         sum(compMolFrac[2, :]) = 1;
115     elseif P >= Pdew then
116 //VLE region
117         for i in 1:NOC loop
118             compMolFrac[3, i] = K[i] * compMolFrac[2, i];
119         end for;
120         sum(compMolFrac[3, :]) = 1;
121 //sum y = 1
122     else

```

```

107 //above dew point region
108   compMolFrac[2, :] = zeros(NOC);
109   sum(compMolFrac[3, :]) = 1;
110   end if;
111   algorithm
112     for i in 1:NOC loop
113       MW[:] := MW[:] + comp[i].MW * compMolFrac[:, i];
114     end for;
115     LiqDens[:] := Thermodynamic_Functions.Density_Racket(NOC, T, P, comp[:].
      Pc, comp[:].Tc, comp[:].Racketparam, comp[:].AF, comp[:].MW, Psat
      [:]);
116
117     Liquid_Phase_Density := 1 / sum(compMasFrac[2, :] ./ LiqDens[:]) / MW[2];
118
119   end Mat_Stream;

```

```

1   model UNIQUAC_Correction
2     //Libraries
3     import Simulator.Files.*;
4     //Parameter Section
5     //Binary Interaction Parameters
6     //Function :BIP-UNIQUAC is used to obtain the interaction parameters
7     parameter Real a[NOC, NOC] = Thermodynamic_Functions.BIP-UNIQUAC(NOC,
      comp.name);
8     //Uniquac Parameters R and Q called from Chemsep Database
9     parameter Real R[NOC] = comp.UniquacR;
10    parameter Real Q[NOC] = comp.UniquacQ;
11    parameter Integer Z = 10 "Compressibility-Factor";
12    //Variable Section
13    Real tow[NOC, NOC] "Energy interaction parameter";
14    //Intermediate variables to calculate the combinatorial and residual
      part of activity coefficient at the input conditions
15    Real r(each start=2, min=0,max=1), q(each start=2);
16    Real teta[NOC];
17    Real S[NOC](each start = 1);
18    Real sum[NOC];
19    //Activity Coefficients
20    Real gammac[NOC](each start = 1.2) "Combinatorial Part of activity
      coefficient at input conditions";
21    Real gammar[NOC](each start = 1.2) "Residual part of activity
      coefficient at input conditions";
22    Real gamma_new[NOC](each start = 1.2);
23    Real gamma[NOC](each start = 1.2) "Activity coefficient with Poynting
      correction";
24    //Fugacity coefficient
25    Real phil[NOC](each start = 0.5) "Fugacity coefficient at the input
      conditions";
26    //Dew Point Calculation Variables
27    Real dewLiqMolFrac[NOC](each start=0.5, each min=0, each max=1);
28    //Intermediate variables to calculate the combinatorial and residual
      part of activity coefficient at dew point
29    Real r_dew(start=2), q_dew(start=2);
30    Real teta_dew[NOC](each start=2);
31    Real S_dew[NOC](each start = 1);
32    Real sum_dew[NOC](each start=2);
33    //Activity Coefficients
34    Real gammac_dew[NOC](each start = 5) "Combinatorial Part of activity
      coefficient at dew point";
35    Real gammar_dew[NOC](each start = 2.5) "Residual part of activity
      coefficient at dew point";
36    Real gammaDew_old[NOC](each start = 2.2) "Combinatorial Part of
      activity coefficient(without correction)";
37    Real gammaDew[NOC](each start = 2.2) "Activity coefficient at dew point"

```

```

38     ;
39     //Fugacity coefficient
40     Real vapfugcoeff_dew[NOC] "Vapour Fugacity coefficient at dew point";
41     Real phil_dew[NOC](each start = 0.5);
42     Real PCF_dew[NOC] "Poynting Correction Factor";
43     //Bubble Point Calculation Variables
44     //Intermediate variables to calculate the combinatorial and residual
45     part of activity coefficient at bubble point
46     Real r_bubl(start=2), q_bubl(start=2);
47     Real teta_bubl[NOC];
48     Real S_bubl[NOC];
49     Real sum_bubl[NOC];
50     //Activity Coefficients
51     Real gammac_bubl[NOC](each start = 2) "Combinatorial Part of activity
52     coefficient at bubble point";
53     Real gammar_bubl[NOC](each start = 1) "Residual part of activity
54     coefficient at bubble point";
55     Real gammaBubl_old[NOC](each start = 1) "Combinatorial Part of activity
56     coefficient (without correction)";
57     Real gammaBubl[NOC](each start = 1) "Activity coefficient at bubble
58     point";
59     //Fugacity coefficient
60     Real liqfugcoeff_bubl[NOC];
61     Real phil_bubl[NOC](each start = 0.5) "Liquid Phase Fugacity
62     coefficient";
63     Real PCF_bubl[NOC] "Poynting Correction Factor";
64     //Phase Envelope
65     Real Psat[NOC](each unit = "Pa") "Saturated Vapour Pressure at the
66     input temperature";
67     Real PCF[NOC] "Poynting correction factor";
68     Real K[NOC](each start = 0.7) "Distribution Coefficient";
69     //Residual Energy Parameters
70     Real resMolSpHeat[3], resMolEnth[3], resMolEntr[3];
71     //Transport Properties at the input conditions
72     Real Density[NOC](each unit = "kmol/m^3");
73     Real A[NOC], B[NOC], D[NOC], E[NOC], Ff[NOC];
74     Real C[NOC];
75     Real A_bubl[NOC], B_bubl[NOC], C_bubl[NOC], D_bubl[NOC], E_bubl[NOC], F_bubl
76     [NOC];
77     Real A_dew[NOC], B_dew[NOC], C_dew[NOC], D_dew[NOC], E_dew[NOC], F_dew[NOC];
78     //
79
80     //Equation Section
81     equation
82     //Fugacity coefficients set to 1 since the model type is Activity
83     Coefficient
84     for i in 1:NOC loop
85     liqfugcoeff_bubl[i] = 1;
86     vapfugcoeff_dew[i] = 1;
87     end for;
88     //Calculation of Intermediate parameters to evaluate combinatorial and
89     residual part of the activity coefficient
90     //Note : compMolFrac is the referenced from "Material Stream" model
91
92     r = sum(compMolFrac[2, :] .* R[:]);
93     q = sum(compMolFrac[2, :] .* Q[:]);
94
95     //Calculation of Energy interaction parameter at the input tempetraure
96     //Function :Tow_UNIQUAC is used to instantiated
97     tow = Simulator.Files.Thermodynamic_Functions.Tow_UNIQUAC(NOC, a, T);
98     //Calculation of Combinatorial and Residual Activity coefficient
99
100    for i in 1:NOC loop

```

```

89     if(q>0) then
90     teta[i] = compMolFrac[2, i] * Q[i] * (1 / q);
91     elseif(q<0) then
92     teta[i]=0;
93     else
94     teta[i]=0;
95     end if;
96     end for;
97
98     for i in 1:NOC loop
99         if (teta[i]==0) then
100         S[i]=1;
101         else
102         S[i] = sum(teta[:] .* tow[i, :]);
103         end if;
104
105         if(S[i]==1) then
106         sum[i]=0;
107         else
108         sum[i] = sum(teta[:] .* tow[i, :] ./ S[:]);
109         end if;
110     end for;
111
112     for i in 1:NOC loop
113
114         if(S[i]==1) then
115         C[i] = 0;
116         elseif(S[i]>0) then
117         C[i] = log(S[i]);
118         else
119         C[i]=0;
120         end if;
121
122         (gammar[i]) = exp(Q[i] * (1 - C[i] - sum[i]));
123     end for;
124 // //=====
125 //         equation
126
127     for i in 1:NOC loop
128     if(r>0) then
129     D[i] = R[i]/r;
130     elseif(r<=0) then
131     D[i] =0;
132     else
133     D[i]=0;
134     end if;
135
136     if(q>0) then
137     E[i] = Q[i]/q;
138     elseif(q<=0) then
139     E[i] = 0;
140     else
141     E[i] = 0;
142     end if;
143
144     if(E[i]==0 or D[i]==0) then
145     Ff[i]=0;
146     else
147     Ff[i] = D[i]/E[i];
148     end if;
149
150
151     if(D[i]>0) then
152     A[i] =log(D[i]);

```

```

153     elseif(D[i]==1) then
154     A[i]=0;
155     else
156     A[i]=0;
157     end if;
158
159     if(Ff[i]>1) then
160     B[i] =log(Ff[i]);
161     elseif(Ff[i]==1) then
162     B[i]=0;
163     else
164     B[i]=0;
165     end if;
166
167     log(gammac[i])=1-D[i] + A[i] + (-Z / 2 * Q[i] * (1 - Ff[i] + B[i]));
168
169     (gamma[i]) = (gammac[i]) * (gammar[i]);
170 end for;
171 //

```

```

172 //Excess Energy parameters are set to 0 since the calculation mode is Ideal
173 resMolSpHeat[:] = zeros(3);
174 resMolEnth[:] = zeros(3);
175 resMolEntr[:] = zeros(3);
176 //Calculation of Saturated vapour pressure and Density at the given input
    condition
177 for i in 1:NOC loop
178     Psat[i] = Simulator.Files.Thermodynamic_Functions.Psat(comp[i].VP, T)
179     ;
180     Density[i] = Simulator.Files.Thermodynamic_Functions.Dens(comp[i].
        LiqDen, comp[i].Tc, T, P) * 1E-3;
181 end for;
182 //Calculation of Poynting correction Factor at input conditions,Bubble
    Point and Dew Point
183 //Function :Poynting-CF is called from the Simulator Package
184 PCF[:] = Thermodynamic_Functions.PoyntingCF(NOC, comp[:].Pc, comp[:].
    Tc, comp[:].Racketparam, comp[:].AF, comp[:].MW, T, P, gamma[:],
    Psat[:], Density[:]);
185 PCF_bubl[:] = Thermodynamic_Functions.PoyntingCF(NOC, comp[:].Pc, comp
    [:].Tc, comp[:].Racketparam, comp[:].AF, comp[:].MW, T, Pbubl,
    gamma[:], Psat[:], Density[:]);
186 PCF_dew[:] = Thermodynamic_Functions.PoyntingCF(NOC, comp[:].Pc, comp
    [:].Tc, comp[:].Racketparam, comp[:].AF, comp[:].MW, T, Pdew, gamma
    [:], Psat[:], Density[:]);
187 //Calculation of Fugacity coefficient with Poynting correction
188 phil[:] = gamma[:] .* Psat[:] ./ P .* PCF[:];
189 phil[:] = gamma_new[:] .* Psat[:] ./ P;
190 //Calculation of Distribution coefficient
191 K[:] = gamma_new[:] .* Psat[:] ./ P;
192 //Binary Phase Envelope
193 //The same calculation routine is followed at the DewPoint
194 //Dew Point
195 r_dew = sum(dewLiqMolFrac[:] .* R[:]);
196 q_dew = sum(dewLiqMolFrac[:] .* Q[:]);
197 for i in 1:NOC loop
198     if(q_dew==0 or compMolFrac[1,i]==0) then
199         dewLiqMolFrac[i]=0;
200     else
201         dewLiqMolFrac[i] = compMolFrac[1, i] * Pdew / (gammaDew[i] * Psat[i])
202         ;
203     end if;
204     if(q_dew==0 or dewLiqMolFrac[i]==0) then
205         teta_dew[i]=0;

```



```

204     else
205         teta_dew[i] = dewLiqMolFrac[i] * Q[i] * (1 / q_dew);
206     end if;
207     if(teta_dew[i]==0) then
208         S_dew[i] =1;
209     else
210         S_dew[i] = sum(teta_dew[:] .* tow[i, :]);
211     end if;
212     end for;
213 //

```

```

214
215     for i in 1:NOC loop
216         if(S_dew[i]==1) then
217             sum_dew[i]=0;
218         else
219             sum_dew[i] = sum(teta_dew[:] .* tow[i, :] ./ (S_dew[:]));
220         end if;
221
222
223         if(S_dew[i]==1) then
224             C_dew[i]=0;
225         elseif(S_dew[i]>0) then
226             C_dew[i] =log(S_dew[i]);
227         else
228             C_dew[i]=0;
229         end if;
230
231         (gammar_dew[i]) = exp(Q[i] * (1 - C_dew[i] - sum_dew[i]));
232     end for;
233 //

```

```

234
235     for i in 1:NOC loop
236         if(r_dew==0) then
237             D_dew[i] =0;
238         else
239             D_dew[i] = R[i]/r_dew;
240         end if;
241
242         if(q_dew==0) then
243             E_dew[i] = 0;
244         else
245             E_dew[i] = Q[i]/q_dew;
246         end if;
247
248         if(E_dew[i]==0) then
249             F_dew[i]=0;
250         else
251             F_dew[i] = D_dew[i]/E_dew[i];
252         end if;
253
254
255         if(D_dew[i]>0) then
256             A_dew[i] =log(D_dew[i]);
257         elseif(D_dew[i]==1) then
258             A_dew[i]=0;
259         else
260             A_dew[i]=0;
261         end if;
262
263         if(F_dew[i]>0) then

```

```

264     B_dew[i] =log(F_dew[i]);
265     elseif(F_dew[i]==1) then
266     B_dew[i]=0;
267     else
268     B_dew[i]=0;
269     end if;
270
271     log(gammac_dew[i]=1-D_dew[i] + A_dew[i] + (-Z / 2 * Q[i] * (1 -
      F_dew[i] + B_dew[i]));
272
273     (gammaDew_old[i] ) = (gammac_dew[i]) * (gammar_dew[i]);
274 end for;
275
276 for i in 1:NOC loop
277 if(Pdew==0) then
278 phil_dew[i]=1;
279 gammaDew[i]=1;
280
281 else
282
283 phil_dew[i] = gammaDew_old[i] .* Psat[i] ./ Pdew .* PCF_dew[i];
284 phil_dew[i] = gammaDew[i] .* Psat[i] ./ Pdew;
285 end if;
286 end for;
287 //The same calculation routine is followed at the Bubble Point
288 //Bubble Point
289 r_bubl = sum(compMolFrac[1, :] .* R[:]);
290 q_bubl = sum(compMolFrac[1, :] .* Q[:]);
291 for i in 1:NOC loop
292 if(compMolFrac[1, i]==0) then
293 teta_bubl[i]=0;
294 else
295 teta_bubl[i] = compMolFrac[1, i] * Q[i] * (1 / q_bubl);
296 end if;
297
298 if(teta_bubl[i]==0) then
299 S_bubl[i] =1;
300 else
301 S_bubl[i] = sum(teta_bubl[:] .* tow[i, :]);
302 end if;
303
304 if(S_bubl[i]==1) then
305 sum_bubl[i]=0;
306 else
307 sum_bubl[i] = sum(teta_bubl[:] .* tow[i, :] ./ S_bubl[:]);
308 end if;
309
310
311 if(S_bubl[i]==1) then
312 C_bubl[i] =0 ;
313 elseif(S_bubl[i]>0) then
314 C_bubl[i]=log(S_bubl[i]);
315 else
316 C_bubl[i]=0;
317 end if;
318 log(gammar_bubl[i]) = Q[i] * (1 - C_bubl[i] - sum_bubl[i]);
319 //

```

```

320
321 if(r_bubl==0) then
322 D_bubl[i] =0;
323 else
324 D_bubl[i] = R[i]/r_bubl;

```

```

325     end if;
326
327     if (q_bubl==0) then
328         E_bubl[i] = 0;
329     else
330         E_bubl[i] = Q[i]/q_bubl;
331     end if;
332
333     if (E_bubl[i]==0) then
334         F_bubl[i]=0;
335     else
336         F_bubl[i] = D_bubl[i]/E_bubl[i];
337     end if;
338
339
340     if (D_bubl[i]>0) then
341         A_bubl[i] =log(D_bubl[i]);
342     elseif (D_bubl[i]==1) then
343         A_bubl[i]=0;
344     else
345         A_bubl[i]=0;
346     end if;
347
348     if (F_bubl[i]>0) then
349         B_bubl[i] =log(F_bubl[i]);
350     elseif (F_bubl[i]==1) then
351         B_bubl[i]=0;
352     else
353         B_bubl[i]=0;
354     end if;
355
356     log(gammac_bubl[i])=1-D_bubl[i] + A_bubl[i] + (-Z / 2 * Q[i] * (1 -
        F_bubl[i] + B_bubl[i]));
357
358     (gammaBubl_old[i]) = (gammac_bubl[i]) * (gammar_bubl[i]);
359 end for;
360
361 for i in 1:NOC loop
362 if (Pbubl==0) then
363     phil_bubl[i]=1;
364     gammaBubl[i]=1;
365 else
366     phil_bubl[i] = gammaBubl_old[i] .* Psat[i] ./ Pbubl .* PCF_bubl[i];
367     phil_bubl[i] = gammaBubl[i] .* Psat[i] ./ Pbubl;
368 end if;
369 end for;
370 end UNIQUAC_Correction;

```